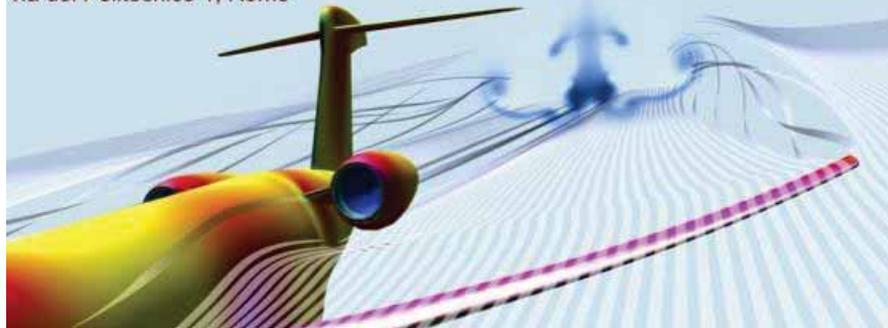


# FLEXIBLE ENGINEERING TOWARD GREEN AIRCRAFT

CAE tools for sustainable mobility

December 14, 9.00 - 14.00

University of Rome "Tor Vergata", Aula Convegni Ingegneria  
via del Politecnico 1, Rome



## Aeroelastic Experimental measurements on the RIBES wing

F. Nicolosi

University of Naples «Federico II»

Dep. of Industrial Engineering

[fabrnico@unina.it](mailto:fabrnico@unina.it)



UNIVERSITÀ DEGLI STUDI DI NAPOLI  
FEDERICO II



DIPARTIMENTO DI  
INGEGNERIA  
INDUSTRIALE

SEZIONE  
INGEGNERIA AEROSPAZIALE



Design of Aircraft and Flight technologies

RESEARCH GROUP

[www.daf.unina.it](http://www.daf.unina.it)

## **DAF (Design of Aircraft and Flight Technologies) research group**

- Focused on Aircraft Design
- Applied aerodynamics and aerodynamic design of transport aircraft
- Wind-Tunnel tests
- Flight Mechanics and performance
- Flight Dynamics, flight tests and flight simulation



UNIVERSITÀ DEGLI STUDI DI NAPOLI  
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SEZIONE  
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*Prof. F. Nicolosi*

*Prof. A. De Marco*

*Prof. P. Della Vecchia*

*Ing. S. Corcione (Post- Doc), Ing. D. Ciliberti (Post-Doc)*

*Ing. V. Cusati (PHD stud)*

*Ing. M. Ruocco (PHD stud)*

*Ing. V. Trifari (PHD stud)*

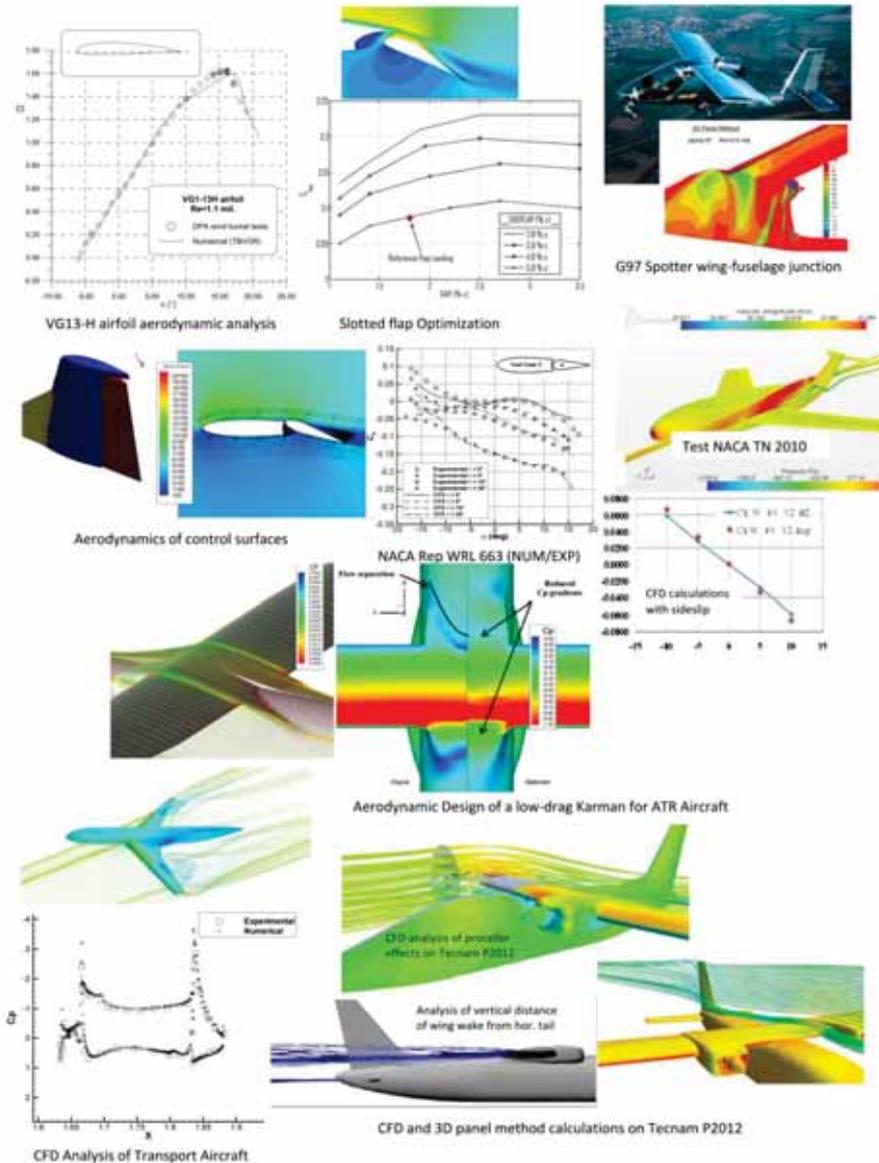
*Ing. L. Stingo (PHD stud)*



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# Aircraft applied aerodynamics and aerodynamic design

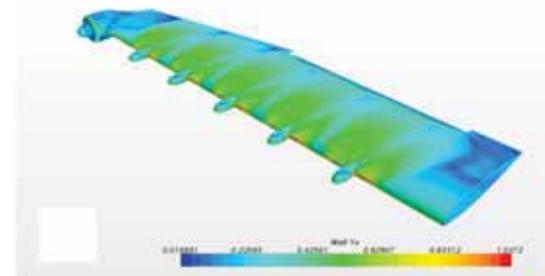


## USE and development of different tools:

- CFD Navier-Stokes analysis
- Panel method
- Vortex lattice
- L1,5 procedures

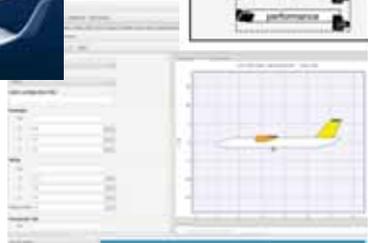
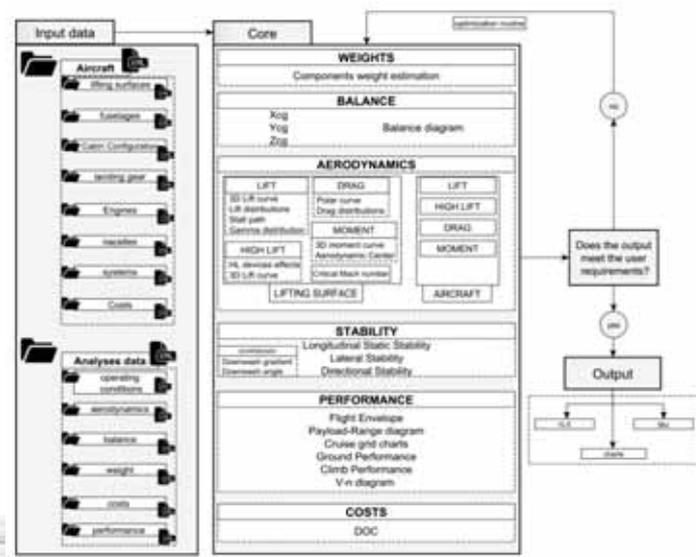
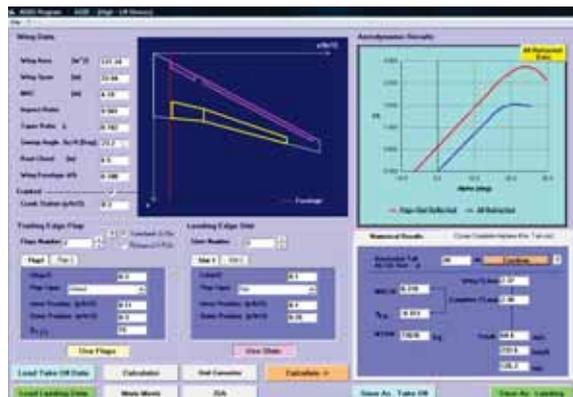
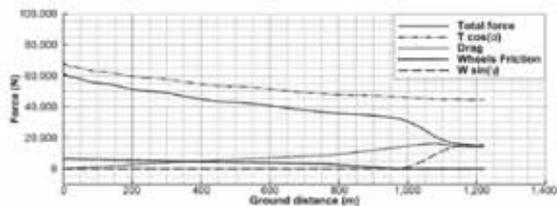
## Component design and optimization

- 2-D airfoil optimization
- Wing optimization
- Winglet
- Fairing and karman
- Control surfaces
- Distributed propulsion



# Aircraft Design and Flight Mechanics

- Aircraft Design
- Aircraft Design framework Development
- Flight Mechanics
- Aircraft Performance
- Aircraft cost and operations
- Aircraft MDO



## Wind-Tunnel tests

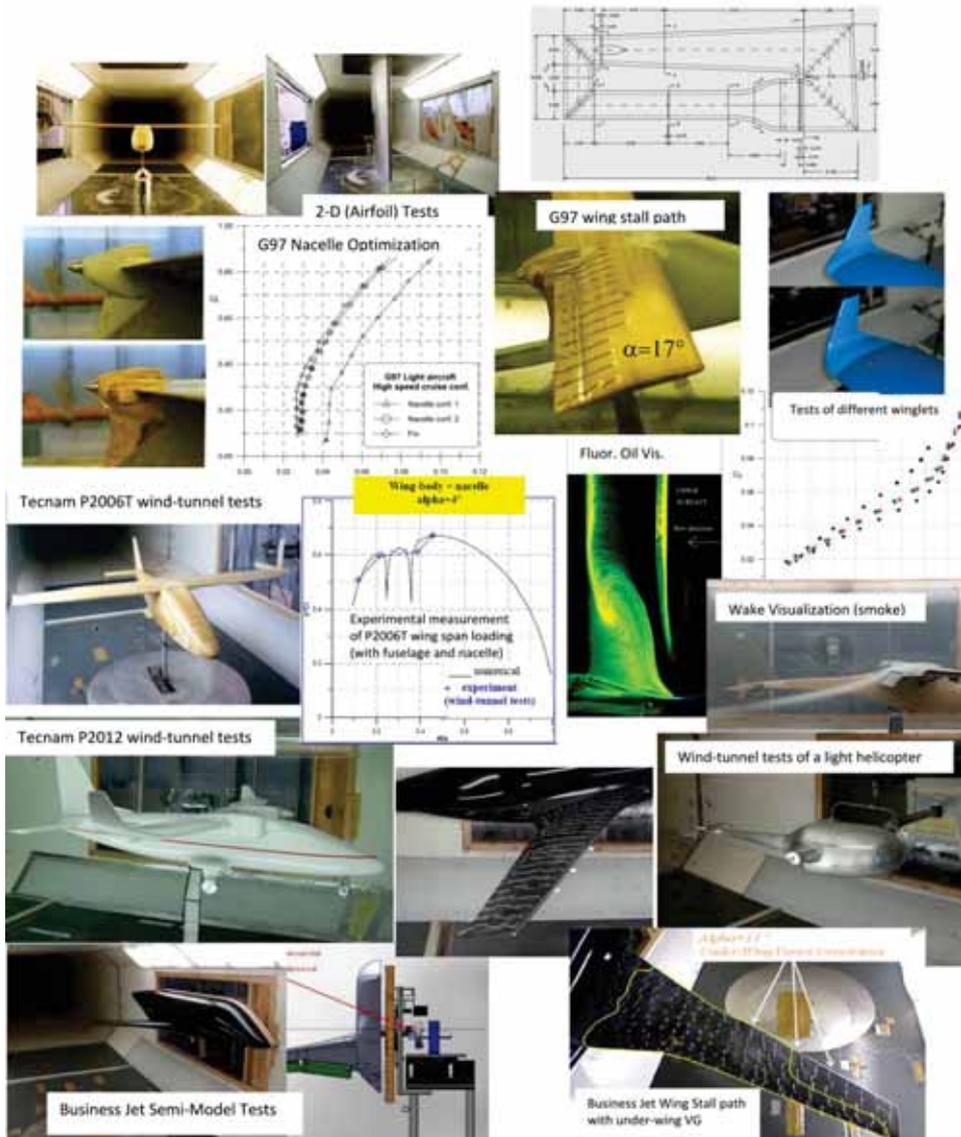
- Design of wind-tunnel models
- Test article instrumentation
- Wind tunnel instrumentation (i.e. visualization)
- Numerical-Experimental comparison

### TESTS

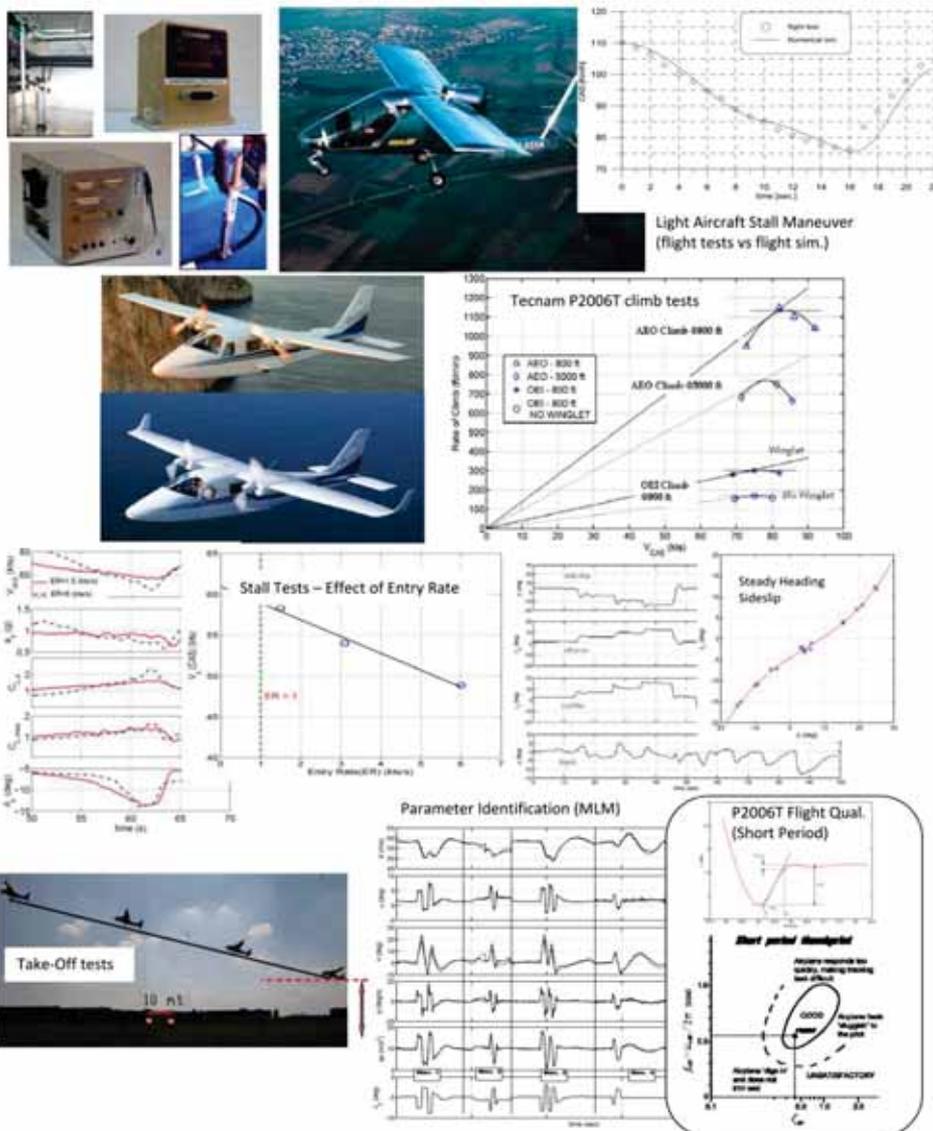
- 3-D scaled model
- Semi-model
- 2-D airfoil tests
- Helicopter (no rotor)

⇒ About 20 airfoils tested (10 designed at UNINA for light aircraft and wind-turbine applications)

⇒ Since 1996 30 aircraft models tested



## Flight Tests and flight simulation



- Flight tests certification
- Performance Estimation and tests
- System identification
- Flight qualities
- Set-up of the flight simulation model

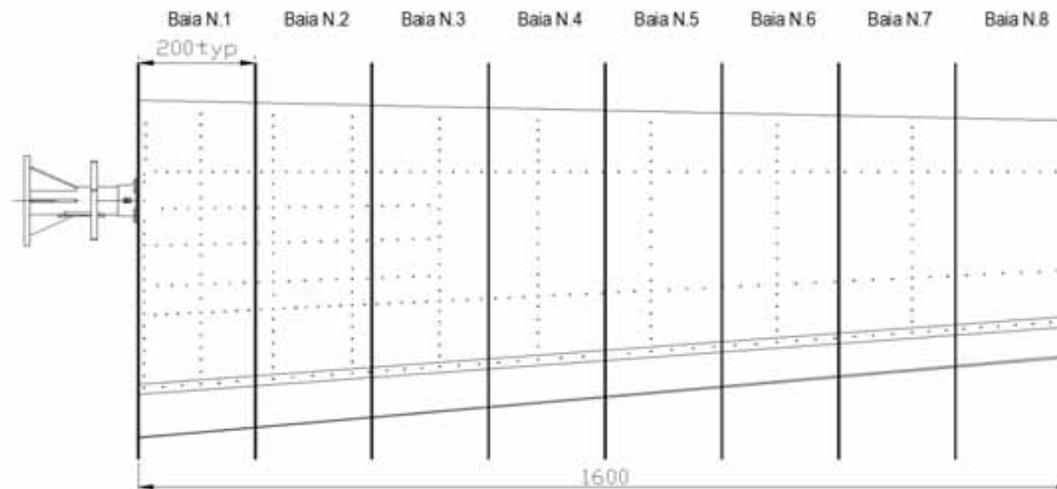
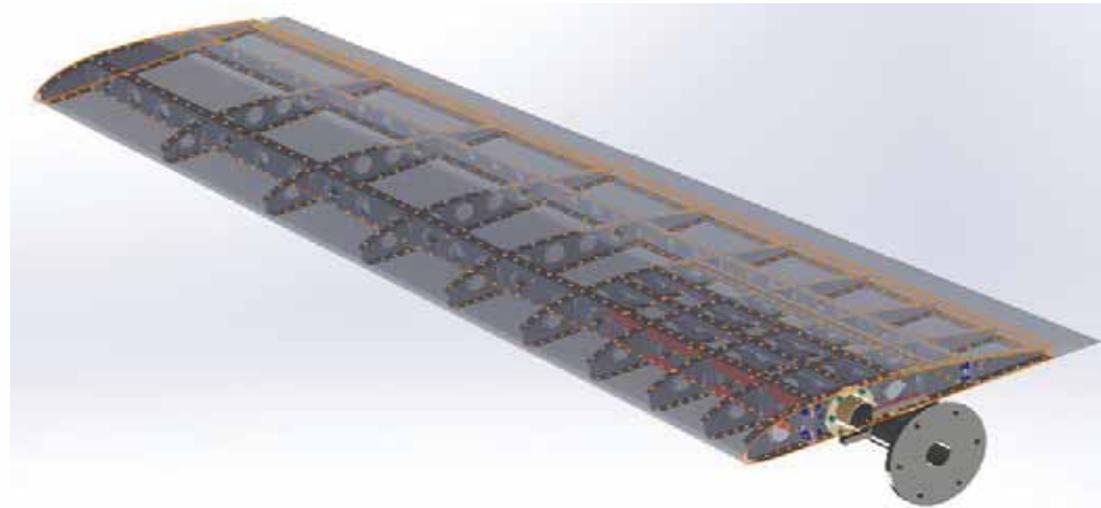
### APPLICATIONS:

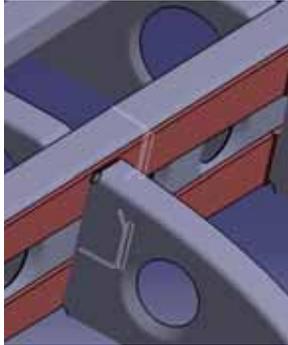
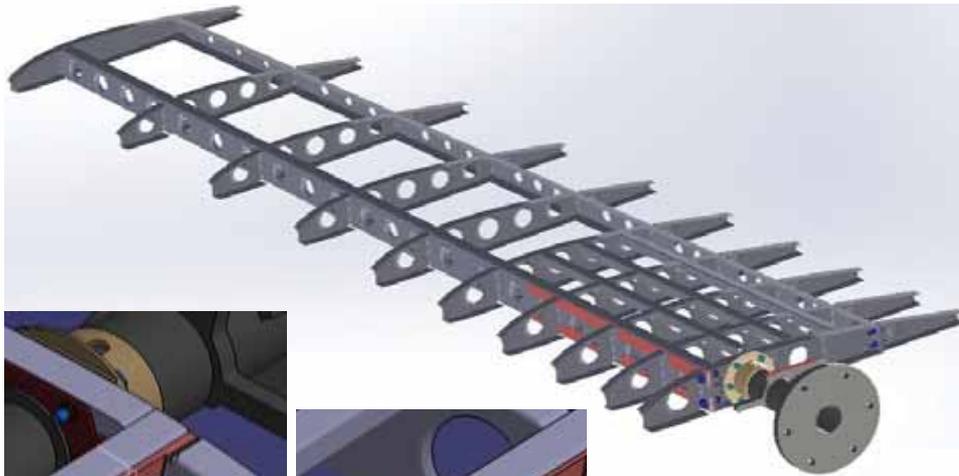
- Flight tests of P92 and P96 (Tecnam)
- Flight tests and VLA certification of G97 Spotter (2000-2004)
- Flight tests and VLA certification of P2000 RG (Tecnam)
- Flight tests and certification of P2006T
- Support for Oma-Sud Sky Car
- Flight tests of P2008

# Design of the wing model for RIBES wind-tunnel tests

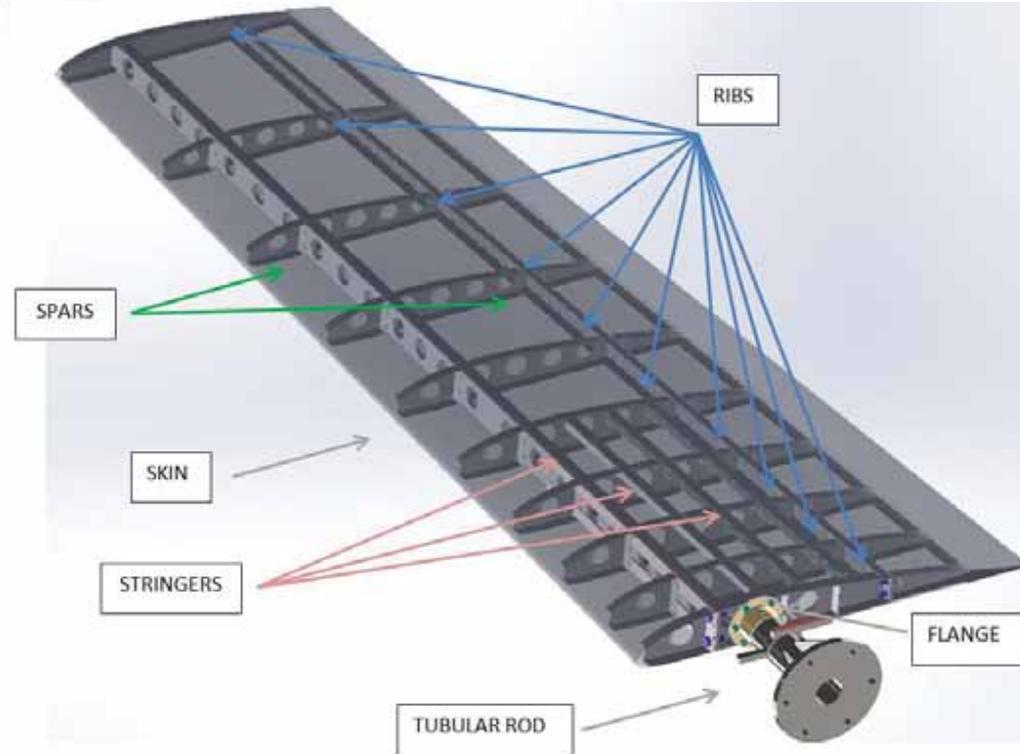
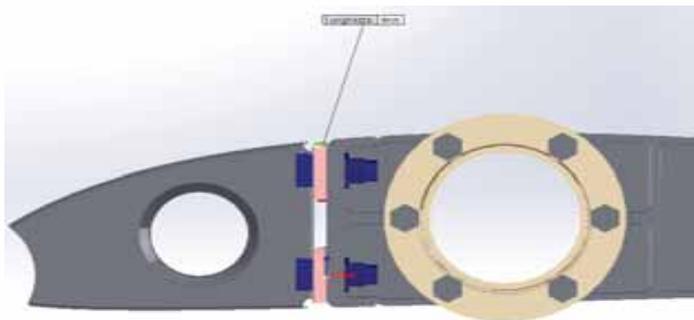


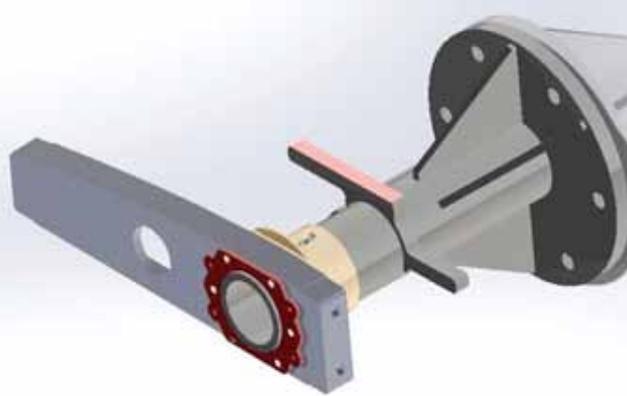
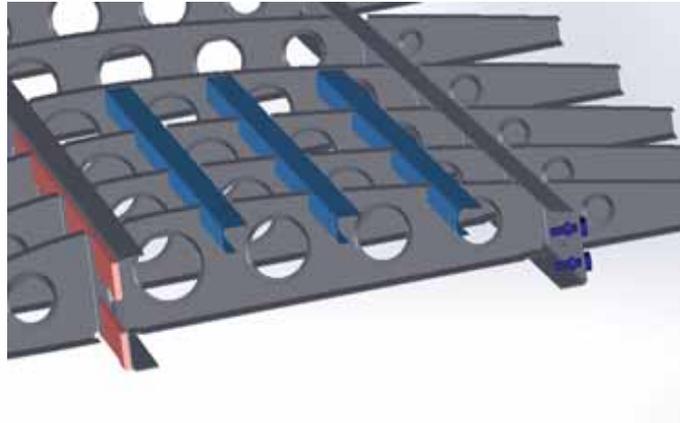
Wing span $b$	1.60 m
Root chord $c_{root}$	0.6 m
Taper ratio TR	0.7
Aft spar position % of chord	20 %
Rear spar position % of chord	65 %
Airfoil	GOE 398
Material	AL2024T3 aluminum alloy



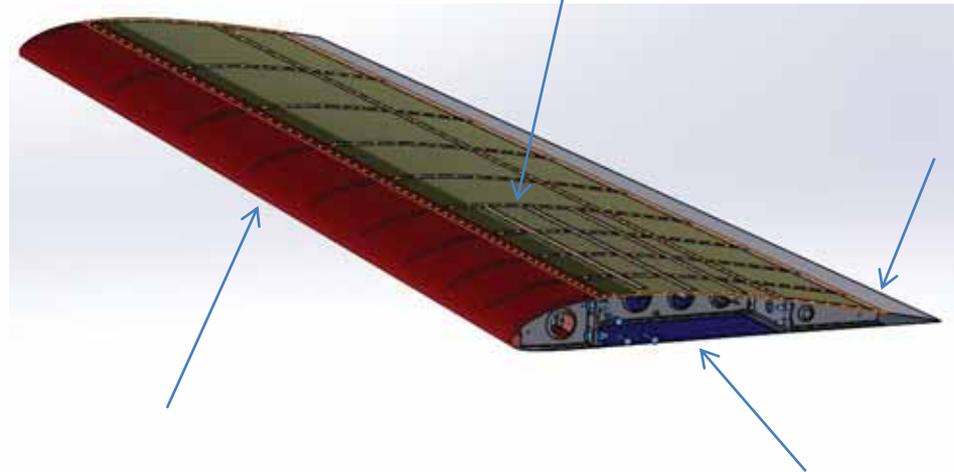
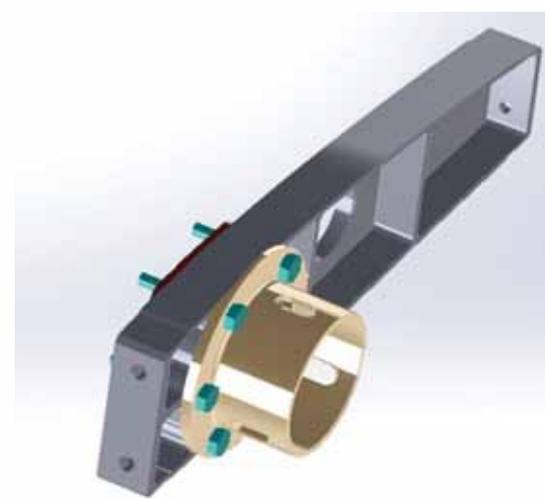


thickening of T2024T3 aluminum alloy on the front spar

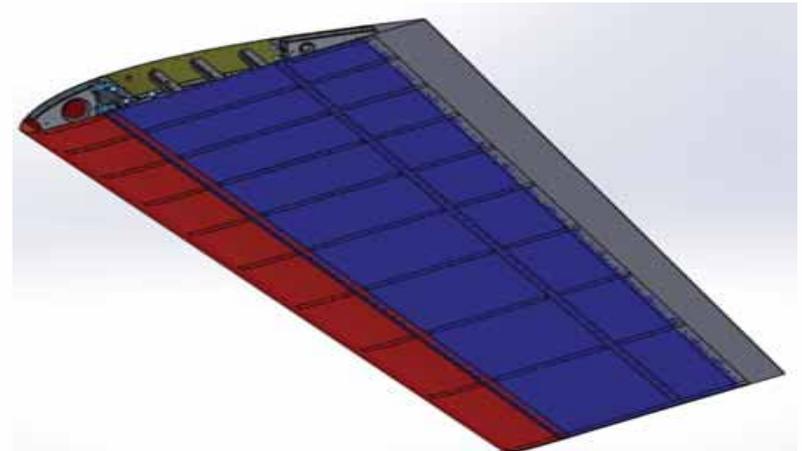


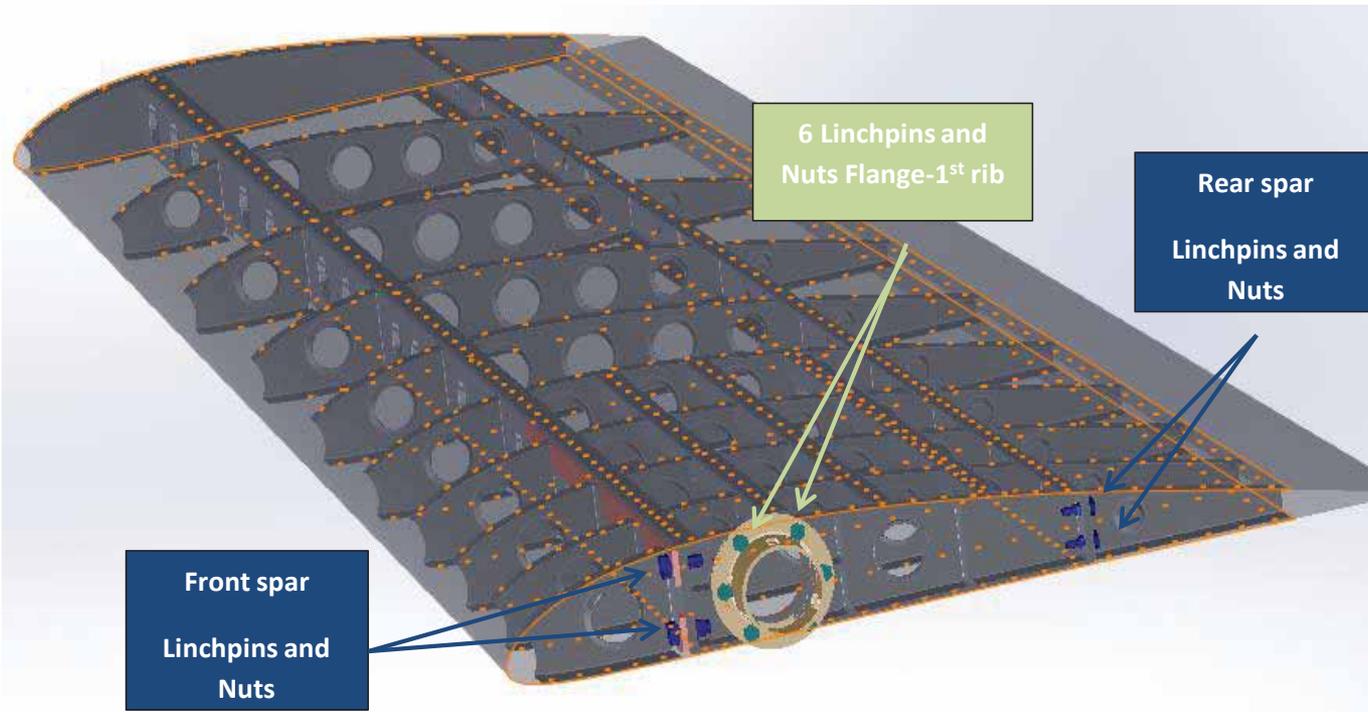


First machined rib and tubular rod attachment for model a. of a. reg.



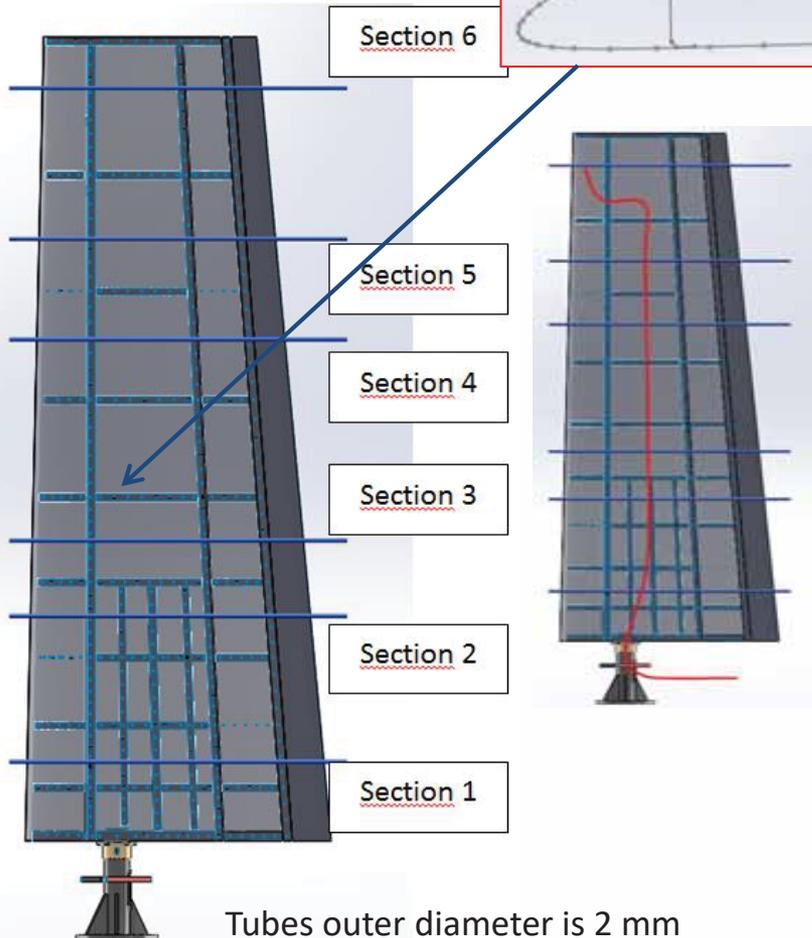
4 Aluminum alloy panels





- n. 800 (eight hundred) rivets cherry max (see Section 4.4 and 4.5)
- n.6 (six) linchpins of 4.8 mm AN type
- n.6 (six) nuts of 4.8 mm MS210442 or equivalent type
- n.2 (two) linchpins of 7.92 mm e n.2 (two) nuts to join front spar to the 1<sup>st</sup> ribs.
- n.2 (two) linchpins of 4.8 mm e n.2 (two) nuts to join rear spar to the 1<sup>st</sup> ribs.

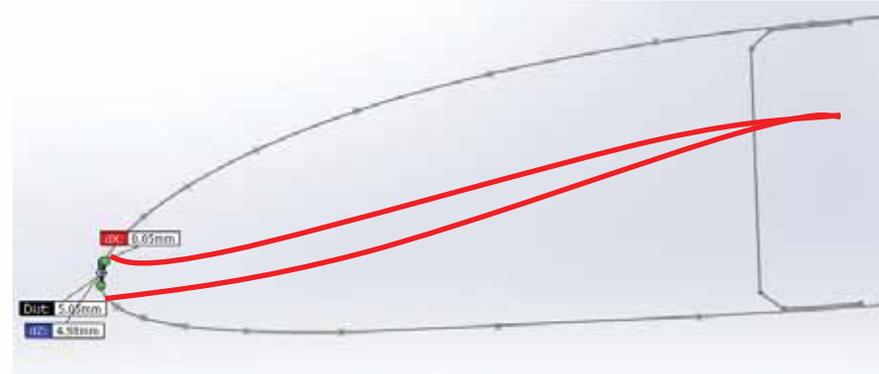
## Pressure taps



Tubes outer diameter is 2 mm  
 Tubes inner diameter is 1 mm  
 Tubes do not coincide with rivets and ribs  
 Tubes go through ribs and spars holes

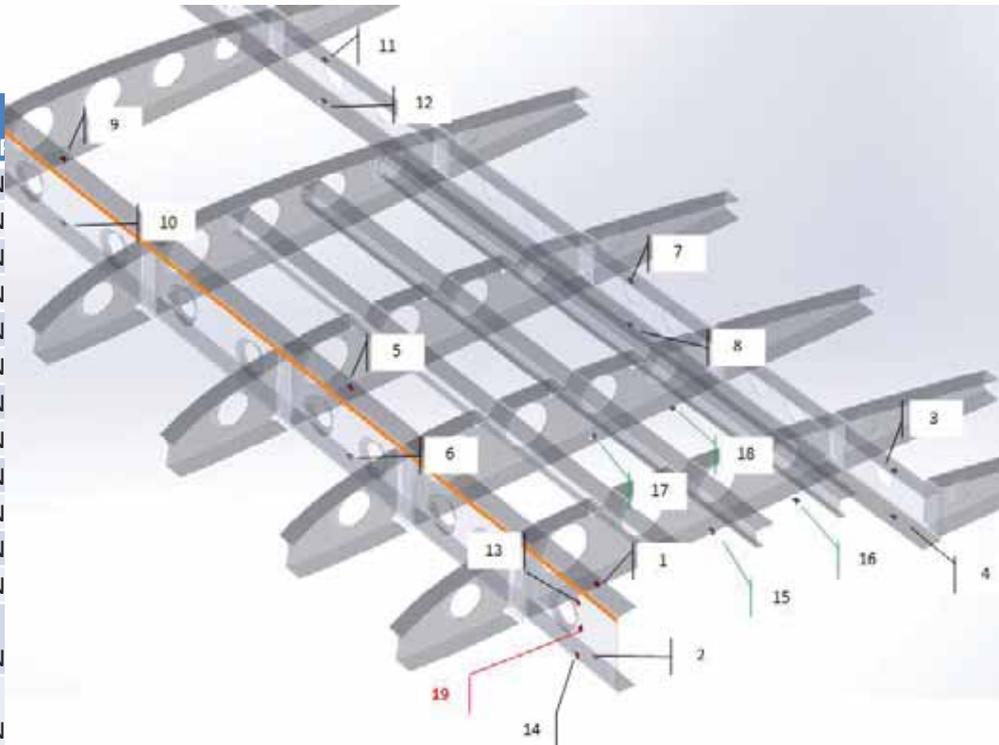


NAM E ID	SECT	y(mm )	$\eta$	Chord( m)	N. Pressure taps
A	1	160	0.100	0.582	4
B	2	450	0.281	0.549	4
C	3	600	0.375	0.533	38
D	4	990	0.619	0.488	4
E	5	1200	0.750	0.465	26
F	6	1600	0.938	0.431	4
Total					80

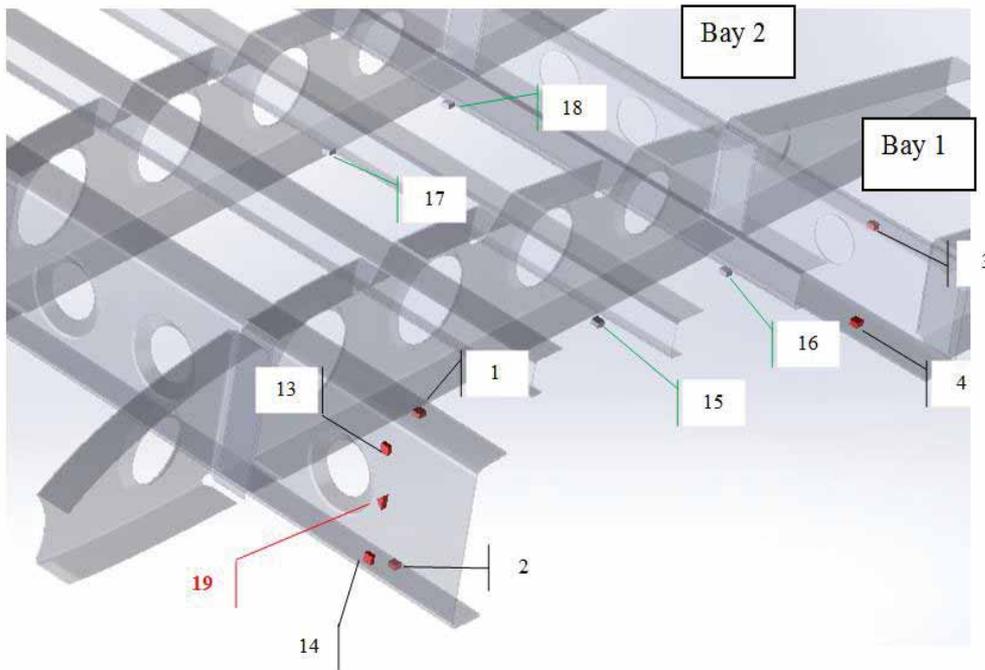
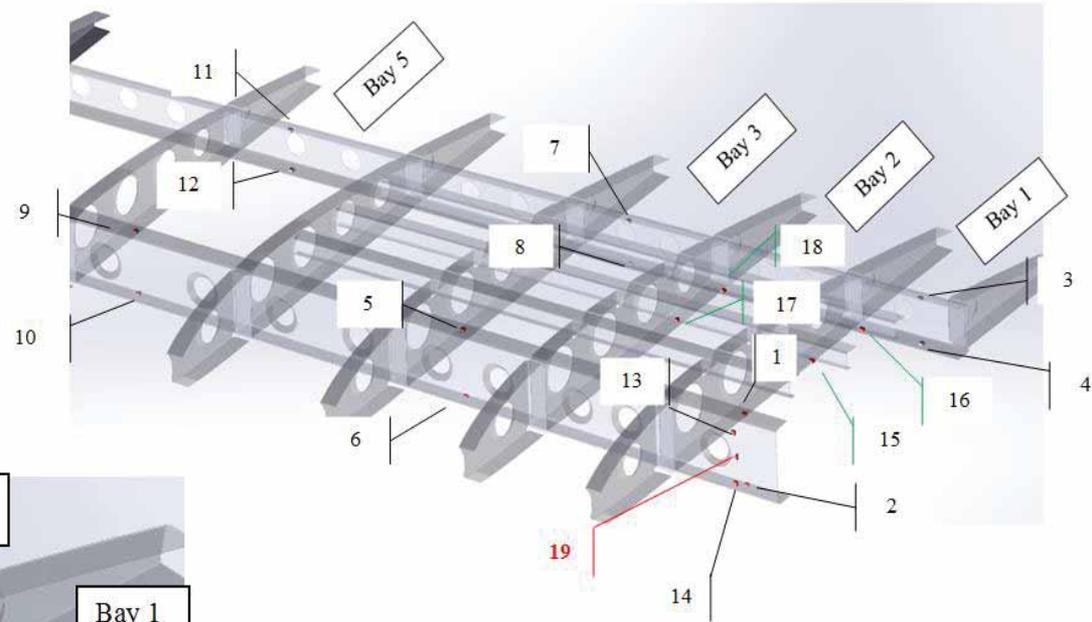


## Strain gauges

ID	Bay	POSITION	INSTALLATION	TYPE		
1	1	between rib1-rib2	front spar	UNIDIRECTIONAL	39.5	0.025
2	1	between rib1-rib2	front spar	UNIDIRECTIONAL	39.5	0.025
3	1	between rib1-rib2	rear spar	UNIDIRECTIONAL	170	0.106
4	1	between rib1-rib2	rear spar	UNIDIRECTIONAL	170	0.106
5	3	between rib3-rib4	front spar	UNIDIRECTIONAL	39.5	0.025
6	3	between rib3-rib4	front spar	UNIDIRECTIONAL	39.5	0.025
7	3	between rib3-rib4	rear spar	UNIDIRECTIONAL	170	0.106
8	3	between rib3-rib4	rear spar	UNIDIRECTIONAL	170	0.106
9	5	between rib5-rib6	front spar	UNIDIRECTIONAL	39.5	0.025
10	5	between rib5-rib6	front spar	UNIDIRECTIONAL	39.5	0.025
11	5	between rib5-rib6	rear spar	UNIDIRECTIONAL	170	0.106
12	5	between rib5-rib6	rear spar	UNIDIRECTIONAL	170	0.106
13	1	between rib1-rib2	front spar thickening	ROSETTE-3SIGNAL	39.5	0.025
14	1	between rib1-rib2	front spar thickening	ROSETTE-3SIGNAL	39.5	0.025
15	1	1stbay, between 1st and 2nd stringer	Skin	UNIDIRECTIONAL	39.5	0.025
16	1	1stbay, between 2nd and 3rd stringer	Skin	UNIDIRECTIONAL	39.5	0.025
17	2	2ndbay, between 1st and 2nd stringer	Skin	UNIDIRECTIONAL	170	0.106
18	2	2ndbay, between 2nd and 3rd stringer	Skin	UNIDIRECTIONAL	170	0.106
19	1	between rib1-rib2	front spar	ROSETTE-3SIGNAL	39.5	0.025



## Strain gauges

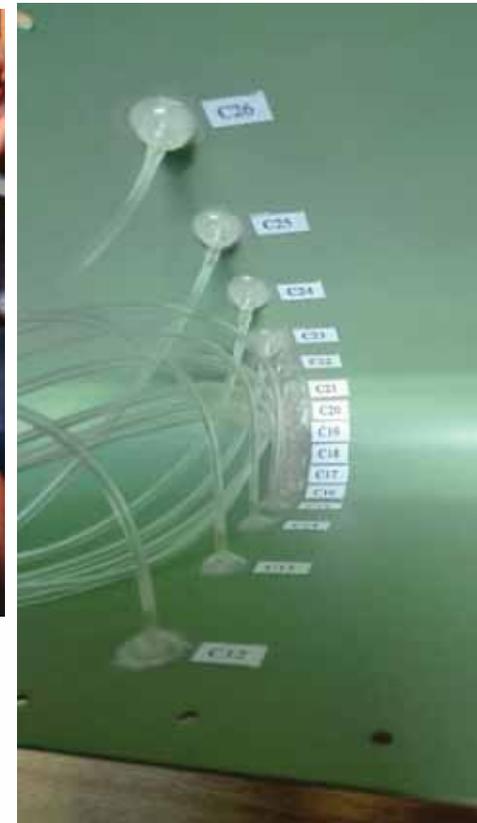
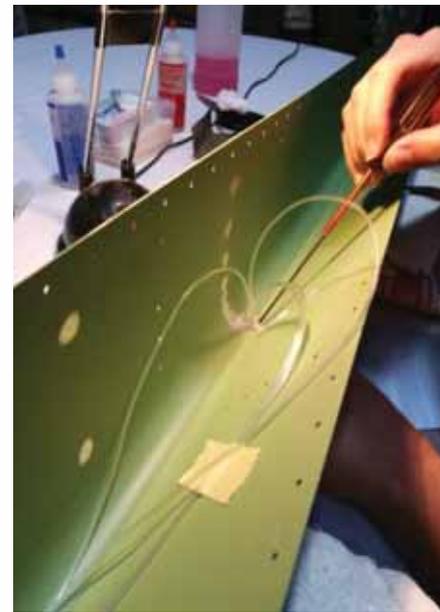


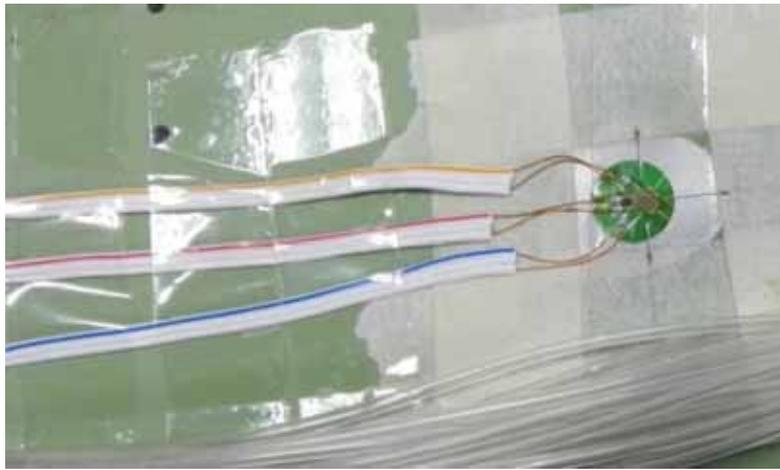










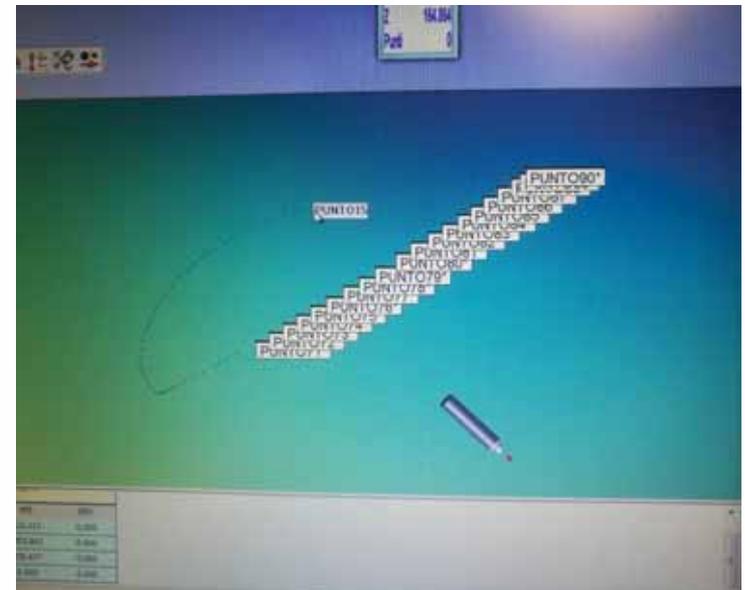
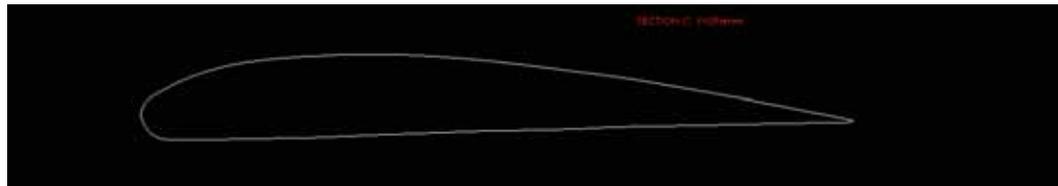


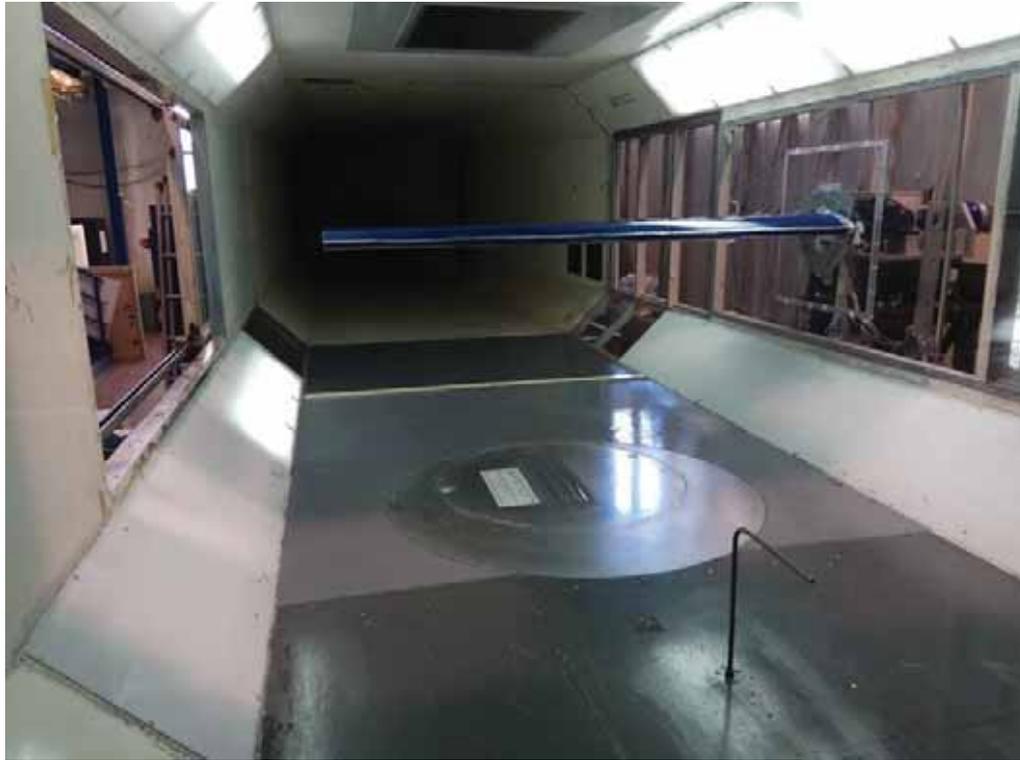






The model geometry has been also reconstructed through a **HEXAGON metrology electronic arm**





## UNINA Low-speed wind-tunnel facility

Type: *closed circuit-closed test section*

Test section dimensions : 2.0 m x 1.4 m

Maximum speed : about 160 Km/h (45 m/s)

Turbulence level : 0.1%

Temperature range : 10-50 °C

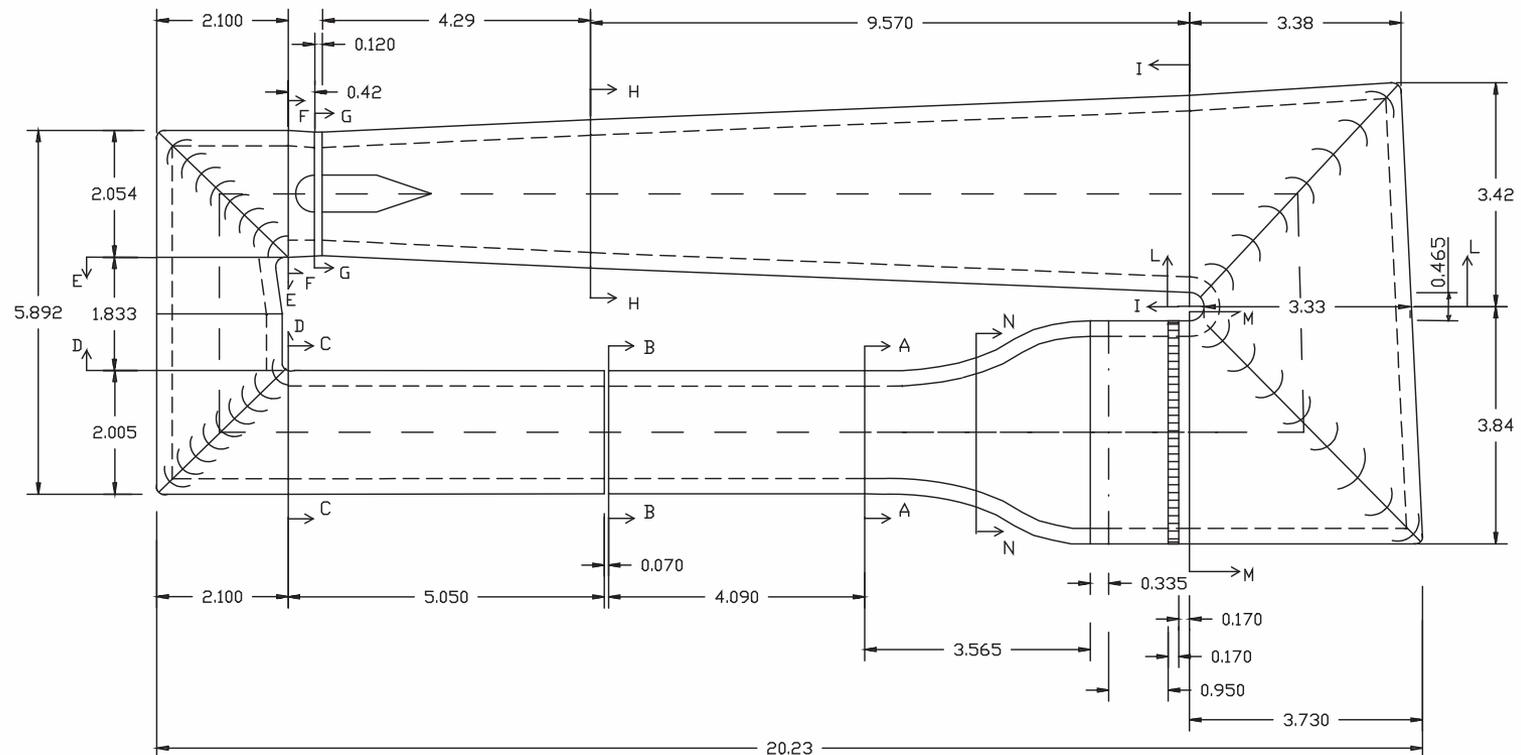
Speed range : 5-45 m/s

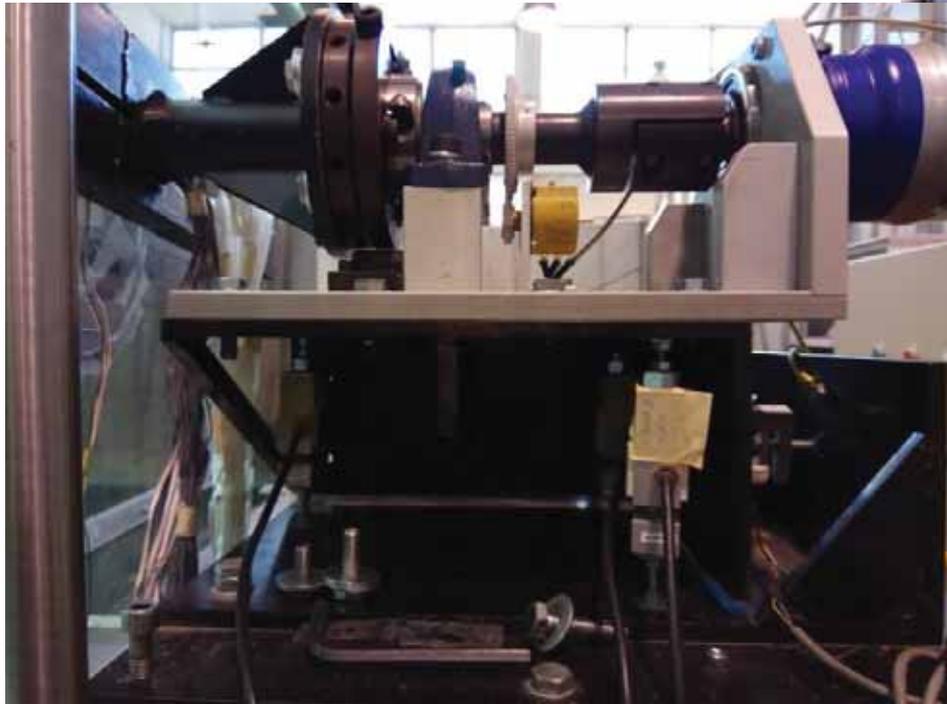
Reynolds number : 1 - 2 mil. For airfoil 2-D tests.

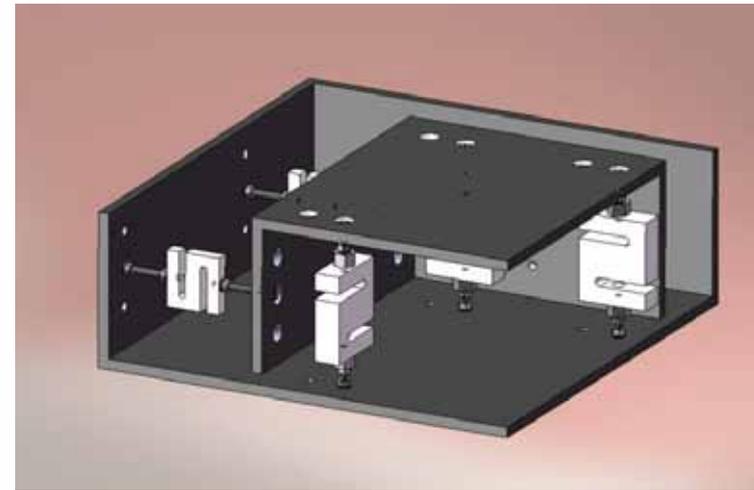
Usually about 0.9 – 1.0 mil. For 3D model tests (chord of about 0.25 m)

Dynamic Pressure : 15 – 1200 Pa

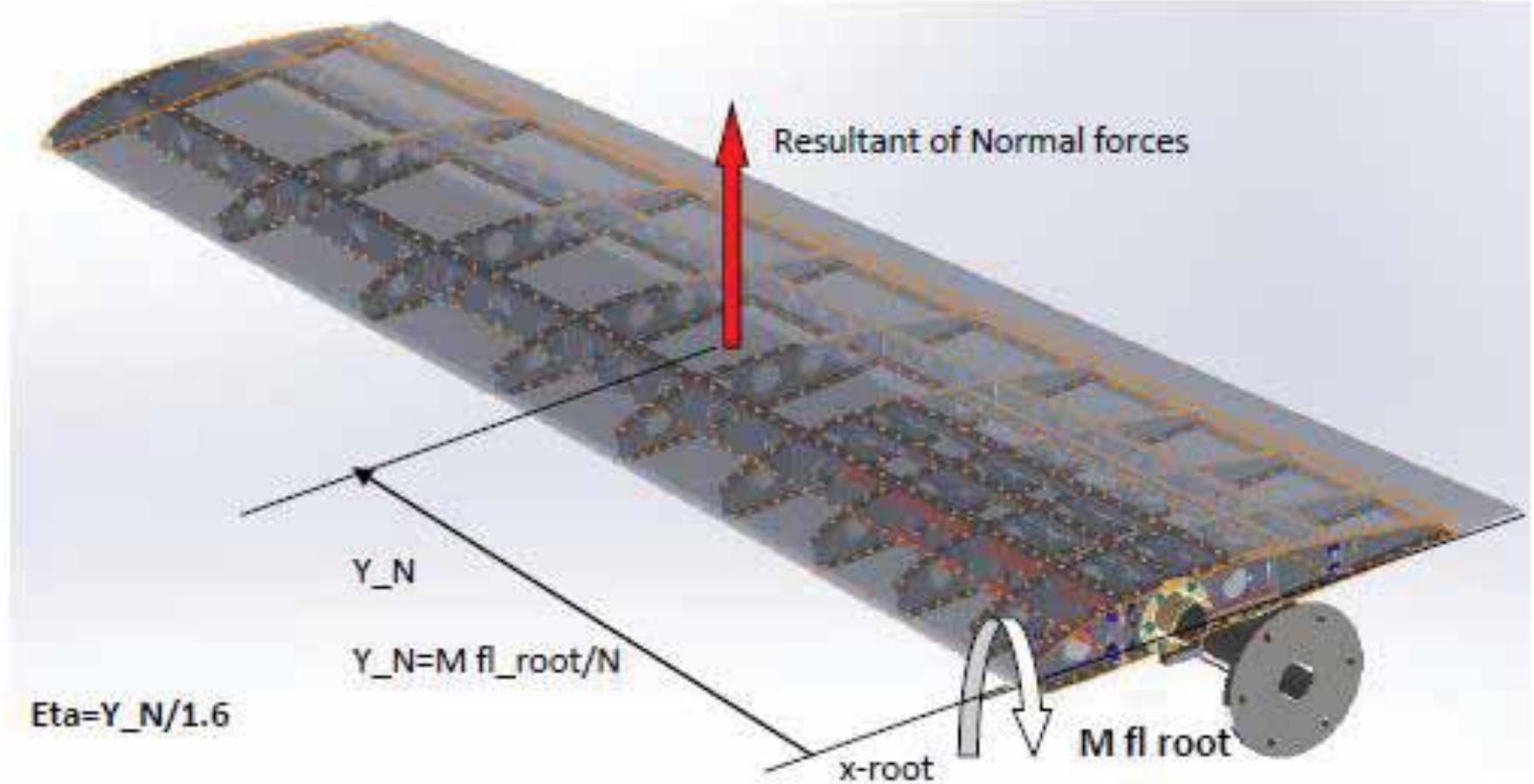
Stagnation pressure : Dyn press + ambient pressure  
(about 103500 Pa + q = 104700 Pa)





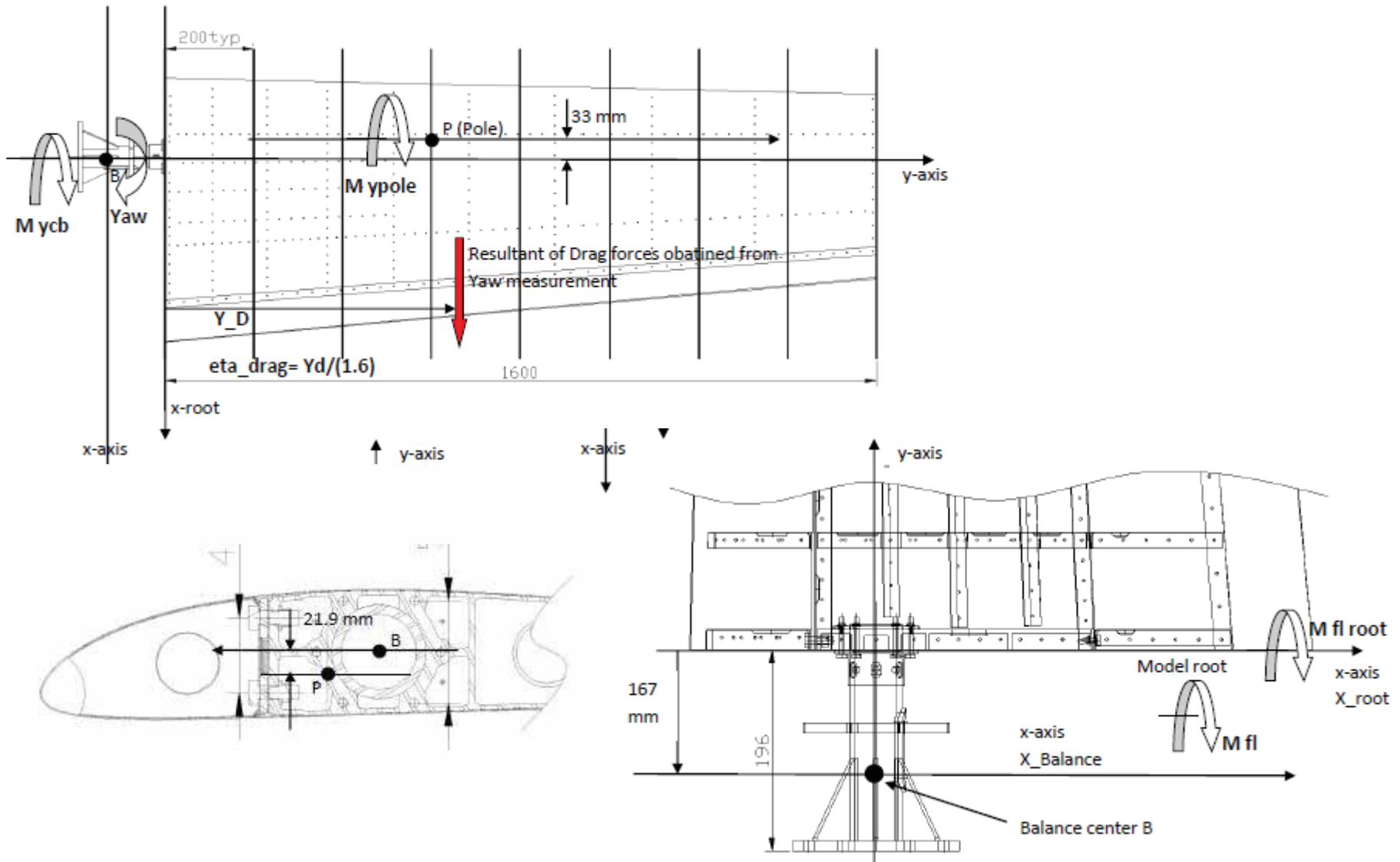


Component	Range		Accuracy
	Min	Max	
Normal force (Lift) L	-80 Kg	100 Kg	0.030 Kg
Horizontal force (Drag) D	-12 Kg	12 Kg	0.005 Kg
Pitching moment My	-15 Kg*m	15 Kg*m	0.010 Kg*m
Bending moment Mfl	-40 Kg*m	60 Kg*m	0.030 Kg*m
Yawing moment Myaw	-8 Kg*m	8 Kg*m	0.006 Kg*m



$S = 0.815 \text{ m}^2$  model reference area (planform area)

$c$  : model reference chord (mean aerodynamic chord,  $c = 0.5153 \text{ m}$ )





## Wind-Tunnel corrections

### Upwash and streamline curvature

$$\Delta\alpha = (1 + \tau_{2w}) \cdot \delta \cdot \left( \frac{S}{A_{wt}} \right) \cdot CL \quad \alpha_{cor} = \alpha_g + \Delta\alpha$$

$$\tau_{2w} = 0.18$$

$$\delta = 0.61$$

The correction is proportional to the developed lift and lift coefficient.

The correction to be applied is positive, it means that with a certain geometrical angle of attack, the effective corrected angle of attack will be slightly higher.

At an angle of attack of about  $6^\circ$  and a lift coefficient of about 0.80 ( $CL=0.80$ ), the correction is about  $1^\circ$ , it means that the effective angle of attack is  $7^\circ$ .

### Solid and wake blockage

Due to the model solid blockage, and due to the wake blockage the dynamic pressure around the model will be increased by a factor that in this case is around 1.013.

That means :

$$q_{cor}/q=1.013 \quad \text{or} \quad q/q_{cor}=0.987$$

$$CL_{cor}=CL \cdot (q/q_{cor})$$

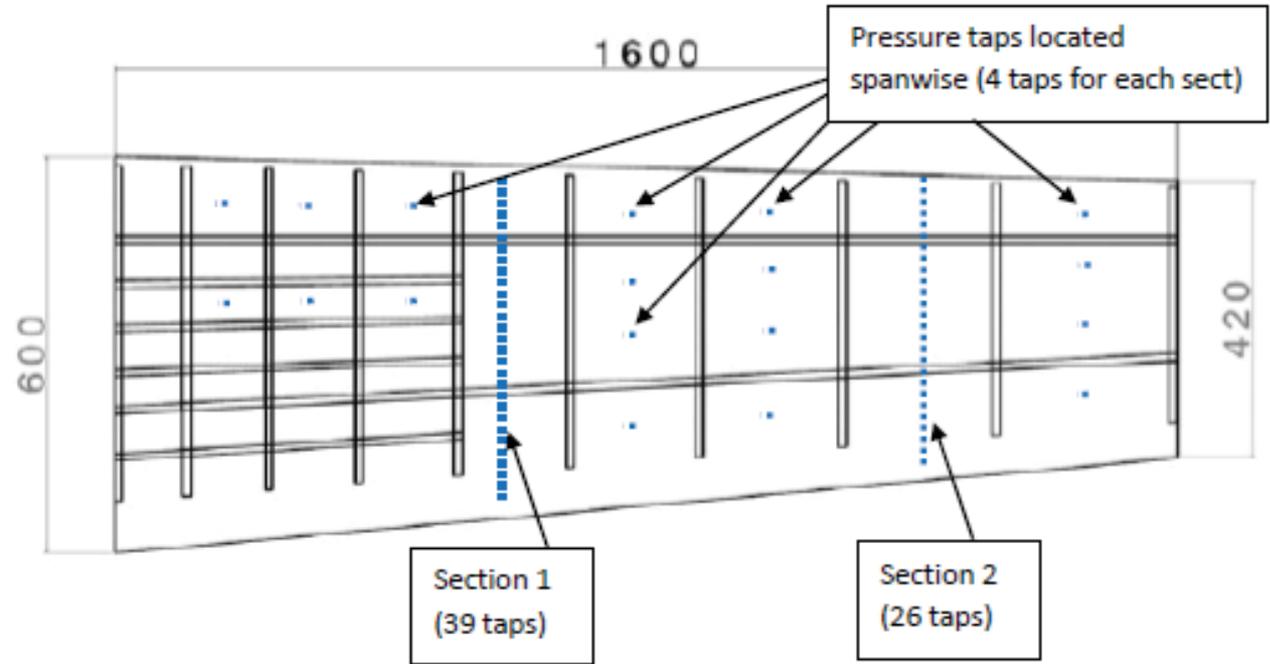
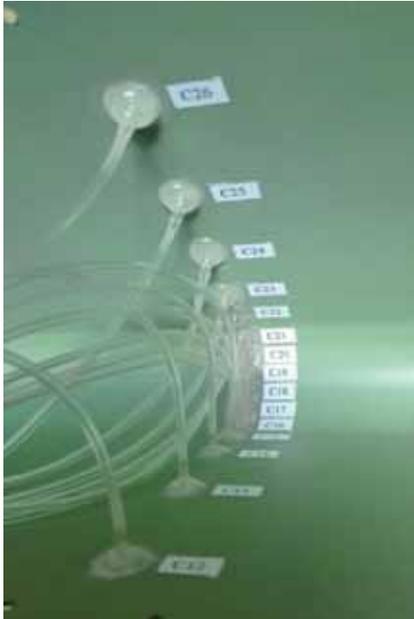
$$CD_{cor}=CD \cdot (q/q_{cor})$$

$$CM_{cor}=CM \cdot (q/q_{cor})$$

$$\Delta CD = \Delta\alpha \cdot CL - \Delta CD_{wake\_blockage}$$

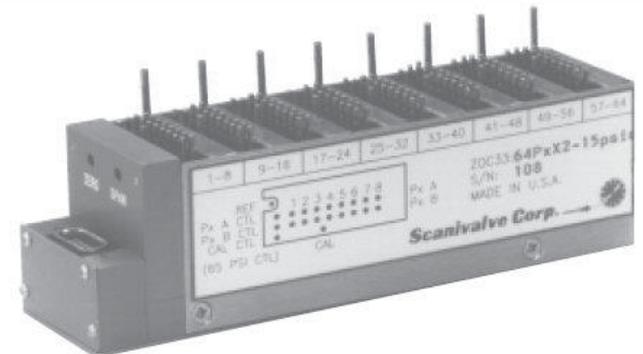
$$CD_{cor} = CD \cdot \left( \frac{q}{q_{cor}} \right) + \Delta\alpha \cdot CL - \Delta CD_{wake\_blockage}$$

## Pressure measurements



### SCANIVALVE 128 channel electronic pressure measurement system

- Accuracy (about 3 Pa)
- Very Fast
- Unsteady measurements



## TEST MATRIX PLANNED and COVERED

Name	flow speed	Reynolds	Measurements and Conditions
Oil	30 m/s	1.06 mill.	Flow vis with fluorescent oil at several a of att
<b><i>CLEAN Conditions</i></b>			
TEST L30	30 m/s	1.06 mill.	Full polar (up to stall) free transition L, D, M, Cp
TEST L35	35 m/s	1.25 mill.	(Up to 10°) polar free trans. L, D, M, Cp
TEST L40	40 m/s	1.43 mill.	Limited (up to 8°) polar free trans. L, D, M, Cp
<b><i>TURBULENT Conditions(b.l. tripped at l.e)</i></b>			
TEST 7/8/13	35 m/s	1.06	Tests at 35 m/s and repeatability check (L,D,M)
TEST T30	30 m/s	1.06 mill.	Full polar fixed trans 1-2% L, D, M, Cp, strain
TEST T35	35 m/s	1.25 mill.	Full polar fixed trans 1-2% L, D, M, Cp, strain
TEST T40	40 m/s	1.43 mill.	Limited polar fixed trans 1-2% L, D, M, Cp, strain
TEST F28	Var speed	Var	$\alpha=4^\circ$ & $6^\circ$ fixed trans 1-2% L, D, M, Cp, strain

## Model deformation measurement through LASER

TEST Da6	40 m/s	1.43 mill.	$\alpha=6^\circ$ , L=60.3Kgf fixed trans 1-2% L, D, M, strain, Model deformation
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## TEST RESULTS, FLUORESCENT OIL VISUALIZATION

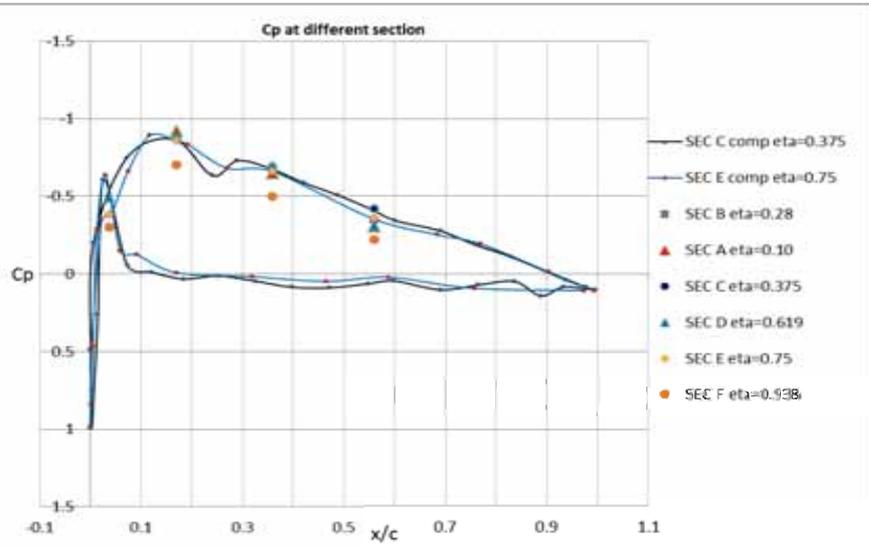
The clean model installed in the wind-tunnel has been covered with some fluorescent oil in several section along the span.

Some paper strip has been placed close to station C ( $y=600$  mm) and station E ( $y=1200$  mm) to highlight with pictures the accurate measurement of the position of the laminar separation bubble, both in terms of curvilinear abscissa (in [mm]) and in terms of fraction of local chord.



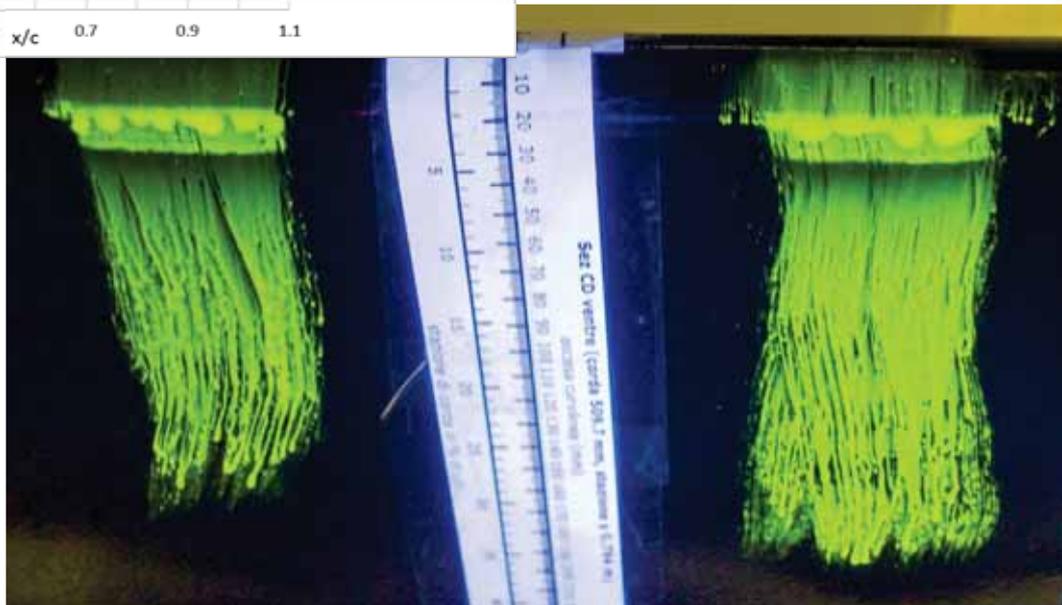
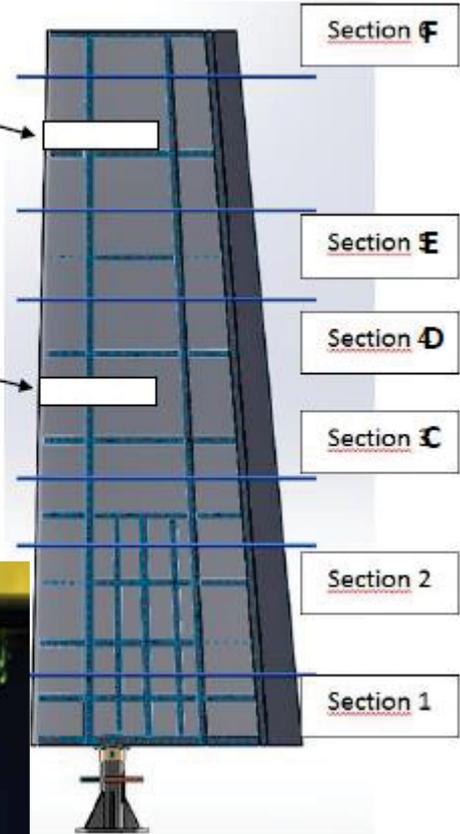
# TEST RESULTS, FLUORESCENT OIL VISUALIZATION

Alpha (geometrical) = 2°, V=30 m/s

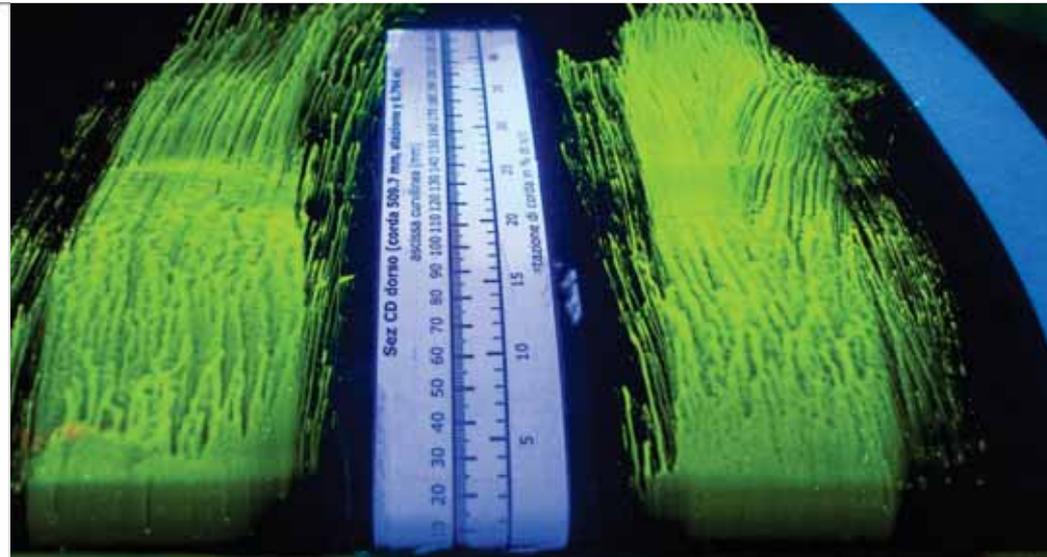
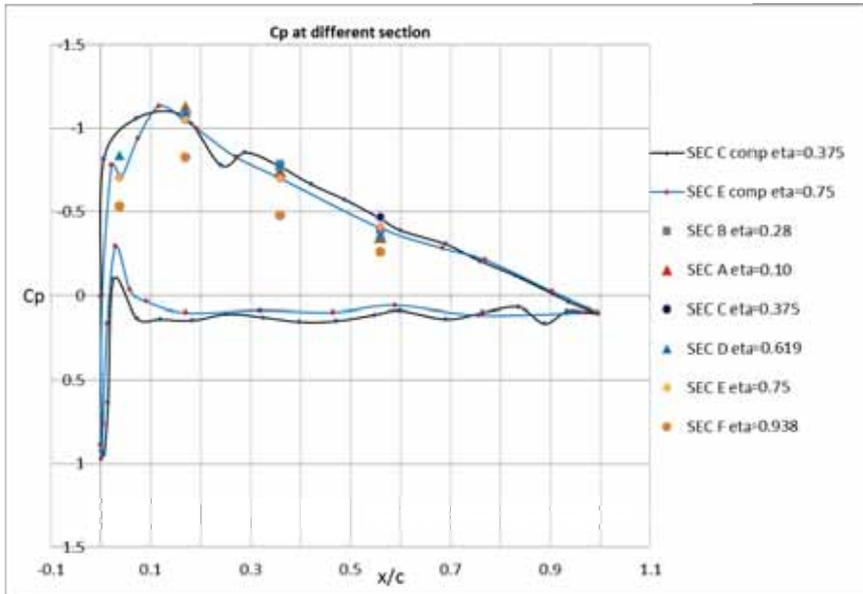


Paper indication placed between section E and section F

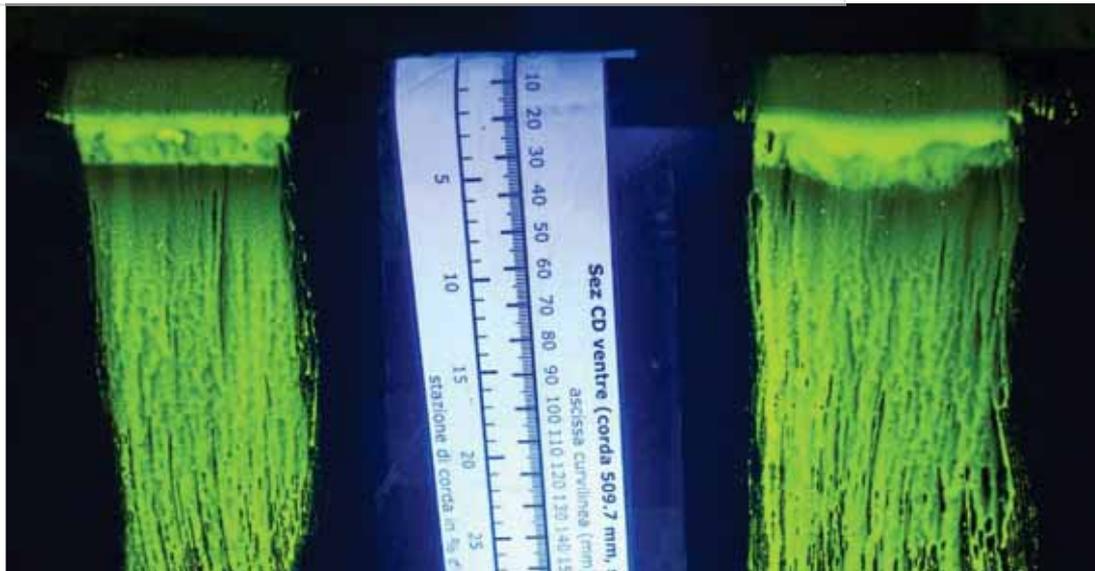
Paper indication placed between section C and section D



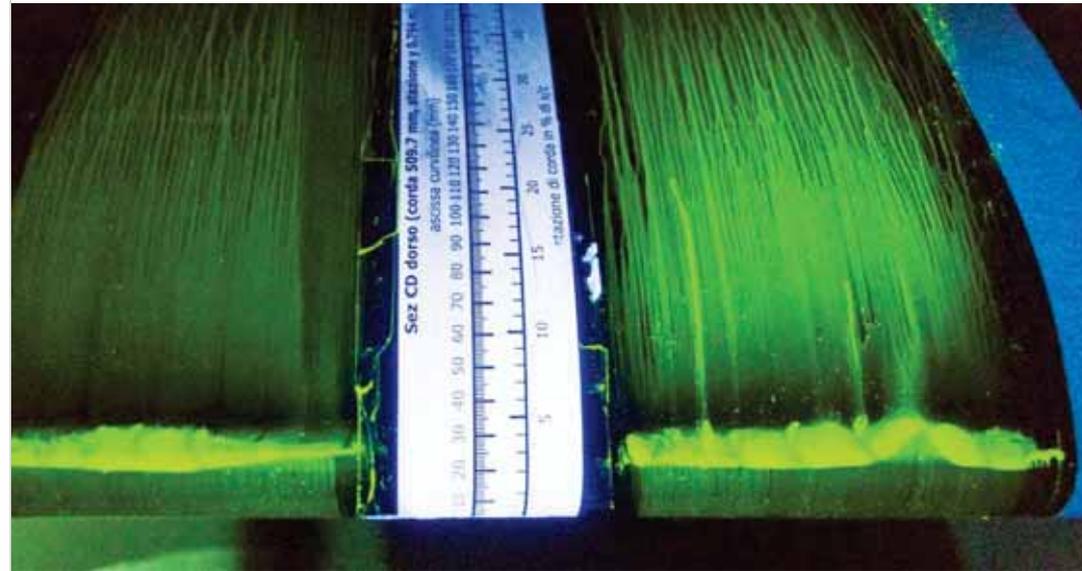
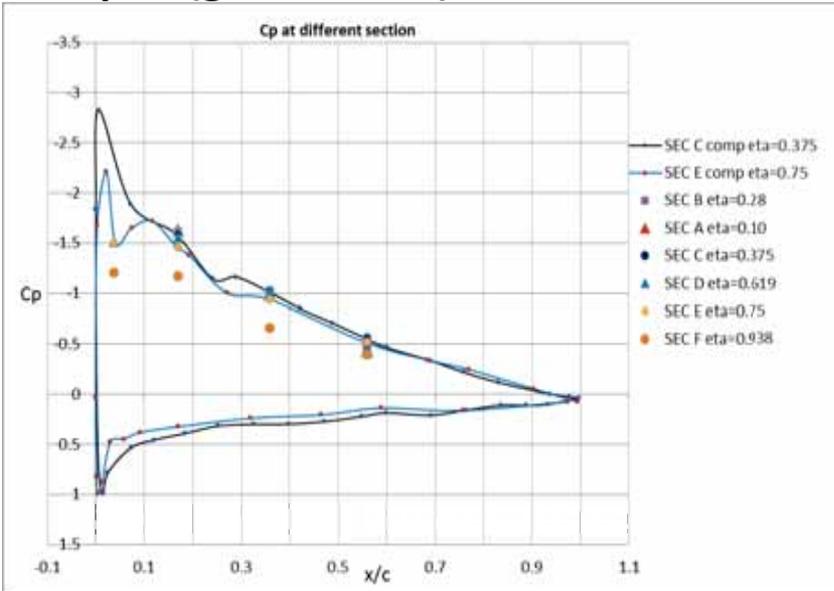
Alpha (geometrical) = 4°, V=30 m/s



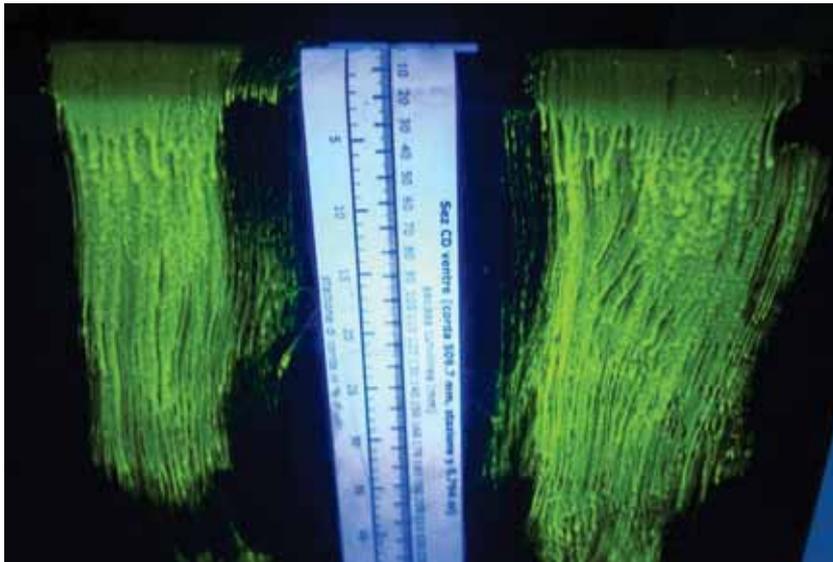
SECTION CD , upper surface



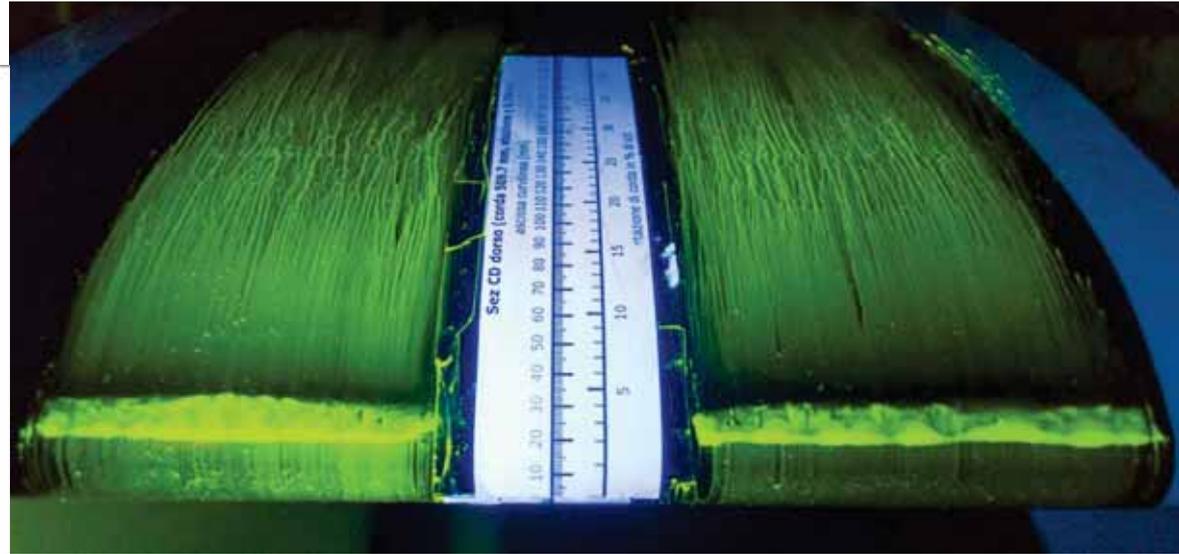
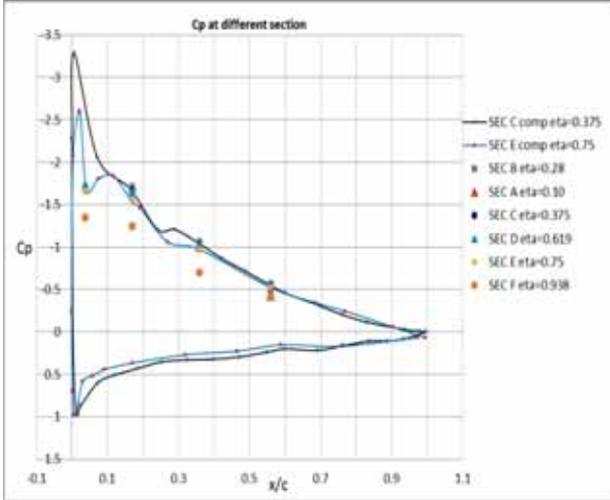
**Alpha (geometrical) = 8°, V=30 m/s**



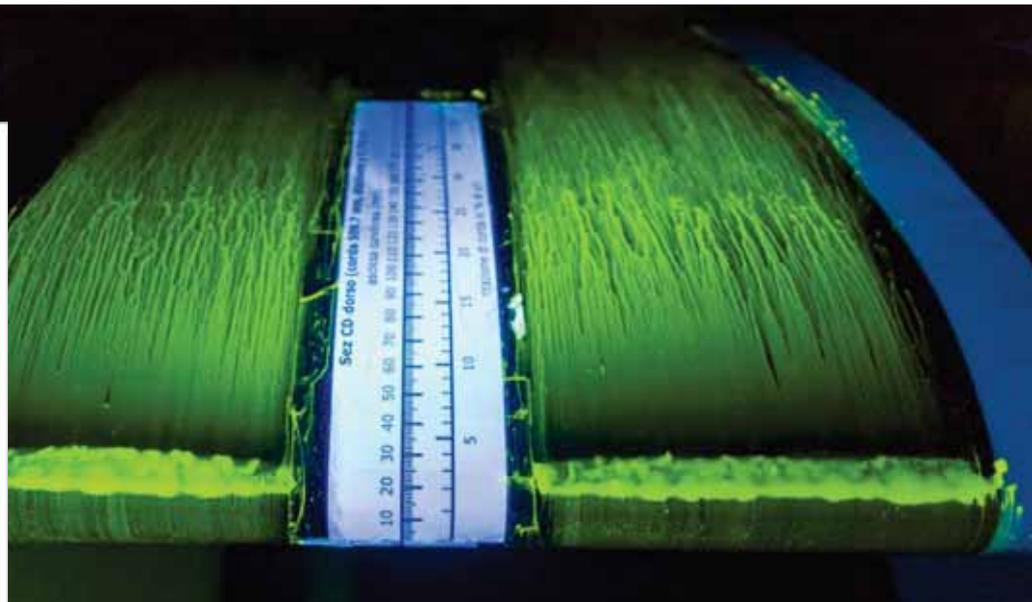
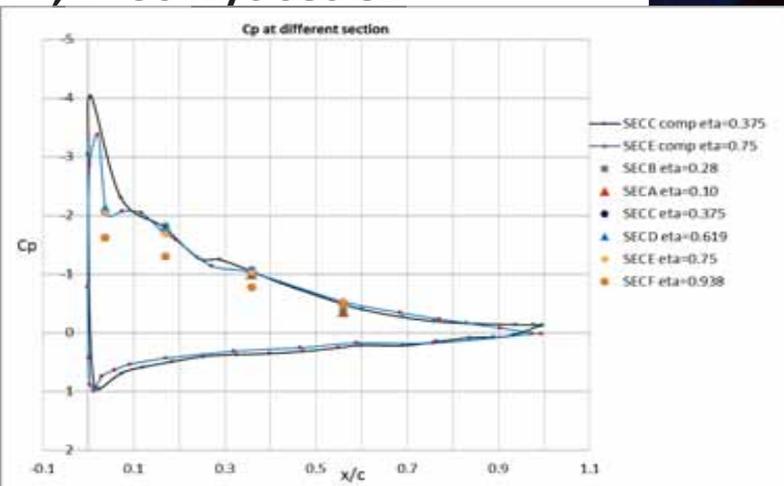
**SECTION CD , upper surface**



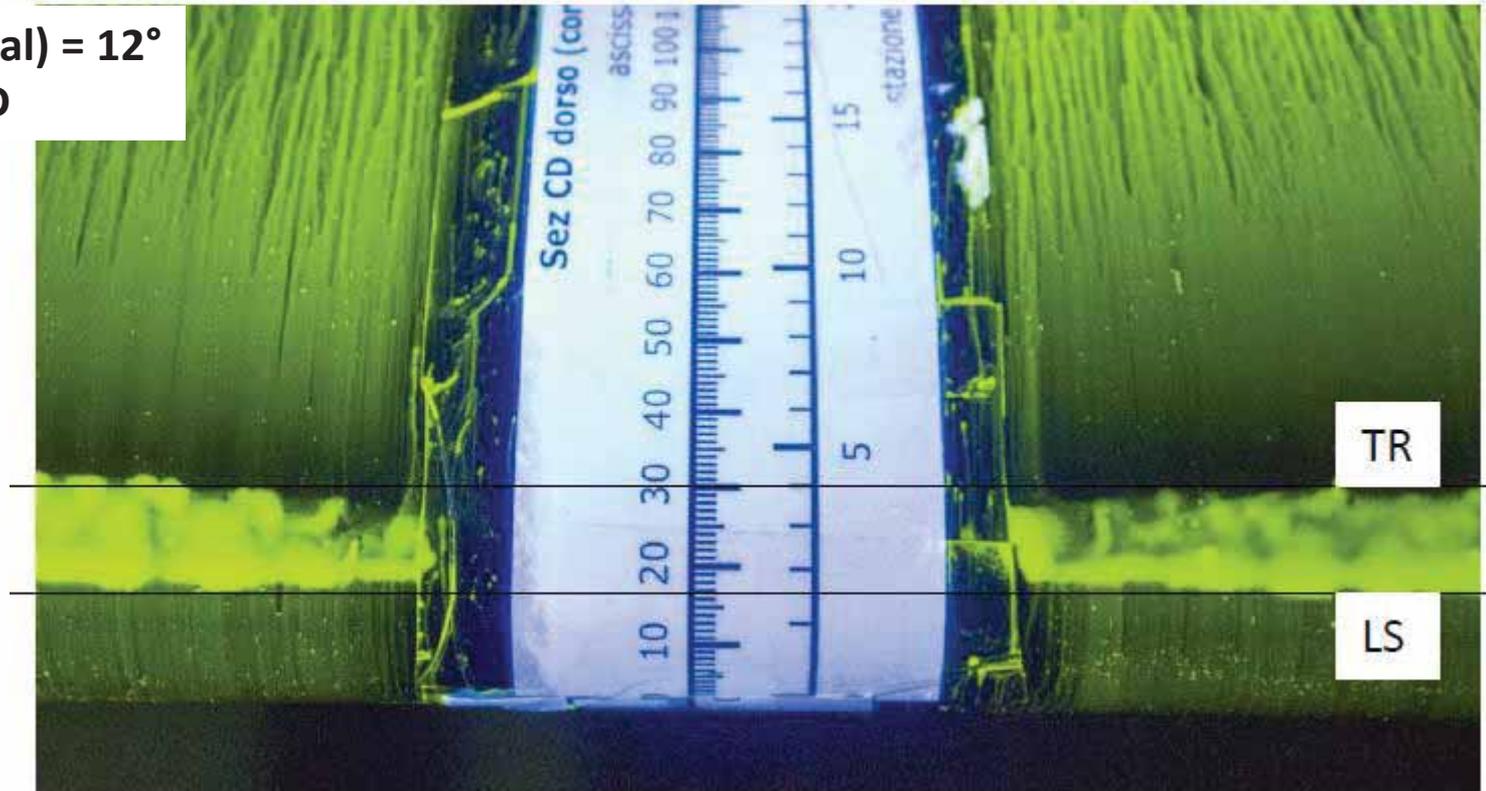
**Alpha (geometrical) = 10°  
, V=30 m/s sec CD**



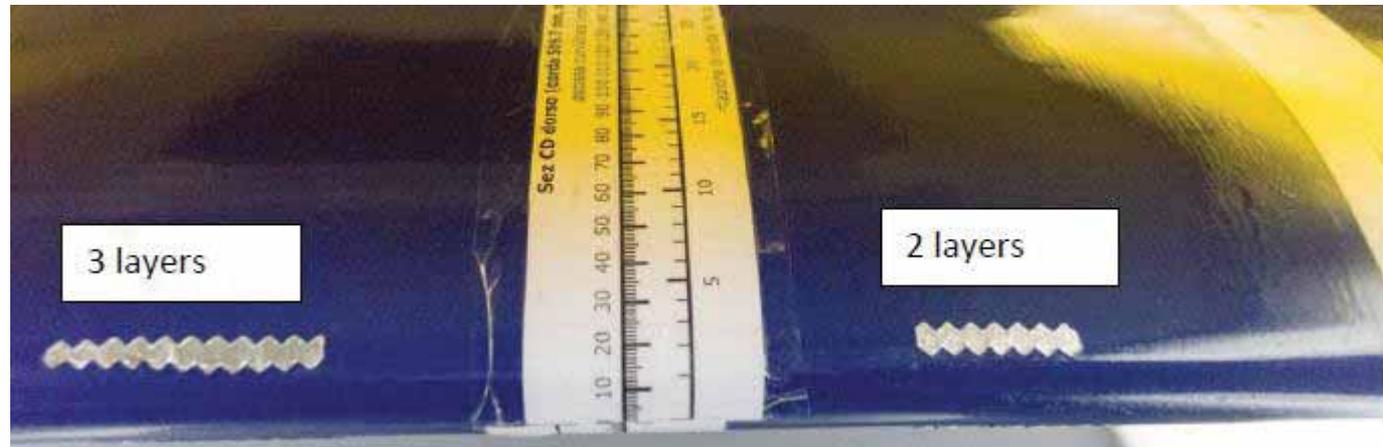
**Alpha (geometrical) = 12°  
, V=30 m/s sec CD**



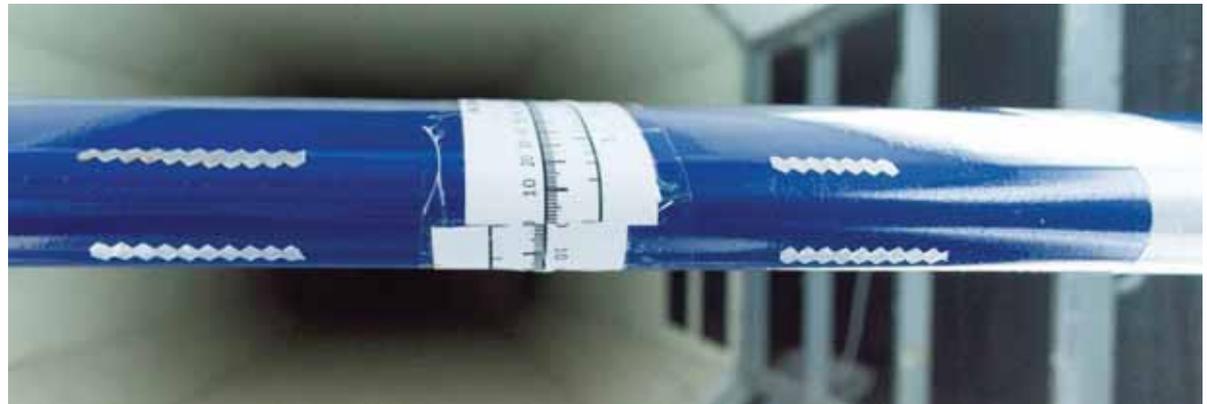
**Alpha (geometrical) = 12°  
, V=30 m/s sec CD**



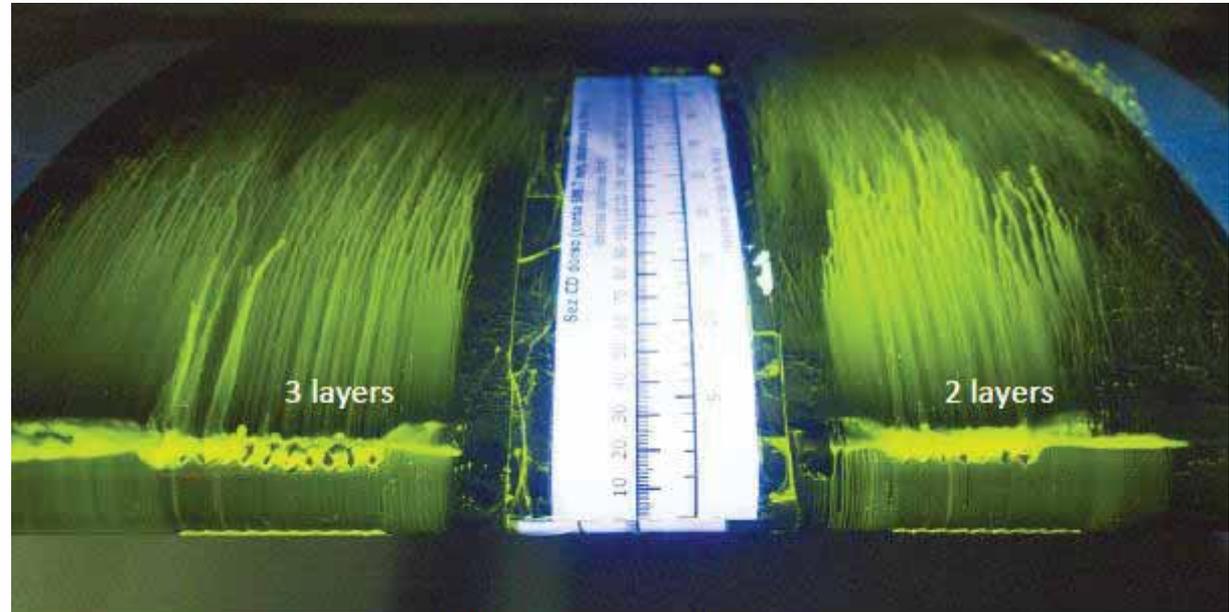
	s [mm]	x/c (local fraction of chord)
LS (Laminar separation) :	17 mm	0.016 (1.6%)
TR (Turbulent reattachment)	30 mm	0.040 (4%)



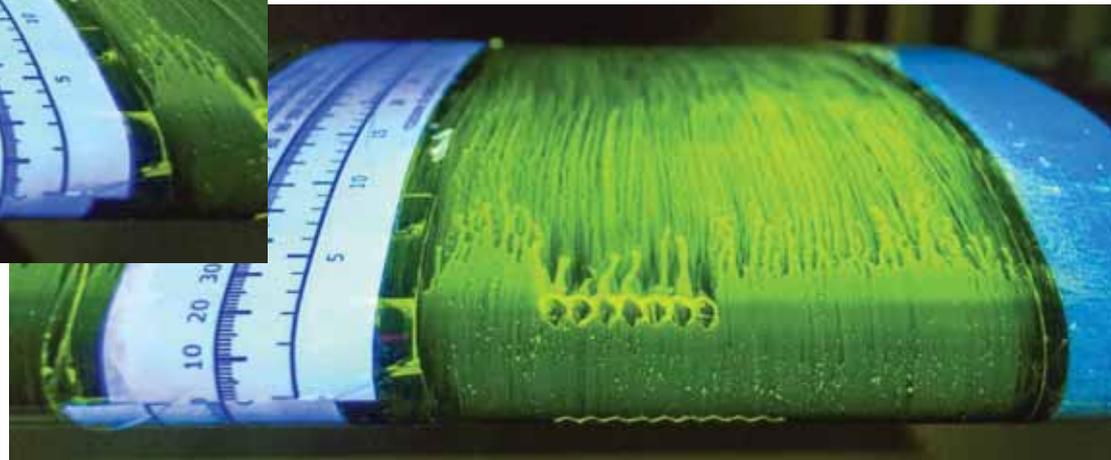
2 layers, about 0.4 mm  
3 layers, about 0.6 mm

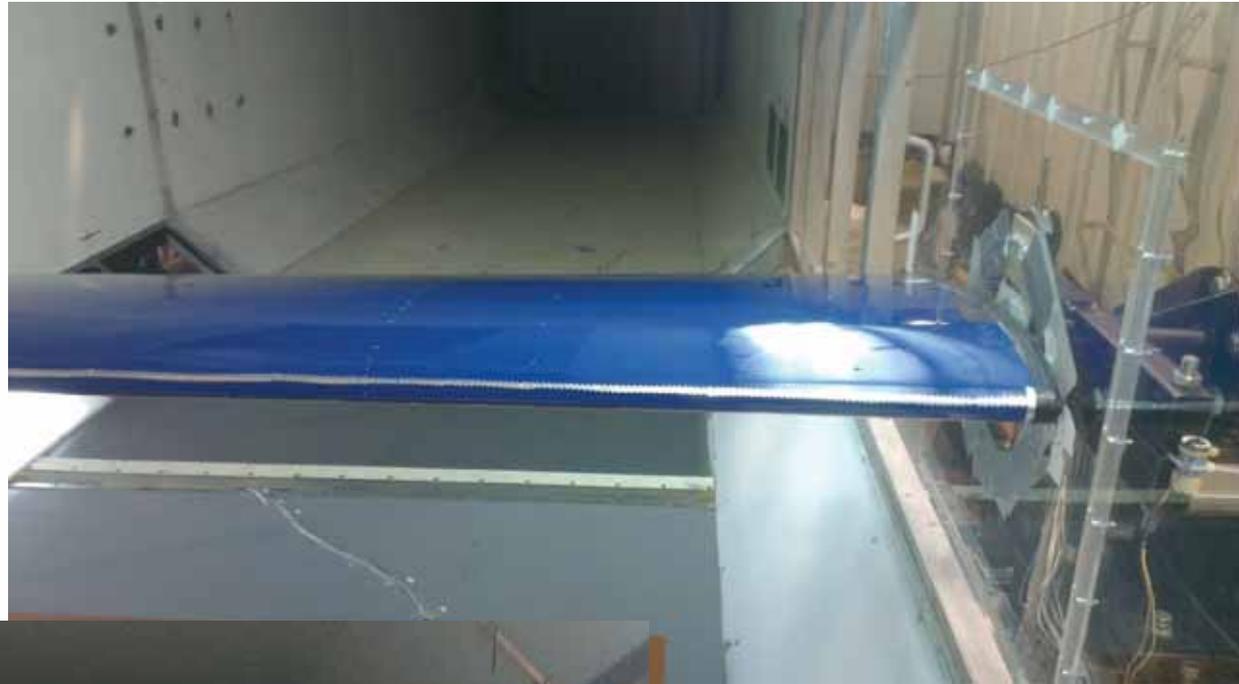


## 3 Layers is better

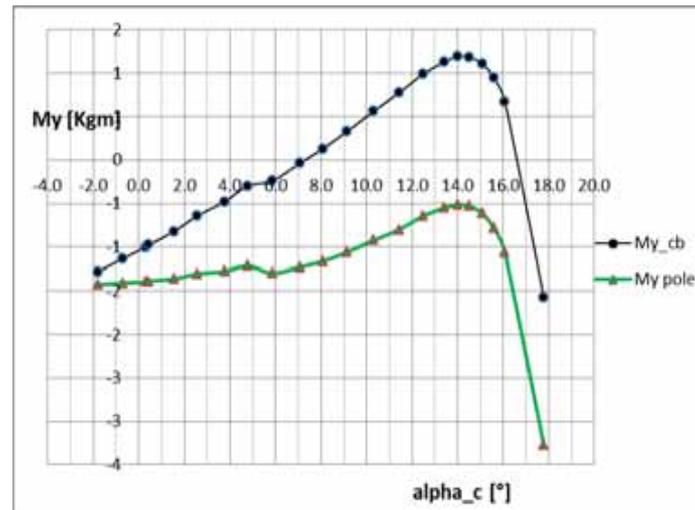
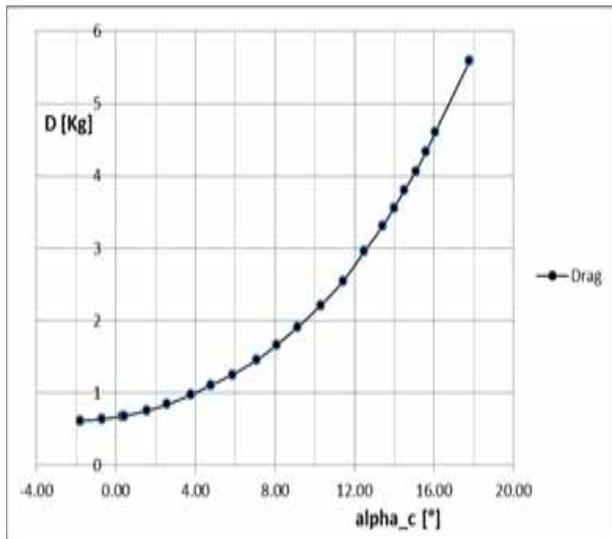
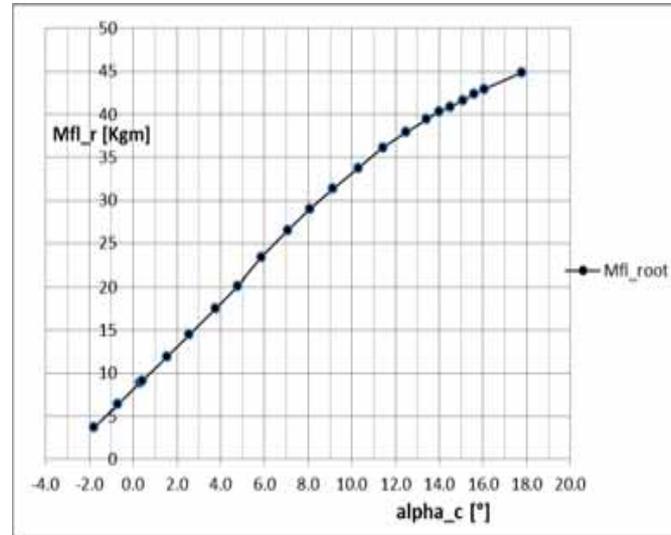
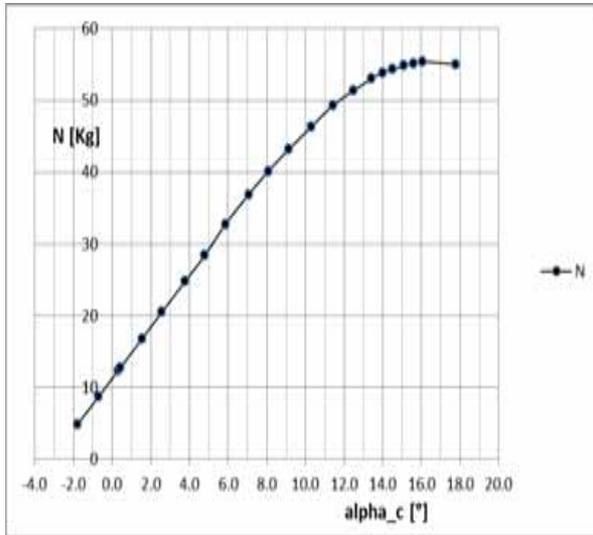


Alpha=12°, section CD

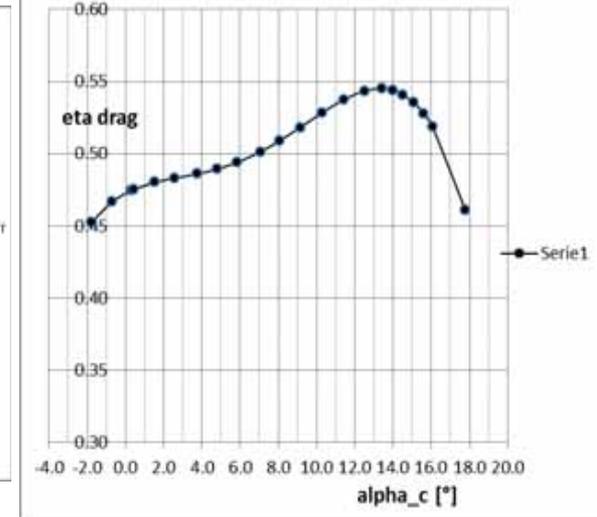
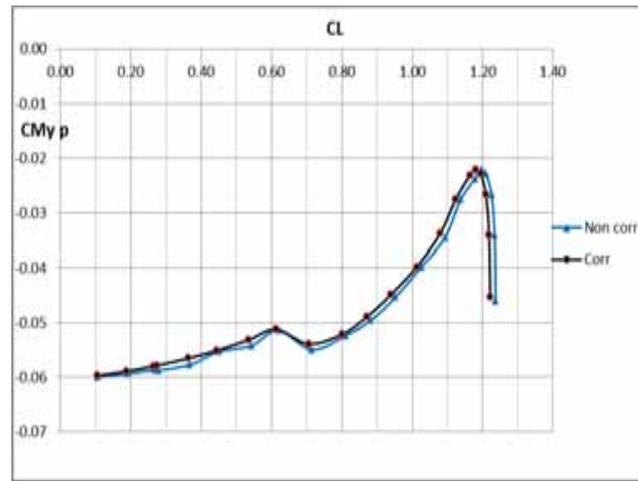
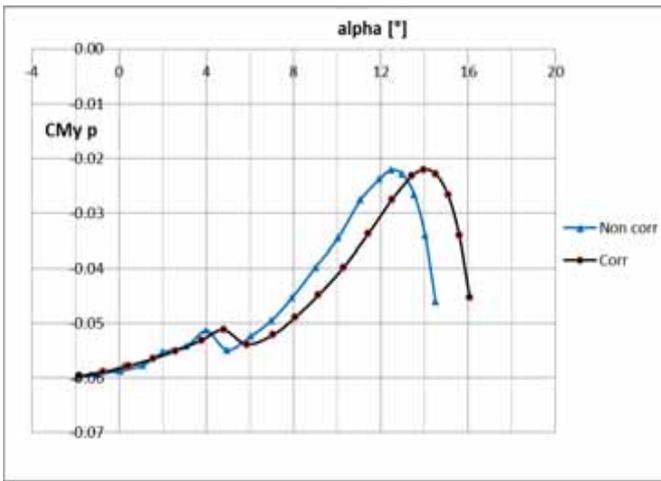
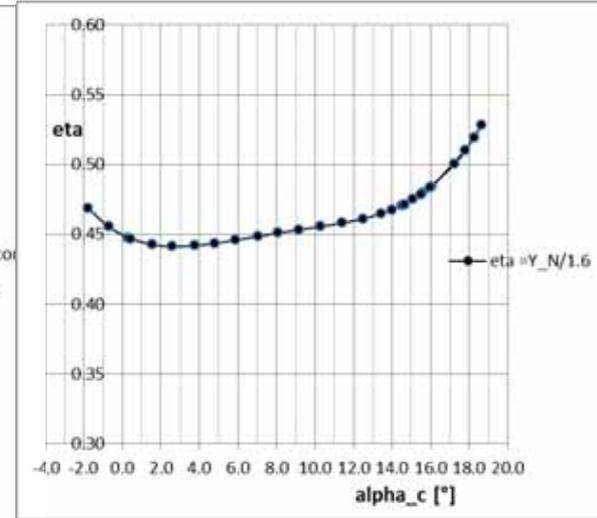
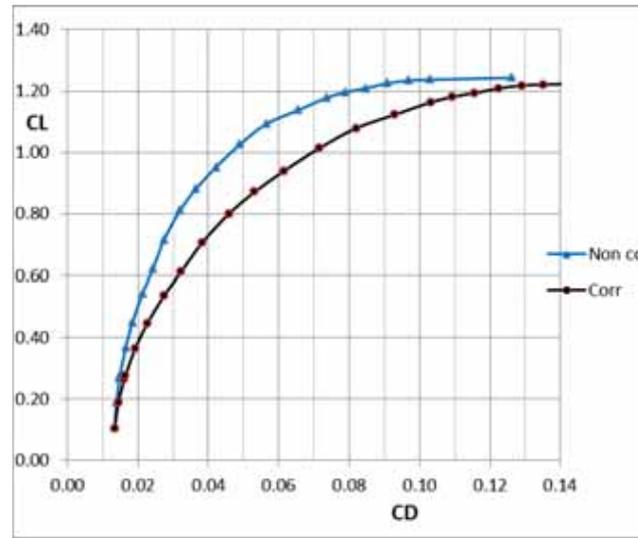
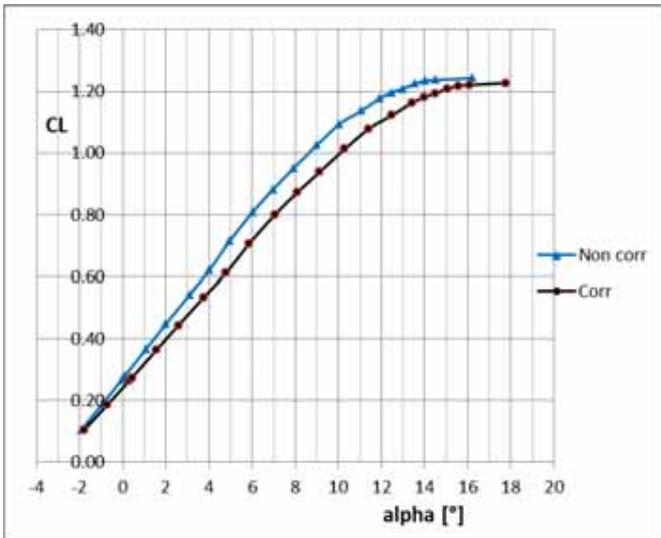




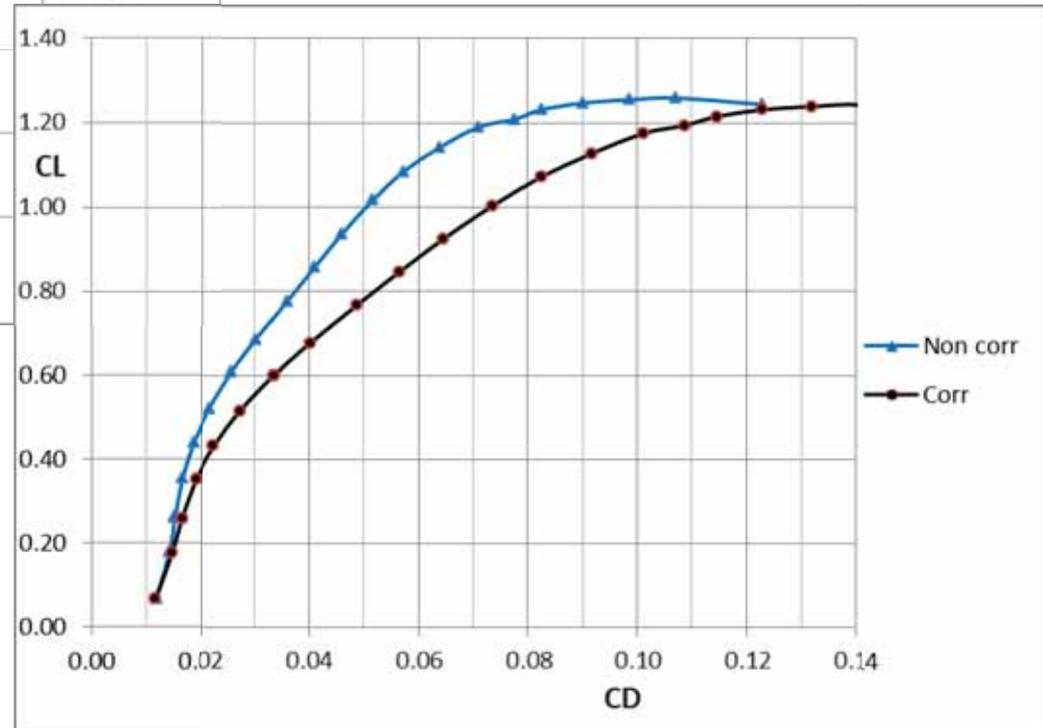
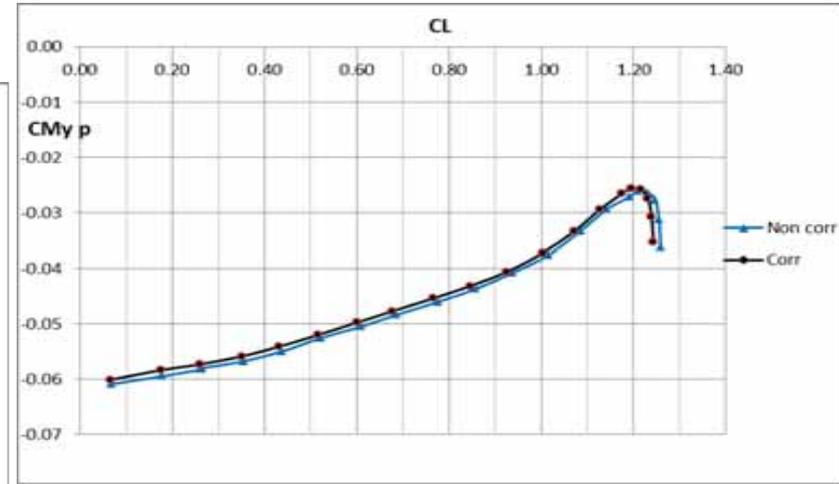
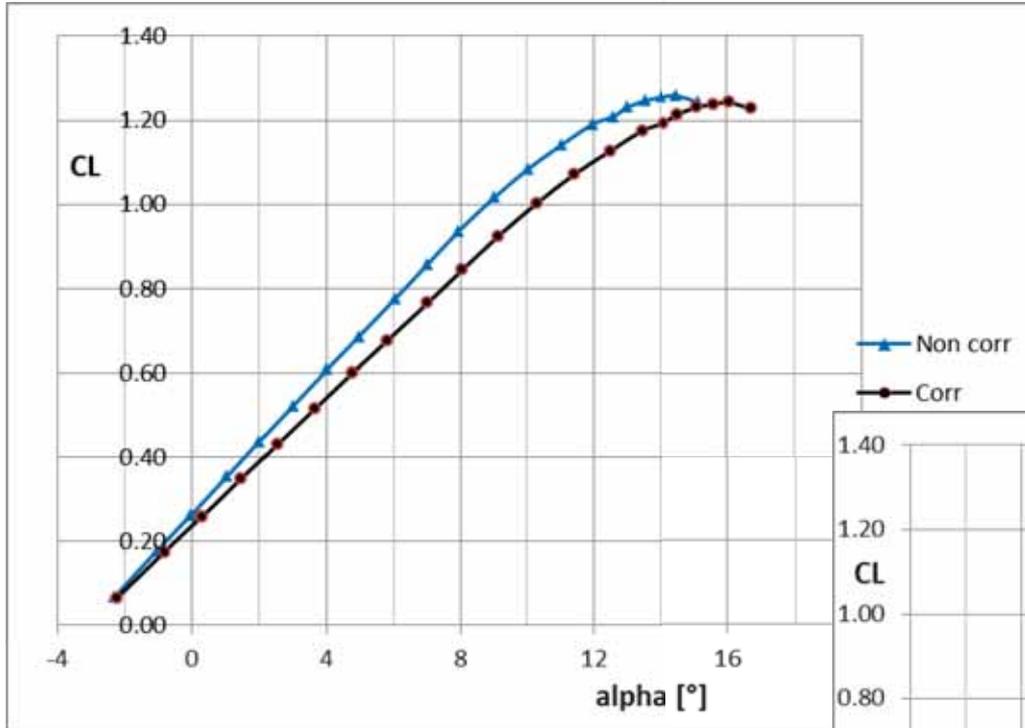
## TEST L30, V=30 m/s Clean Model , Forces and Moments



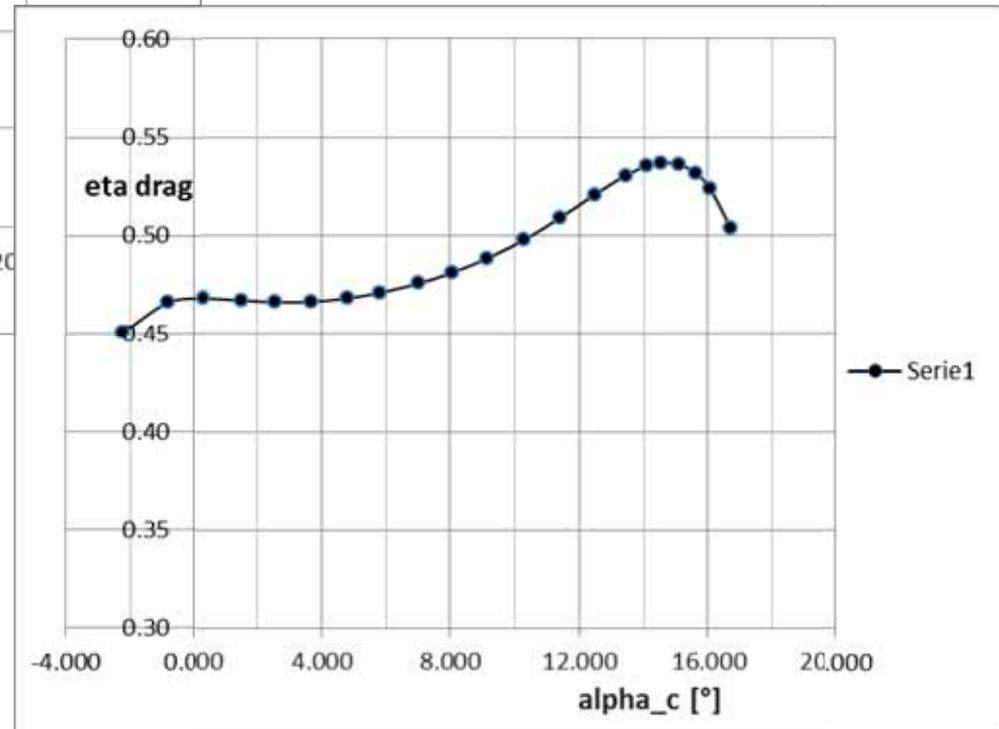
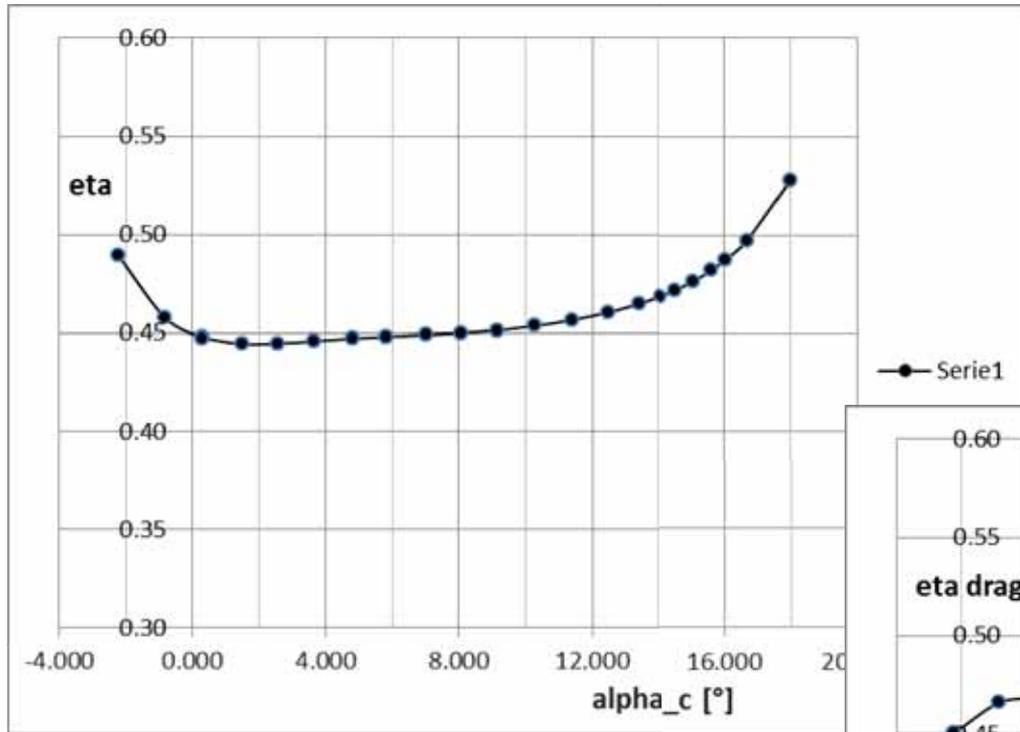
## TEST L30, $V=30$ m/s Clean Model, corrected and non-corrected coefficients



## TEST T30, V=30 m/s Turbulent b.l.

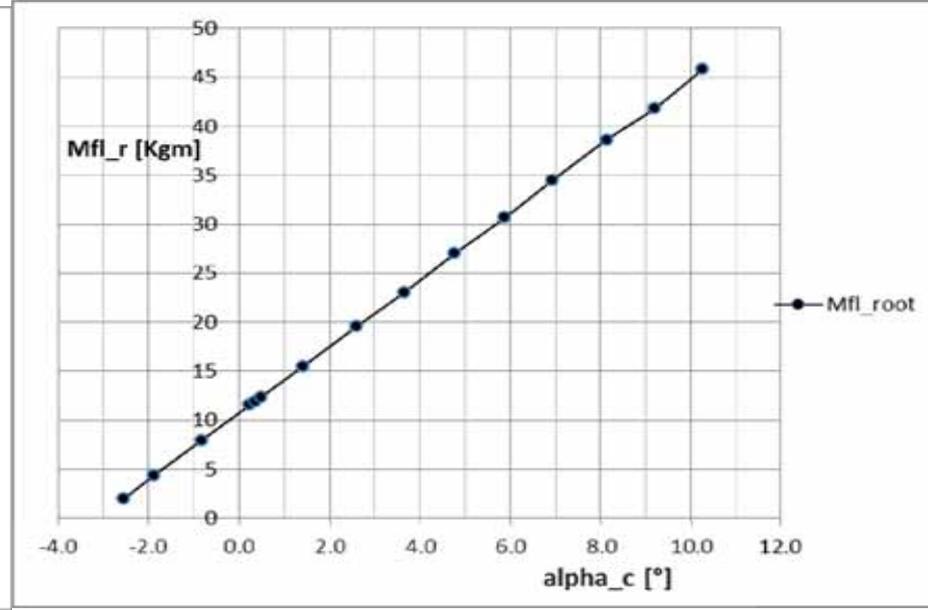
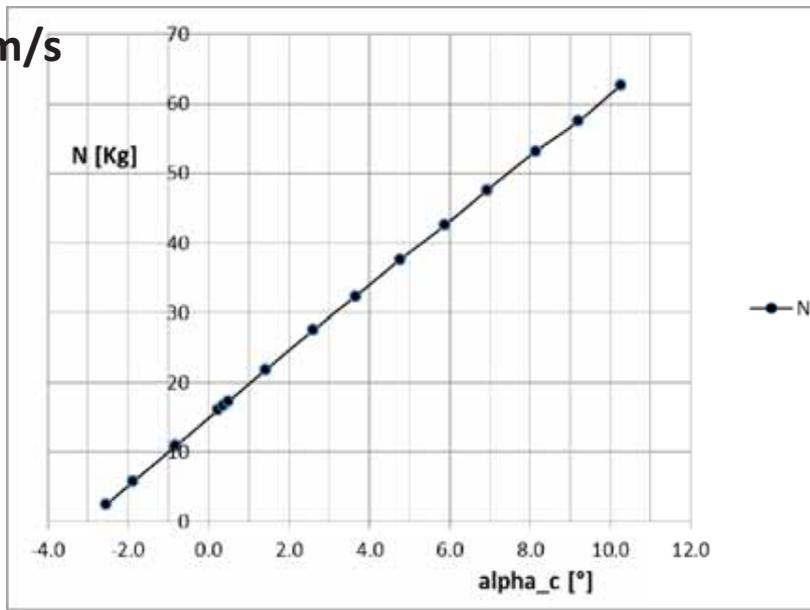


## TEST T30, V=30 m/s Turbulent b.l.

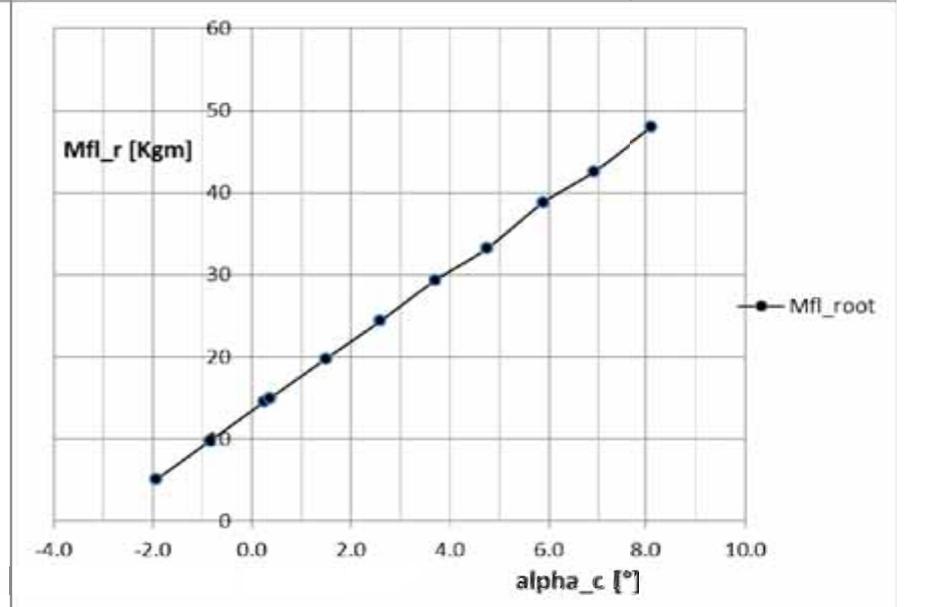
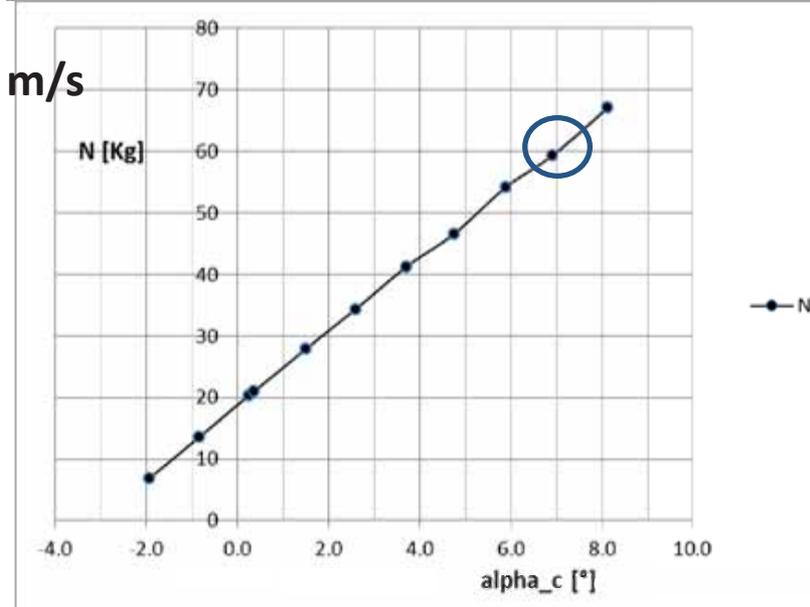


## TEST T35 and T40 Turbulent b.l. LOADS CONDITIONS

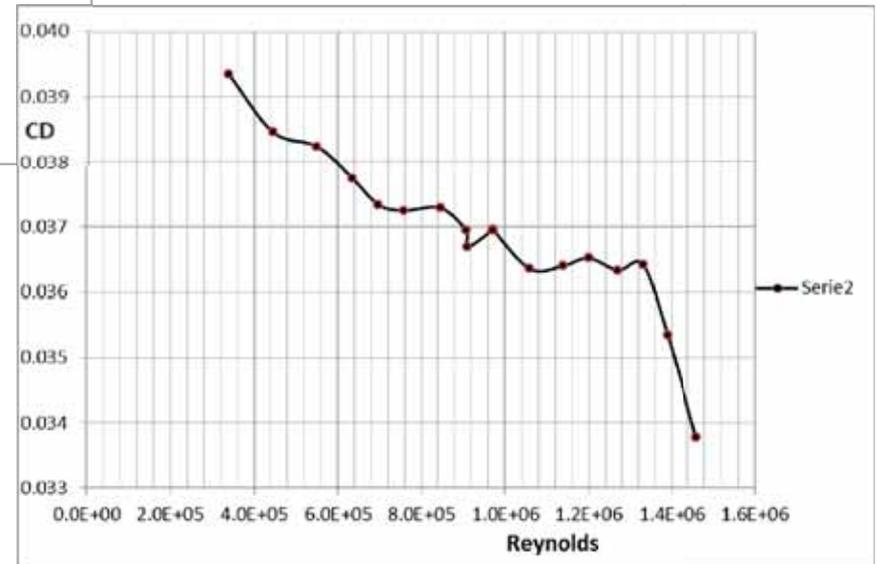
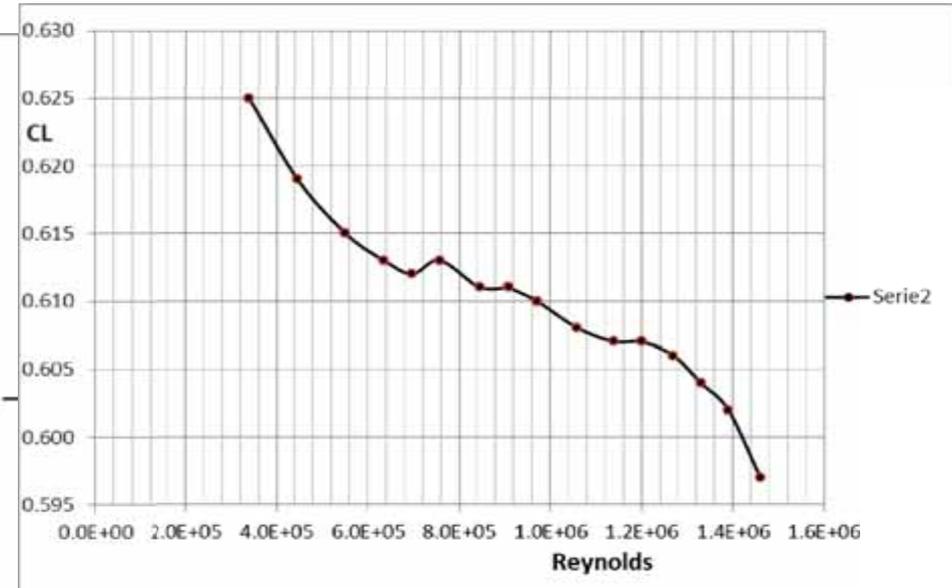
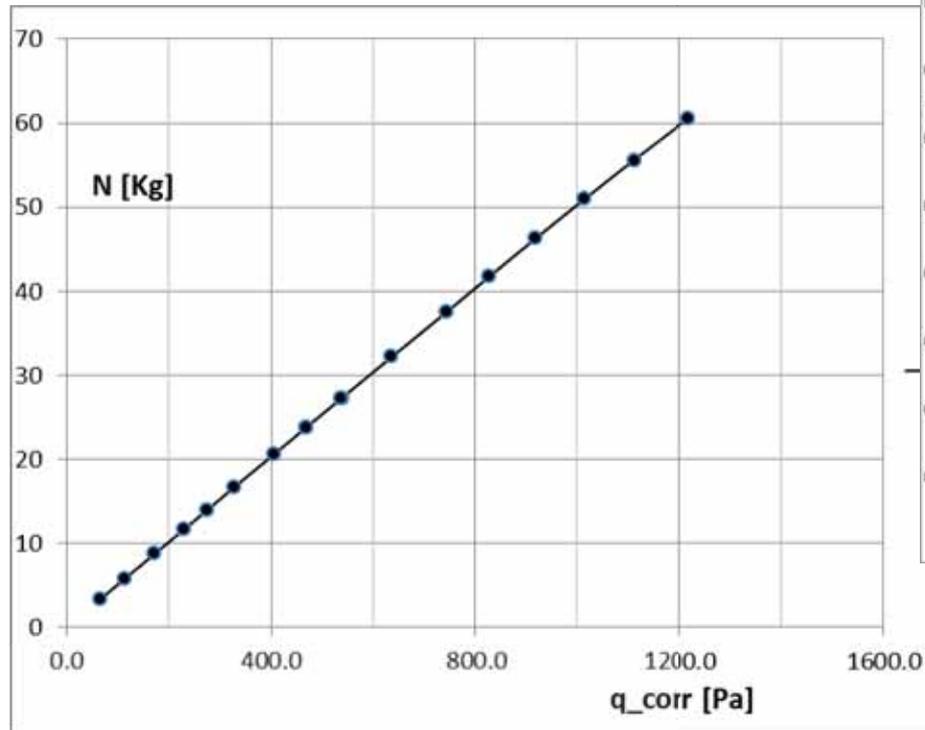
V=35 m/s



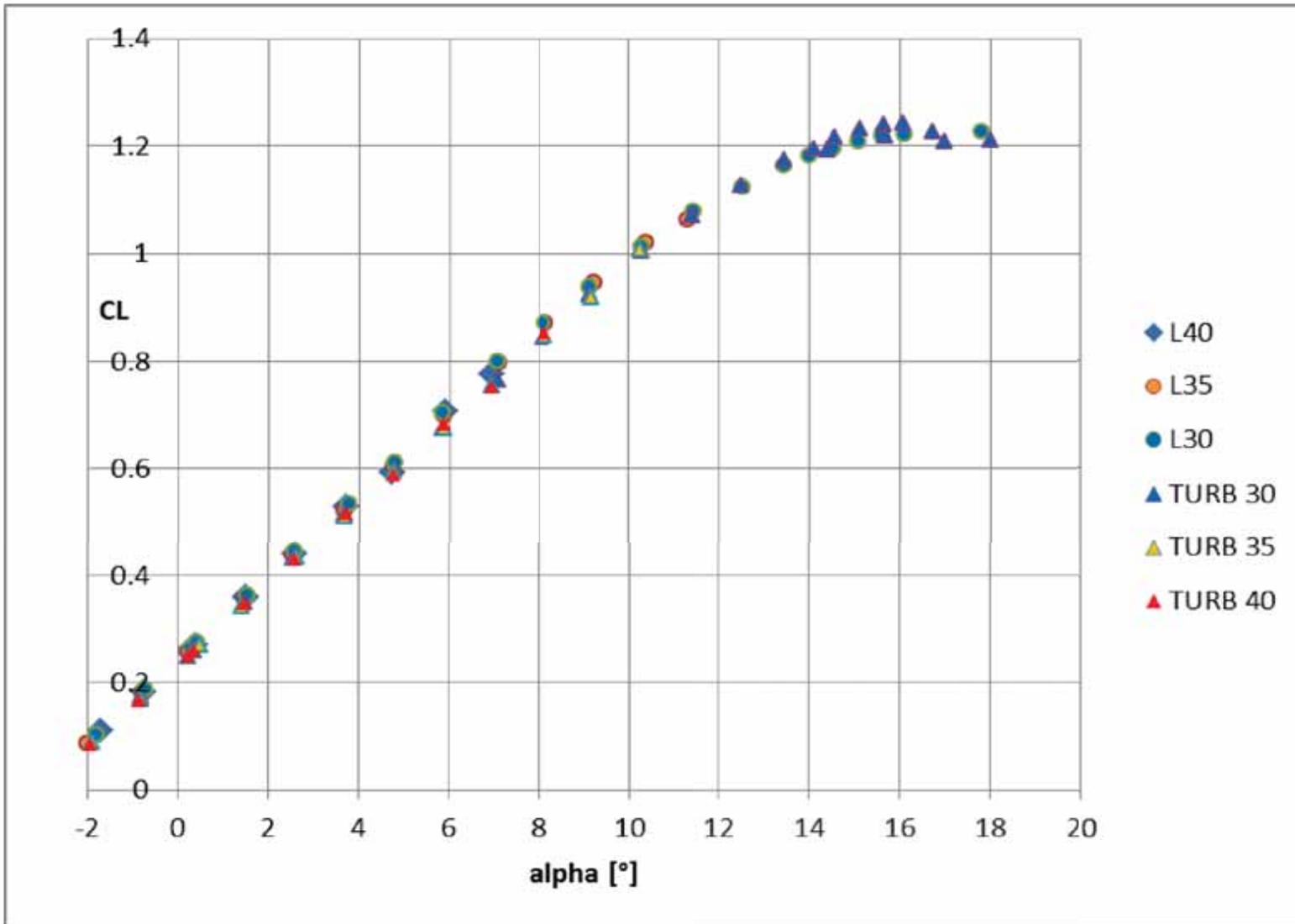
V=40 m/s



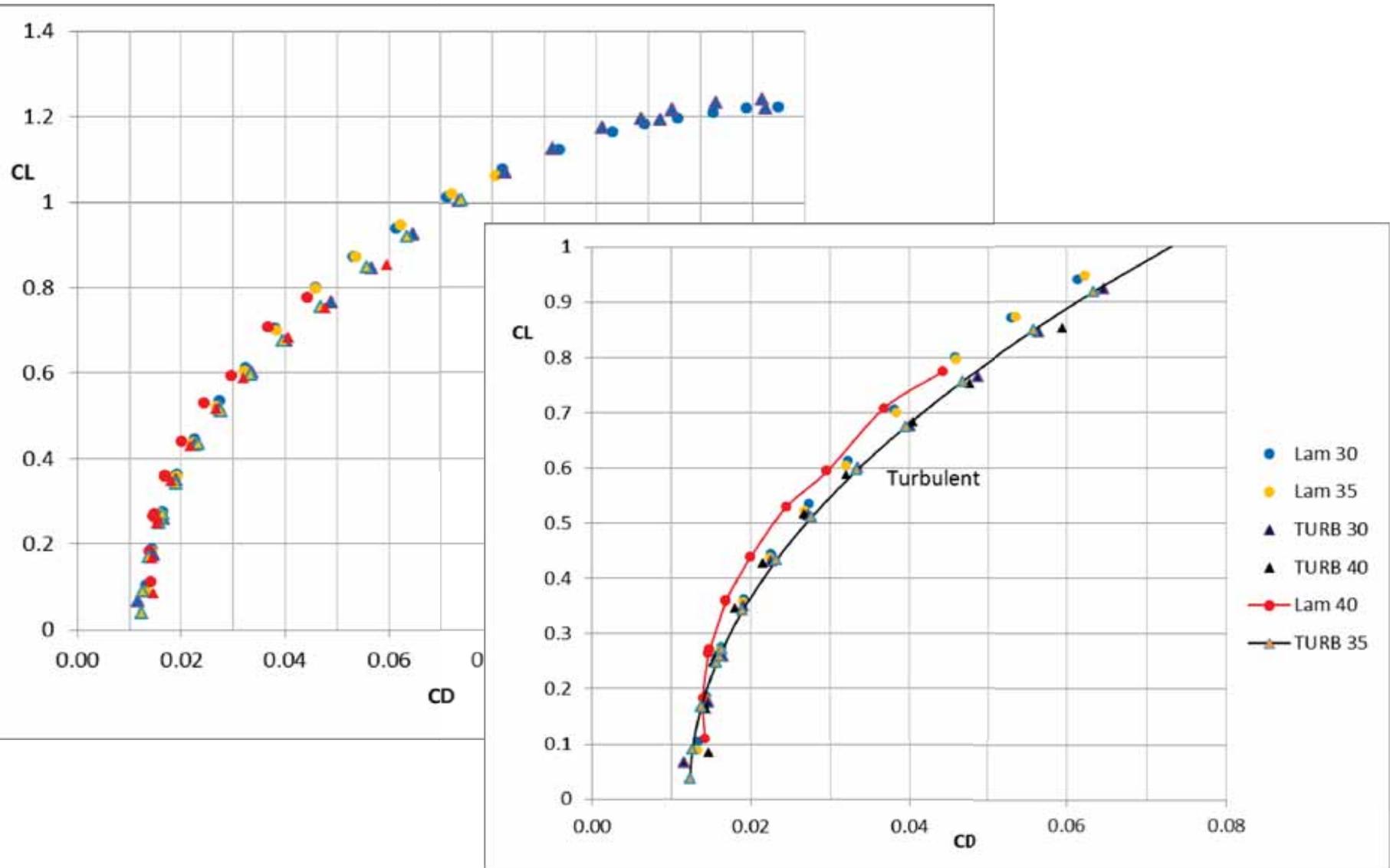
## TEST F28, V=variable, $\alpha=4^\circ$ , Turbulent b.l.



## Comparison of Aerodynamic coefficients. Effect of turbulent b.l. and wind speed (Reynolds)

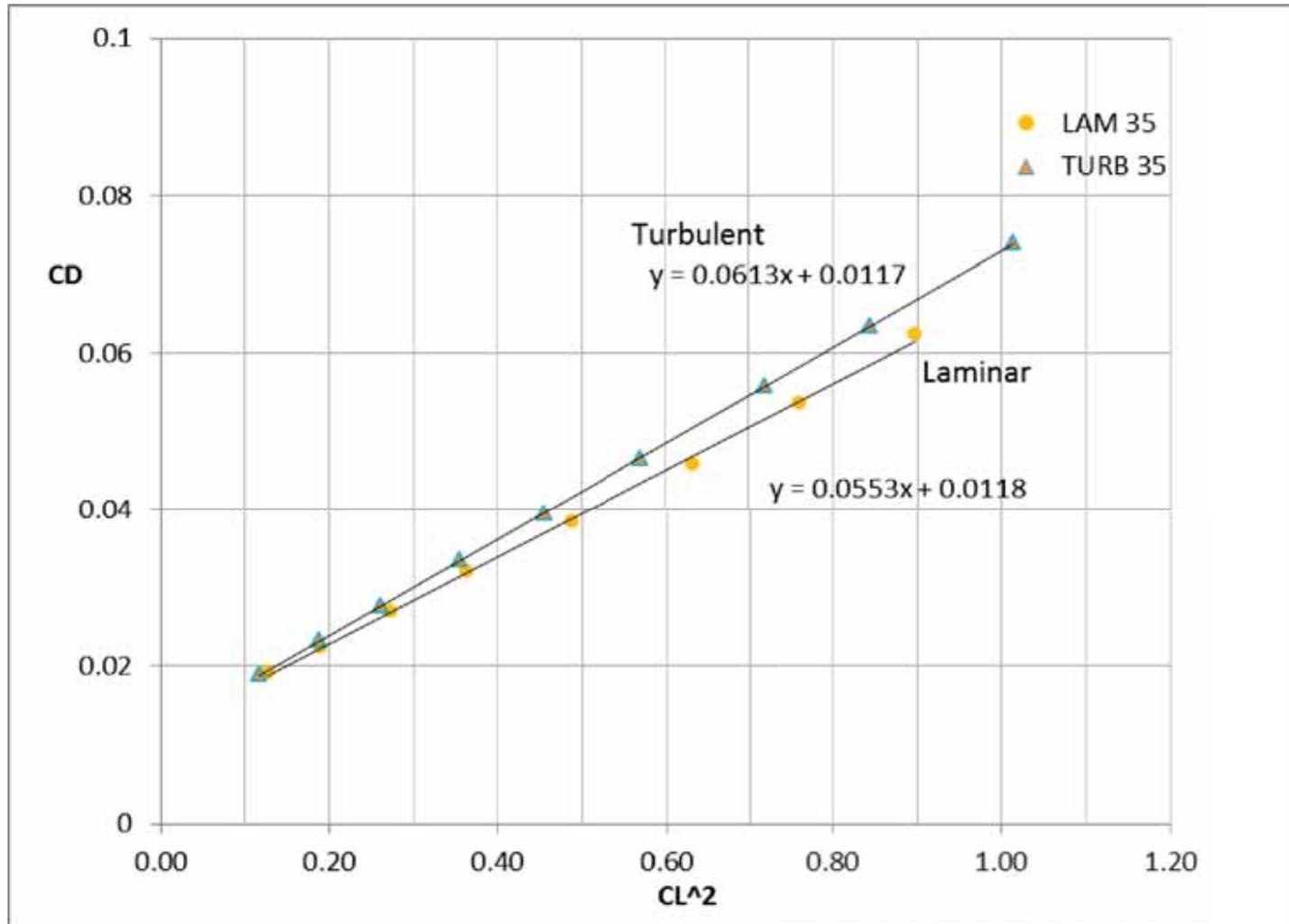


## Comparison of Aerodynamic coefficients. Effect of turbulent b.l. and wind speed (Reynolds)

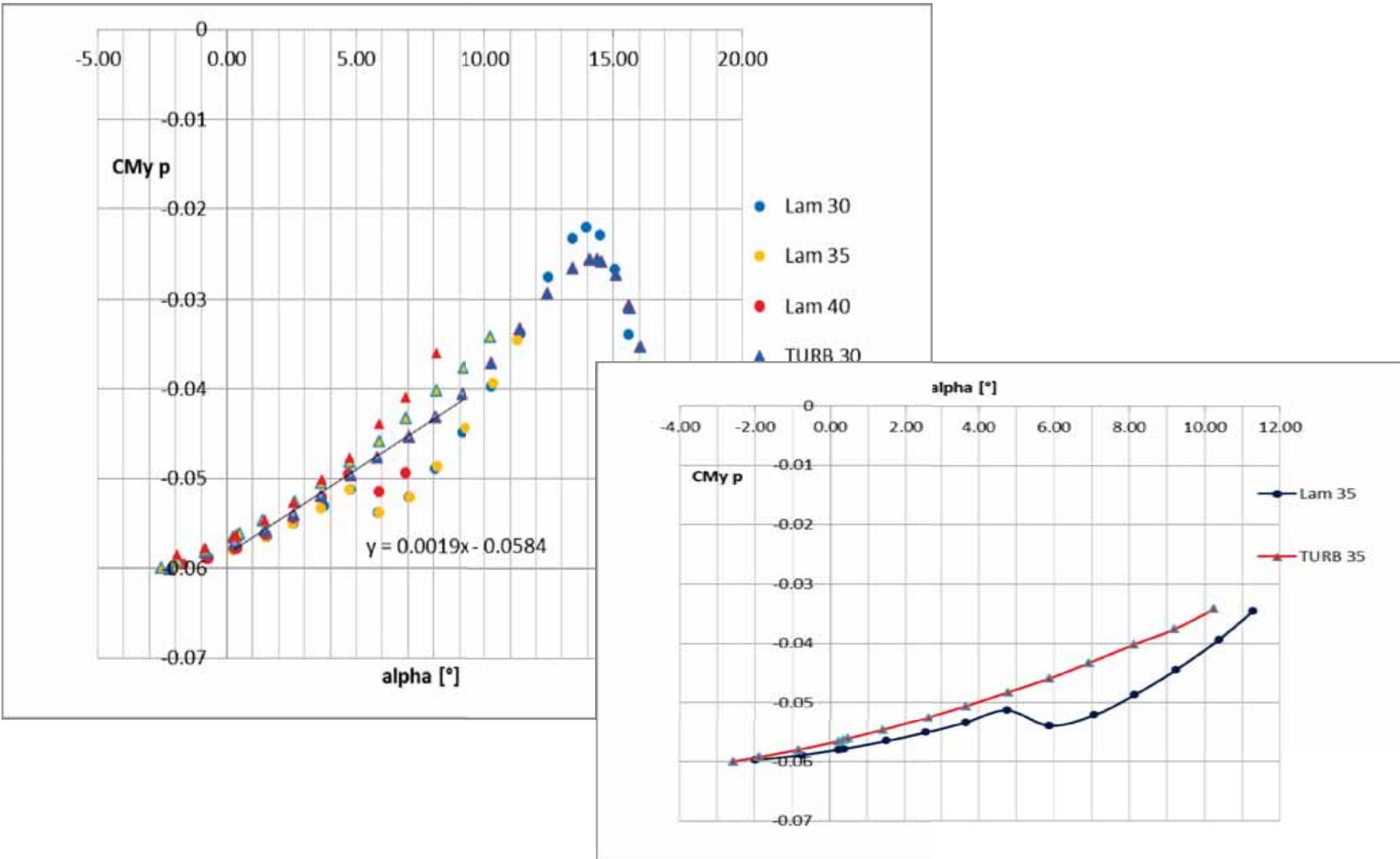


## Comparison of Aerodynamic coefficients. Effect of turbulent b.l. and wind speed (Reynolds)

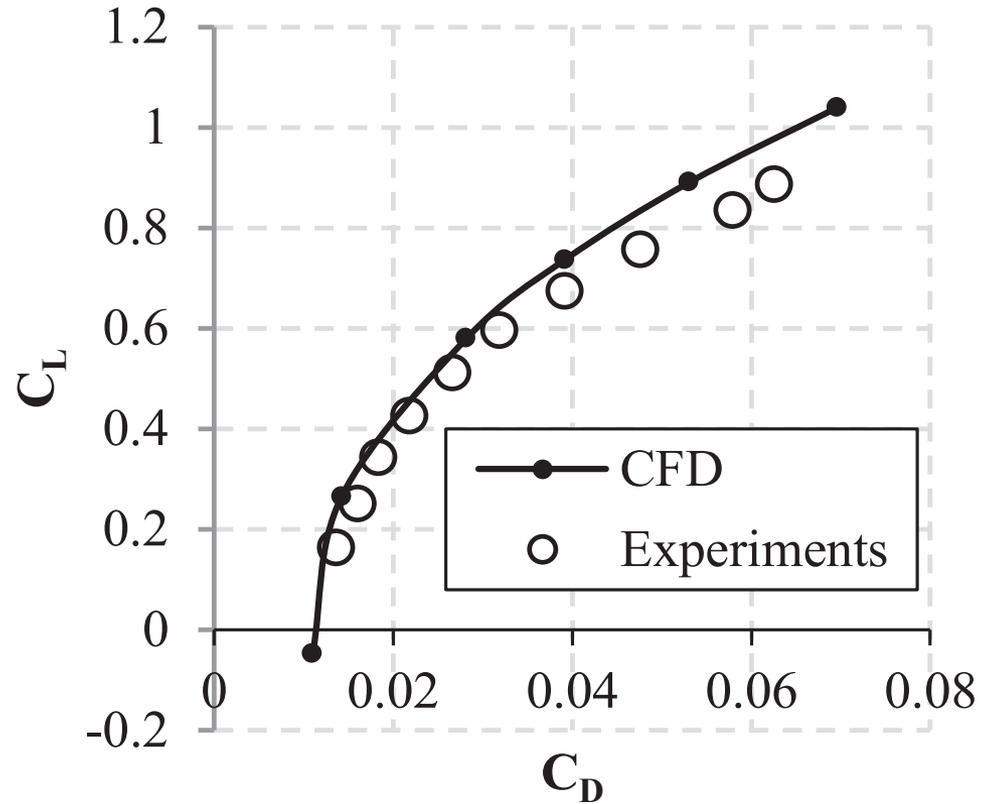
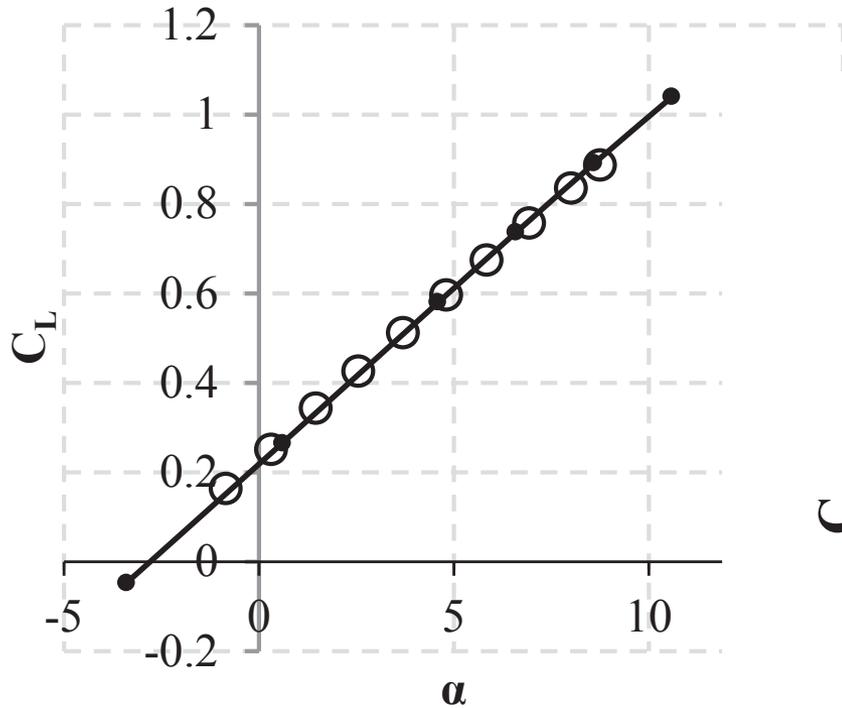
### Wing drag polar



## Comparison of Aerodynamic coefficients. Effect of turbulent b.l. and wind speed (Reynolds)



## FORCE MEASUREMENT – Comparison with CFD prediction





## TEST RESULTS. Pressure measurements

### ***CLEAN Conditions***

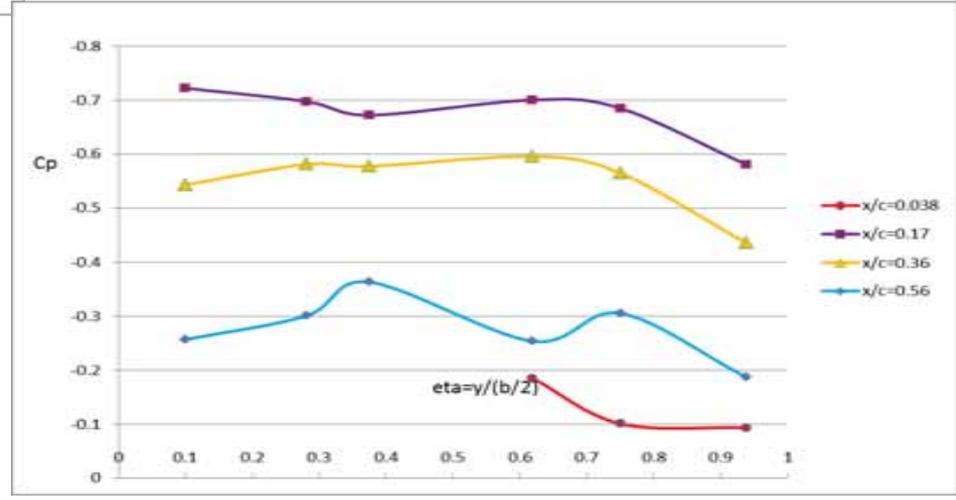
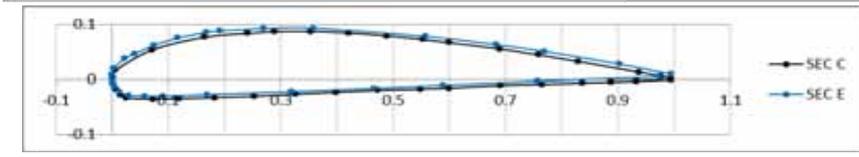
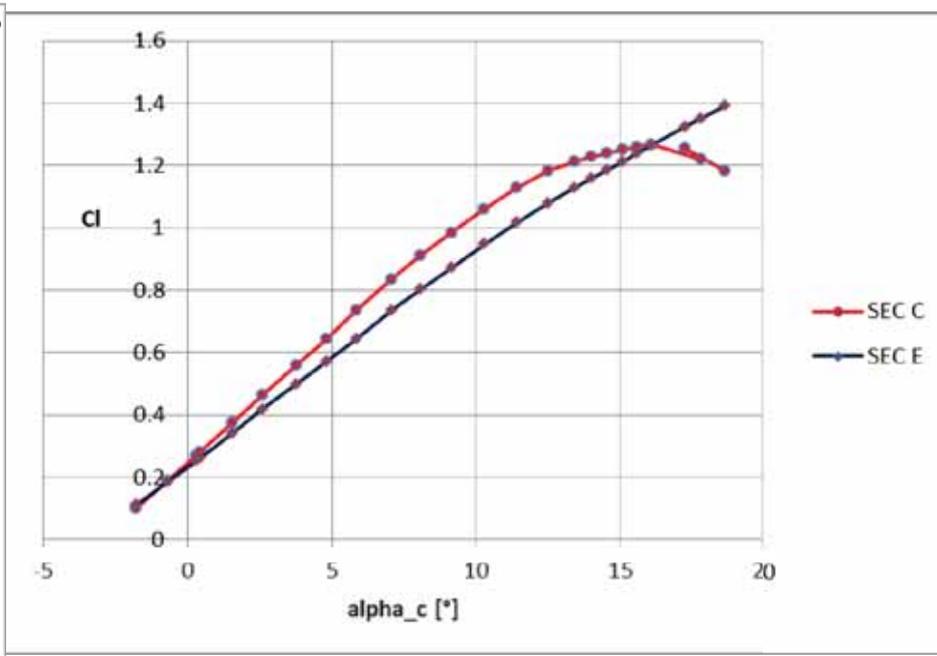
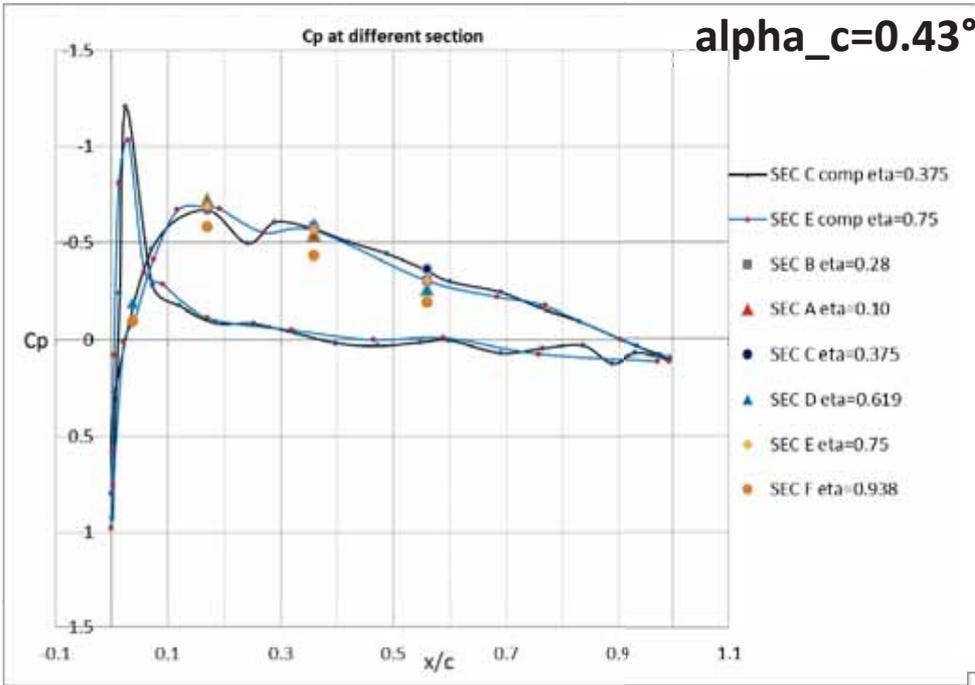
TEST L30	30 m/s	1.06 mill. Full polar (up to stall) free transition	L, D, M, Cp
TEST L35	35 m/s	1.25 mill. (Alpha=0-10°) polar free trans.	L, D, M, Cp
TEST L40	40 m/s	1.43 mill. Limited (up to 8°) polar free trans.	L, D, M, Cp

### ***TURBULENT Conditions(b.l. tripped at l.e)***

TEST T30	30 m/s	1.06 mill. Full polar fixed trans 1-2%	L, D, M, Cp, strain
TEST T35	35 m/s	1.25 mill. Full polar fixed trans 1-2%	L, D, M, Cp, strain
TEST T40	40 m/s	1.43 mill. Limited polar fixed trans 1-2%	L, D, M, Cp, strain

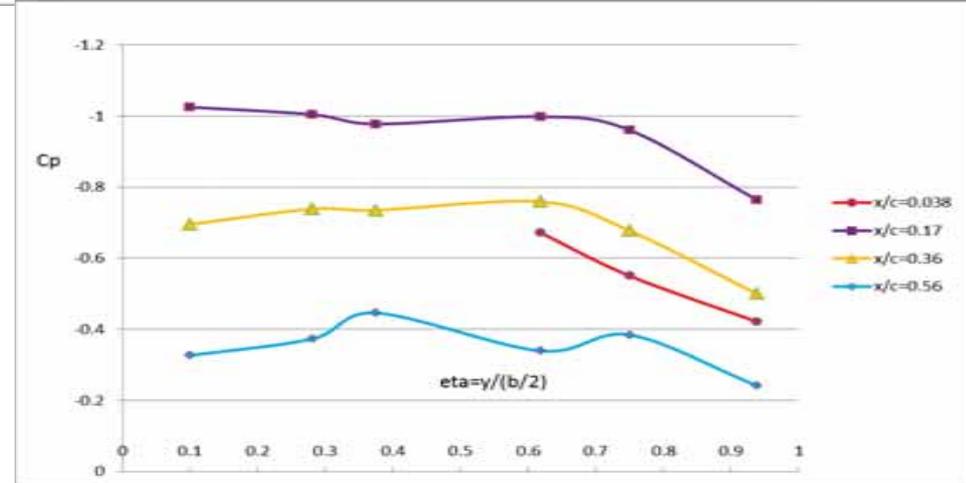
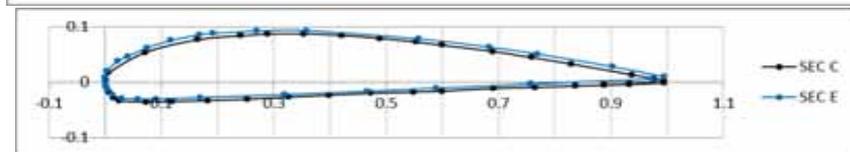
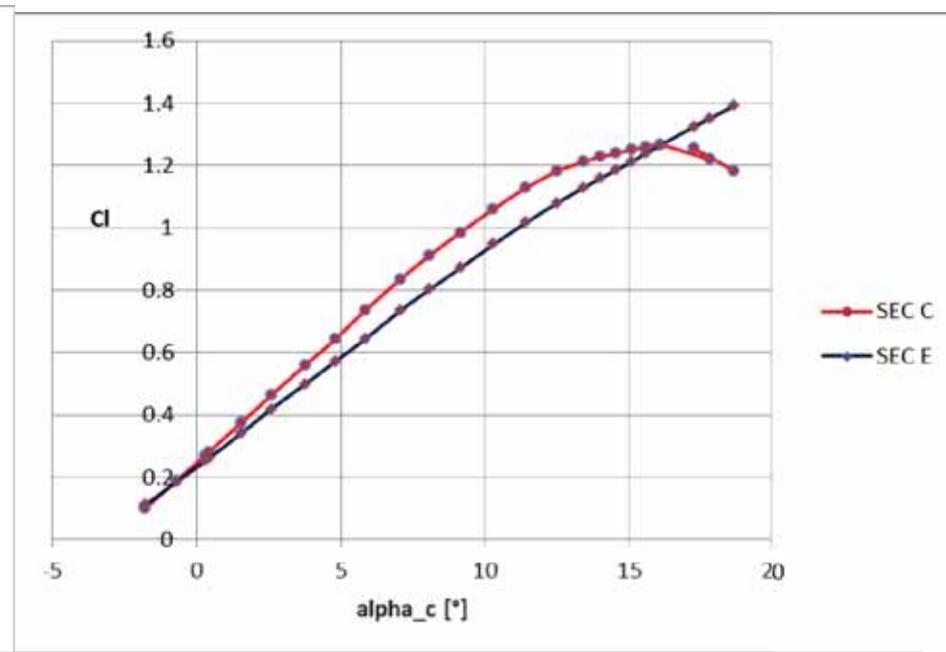
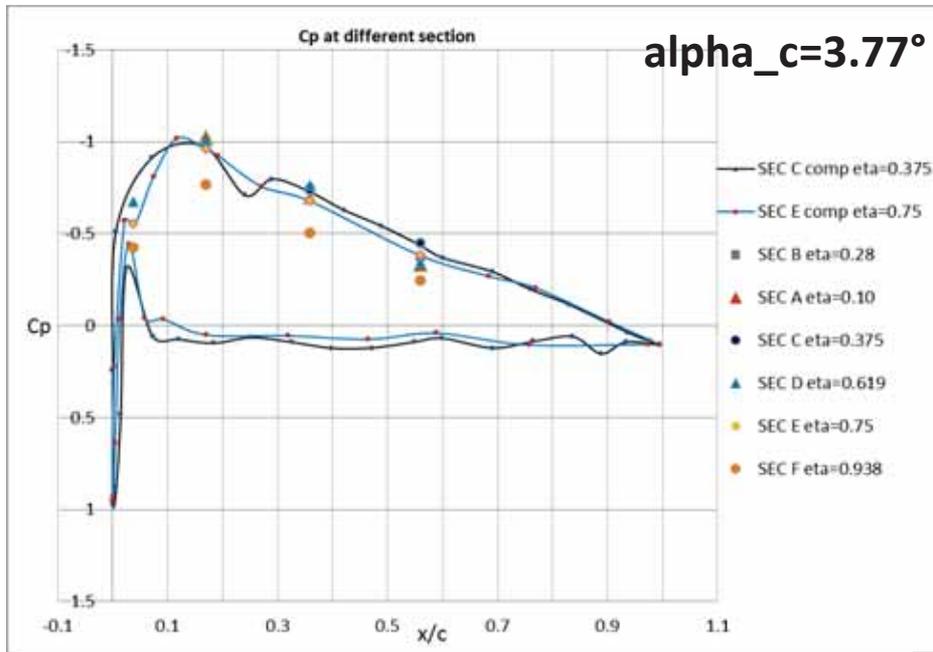
## TEST RESULTS. Pressure measurements

## TEST L30, V=30 m/s Clean Model



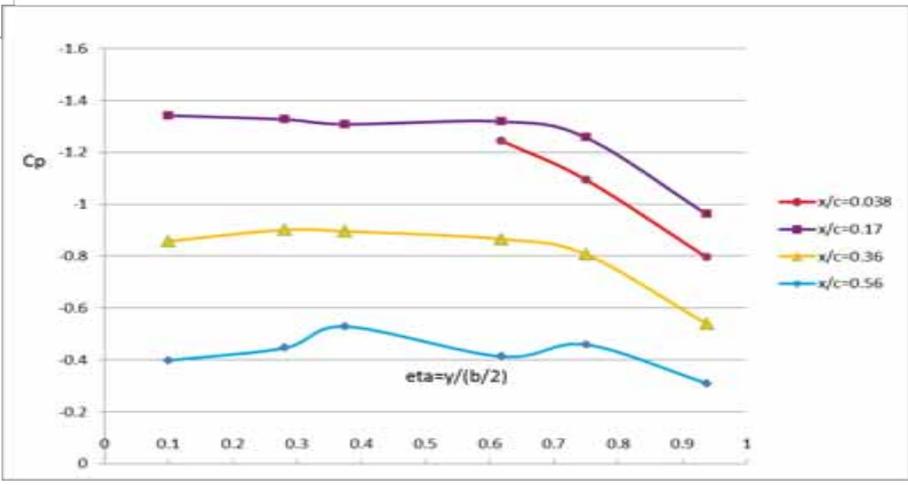
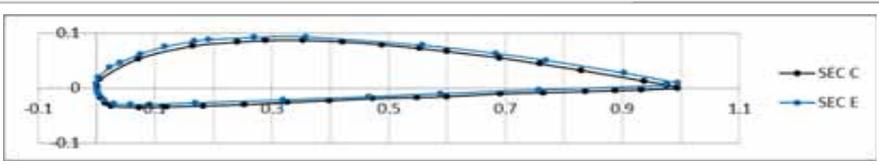
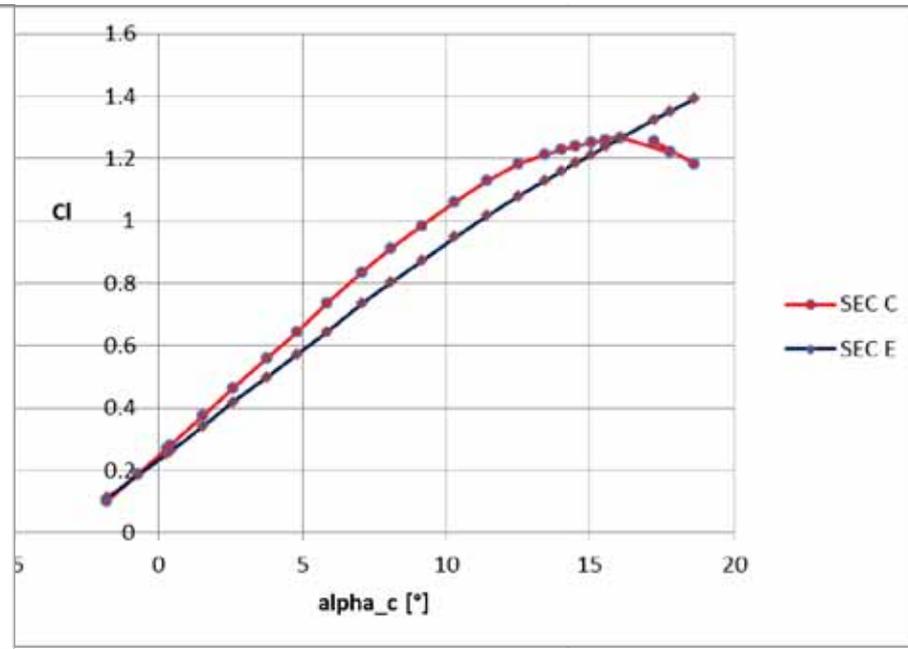
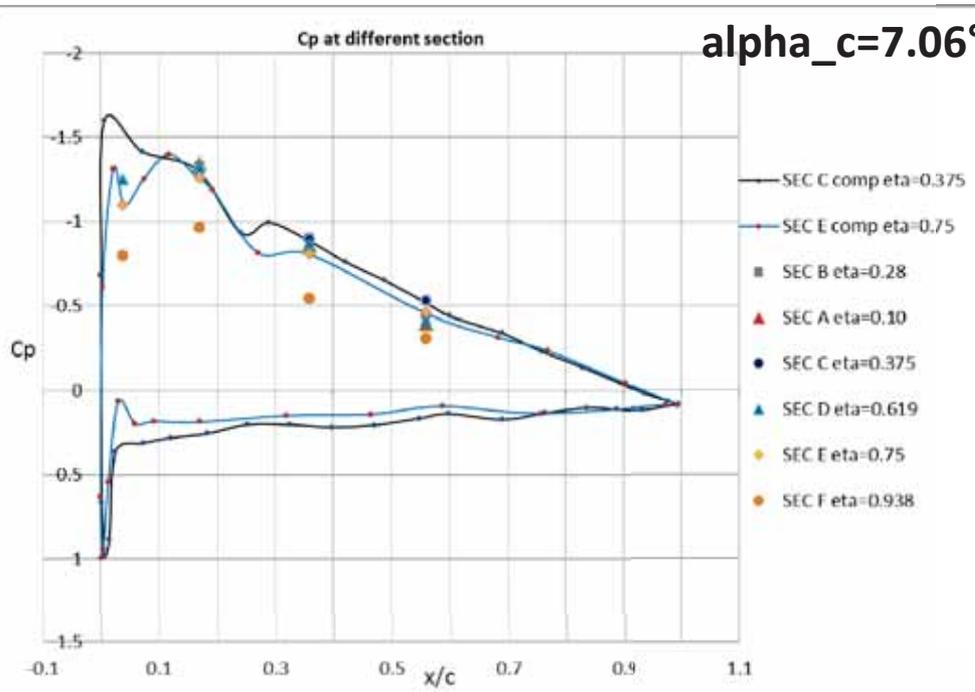
## TEST RESULTS. Pressure measurements

## TEST L30, V=30 m/s Clean Model



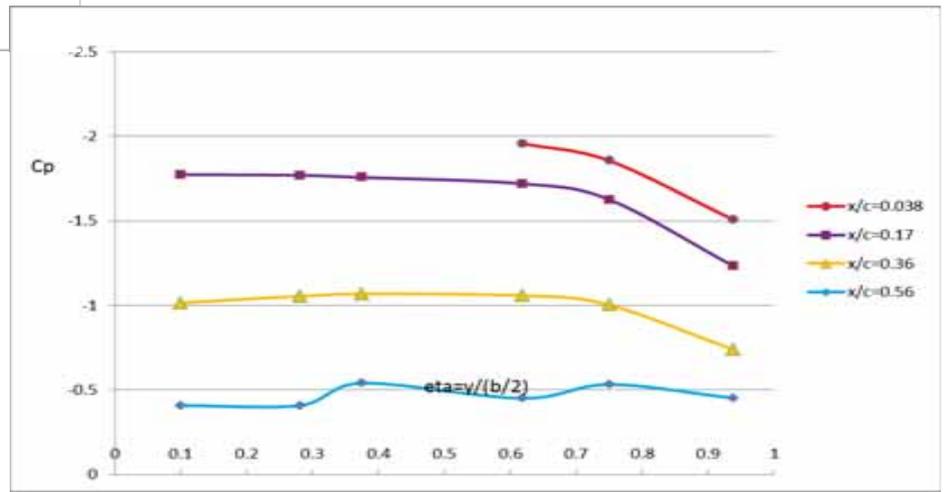
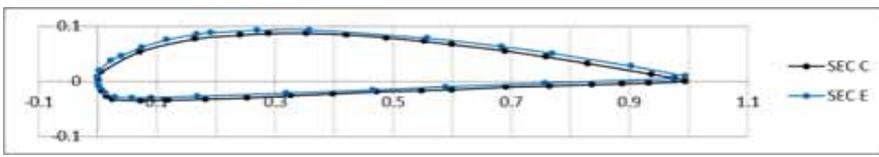
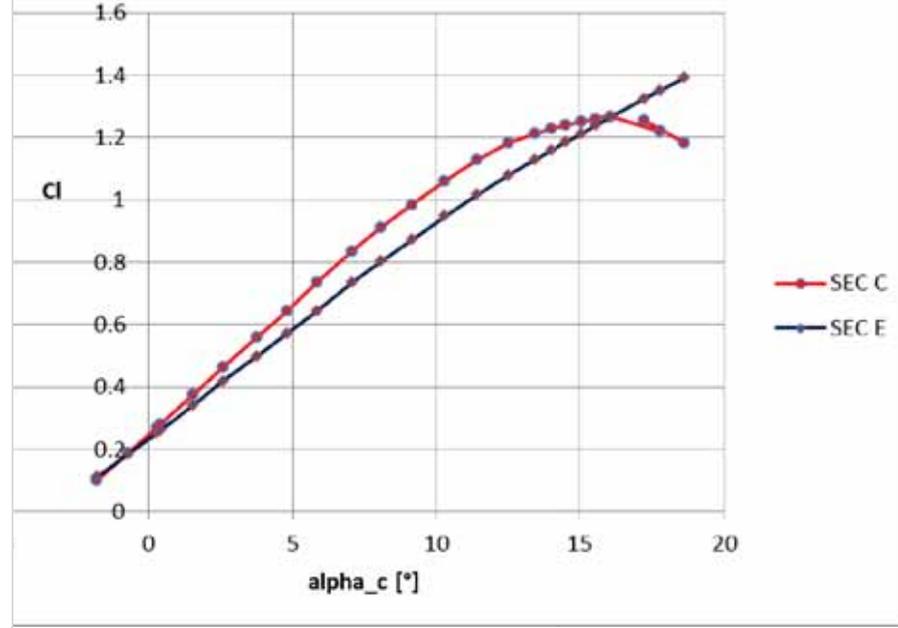
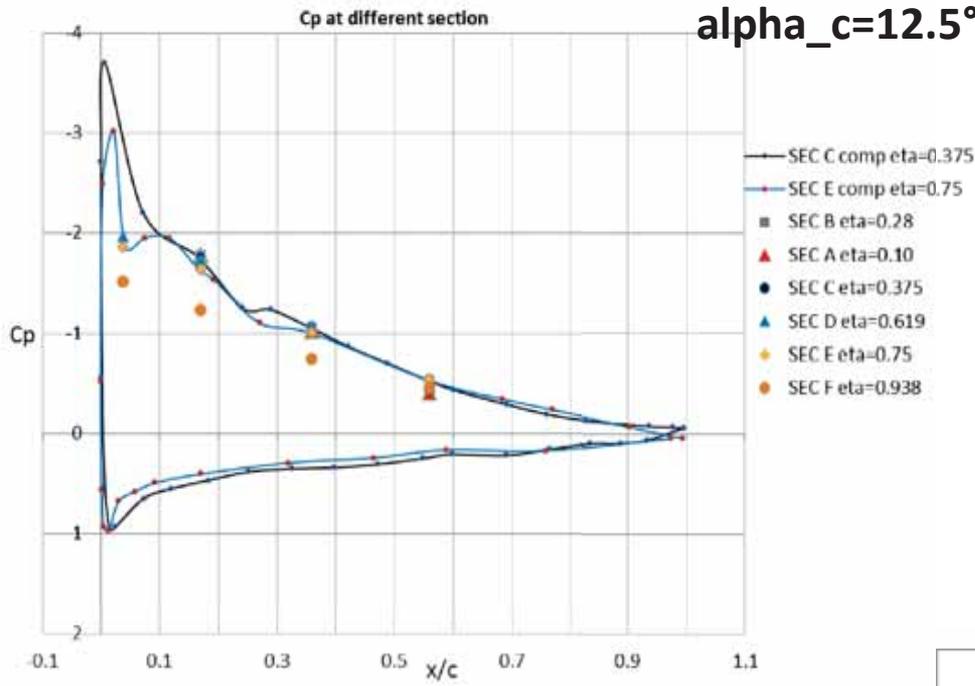
# TEST RESULTS. Pressure measurements

## TEST L30, V=30 m/s Clean Model



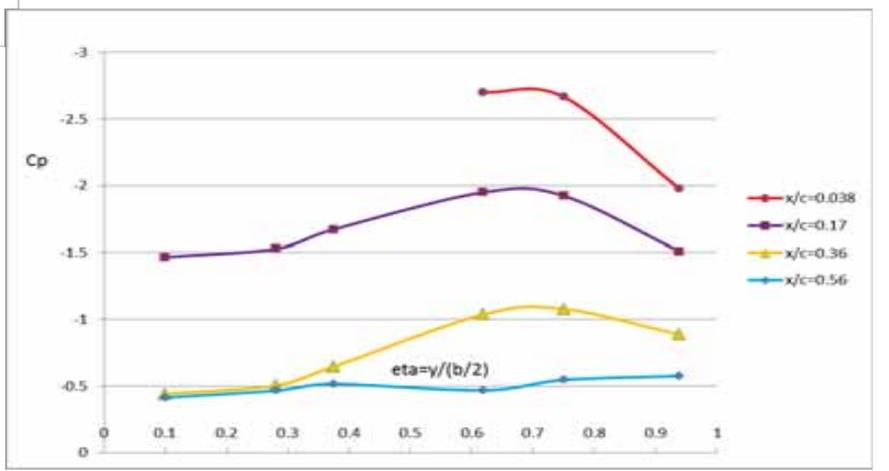
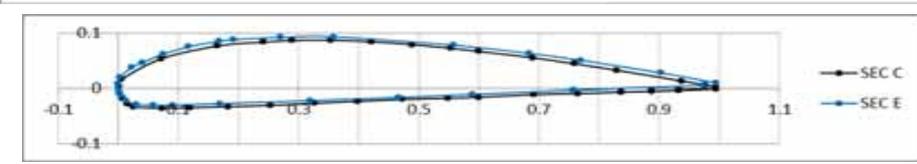
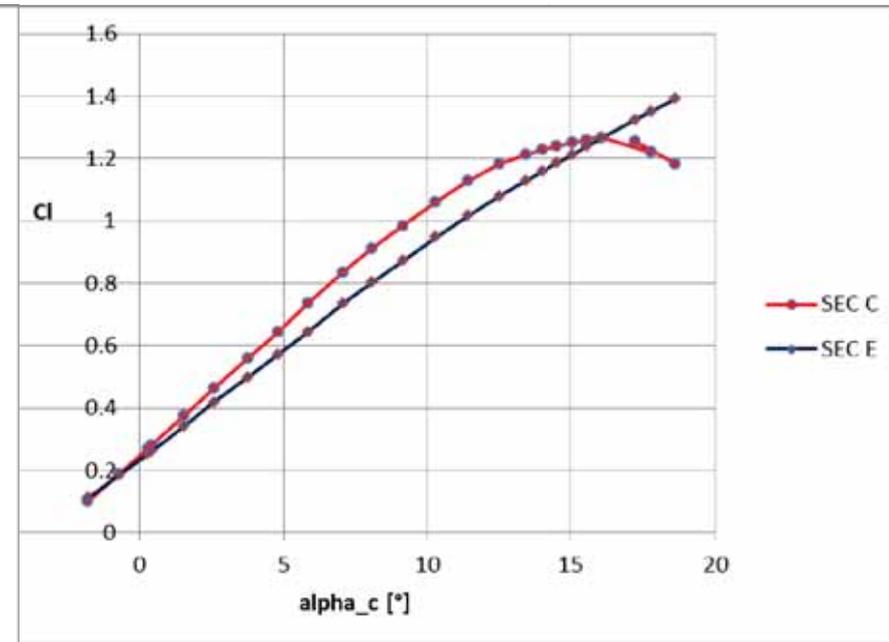
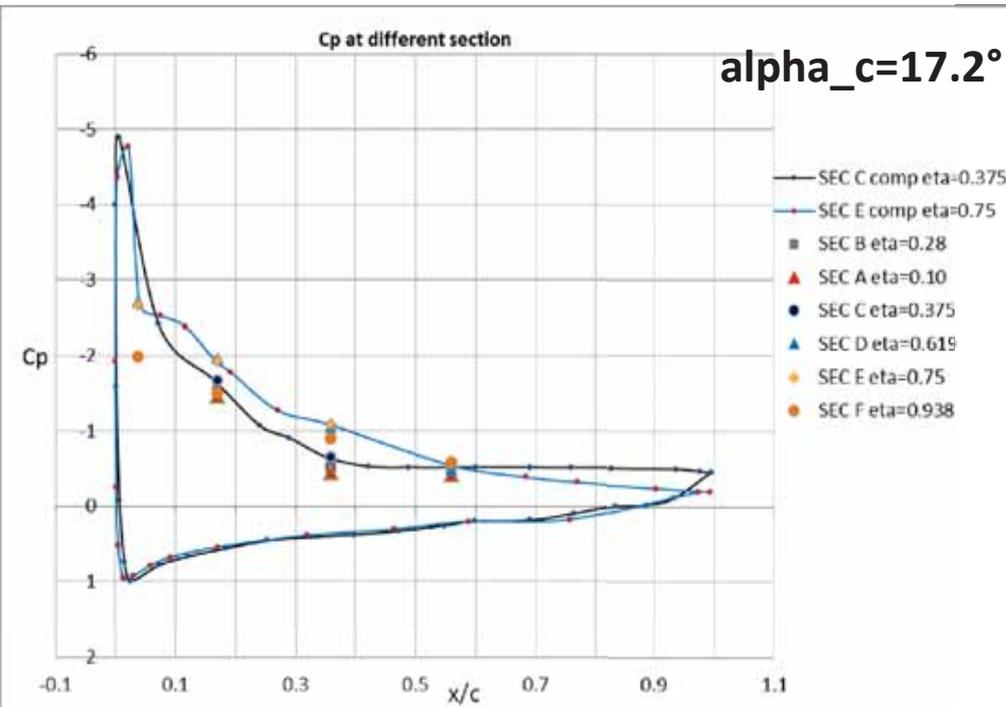
# TEST RESULTS. Pressure measurements

## TEST L30, V=30 m/s Clean Model



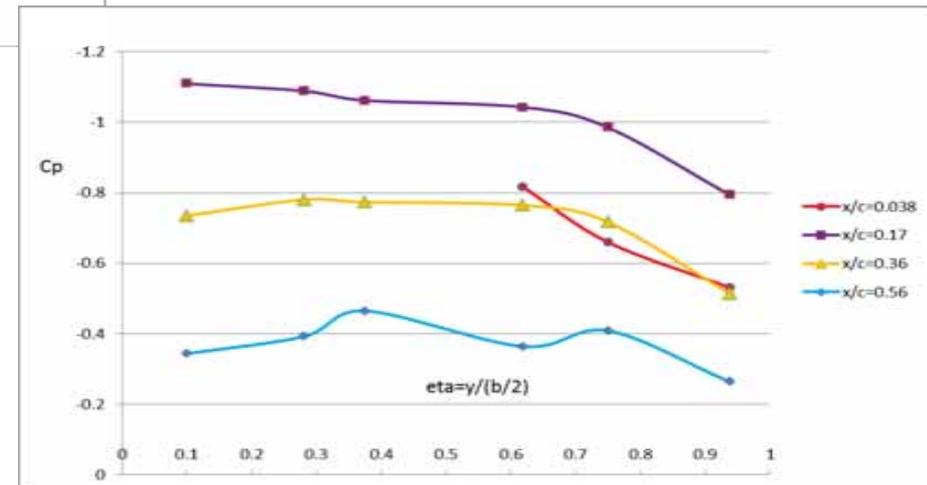
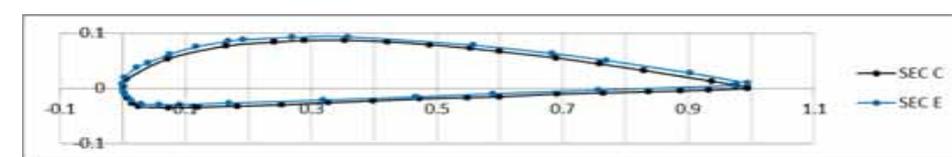
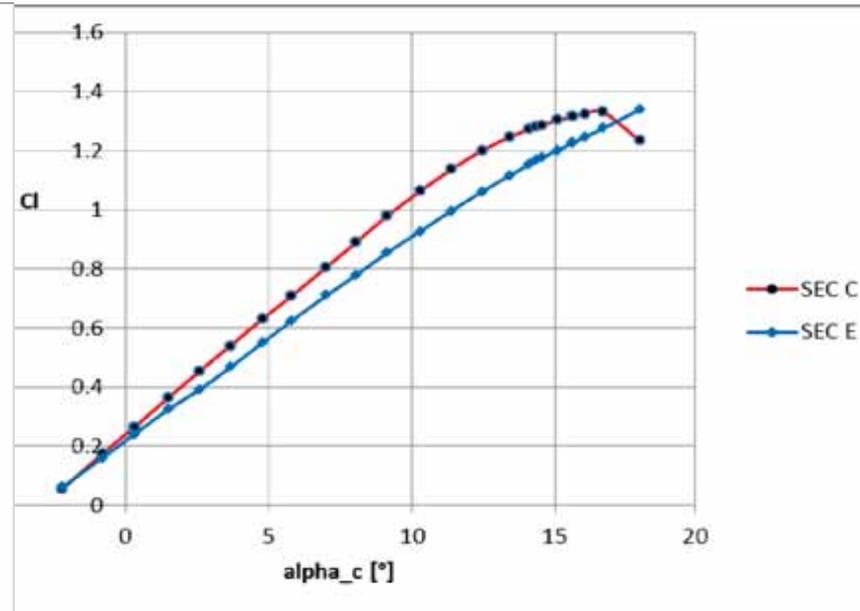
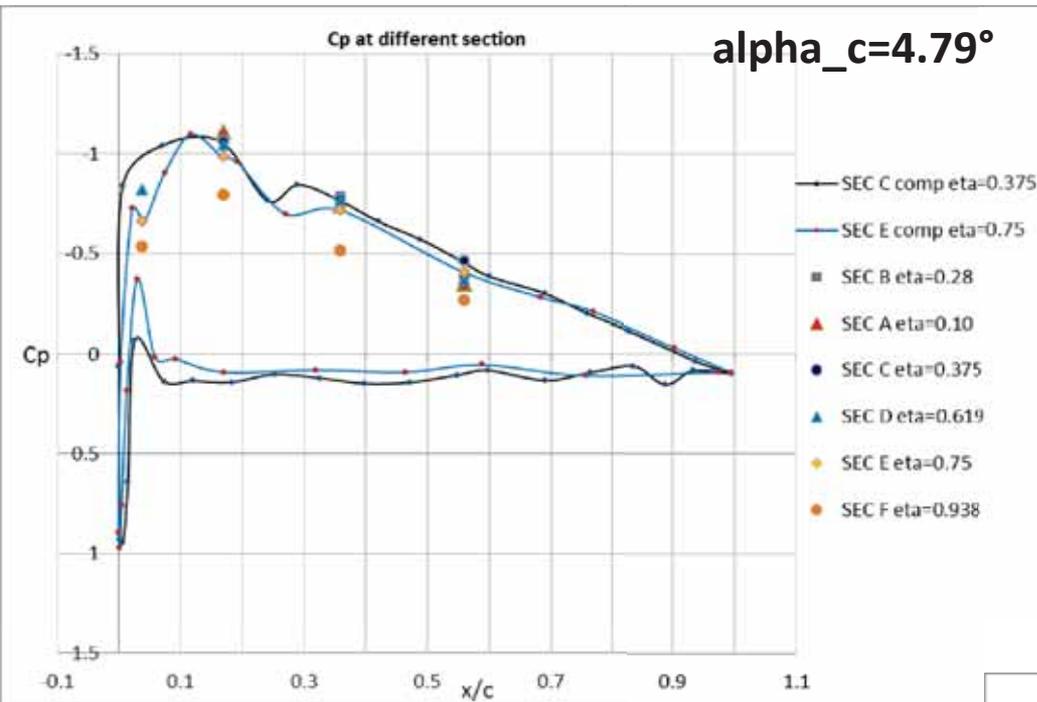
# TEST RESULTS. Pressure measurements

## TEST L30, V=30 m/s Clean Model



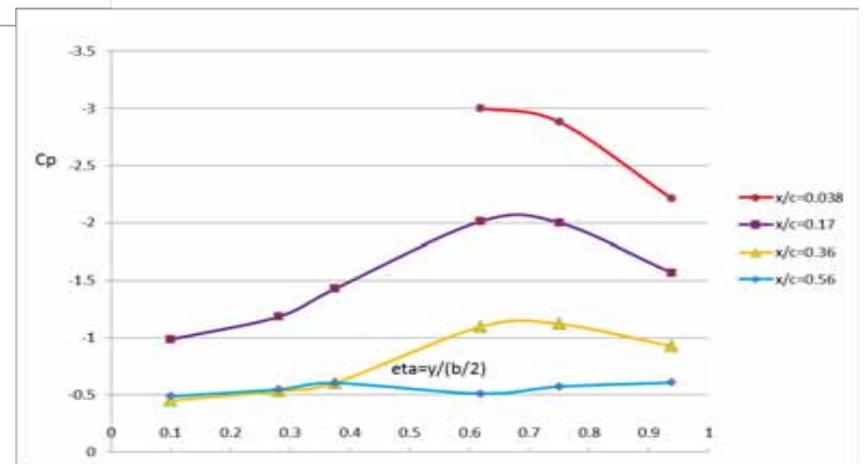
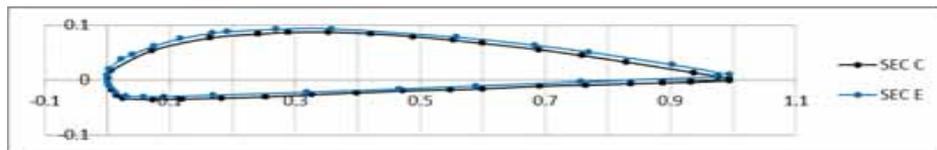
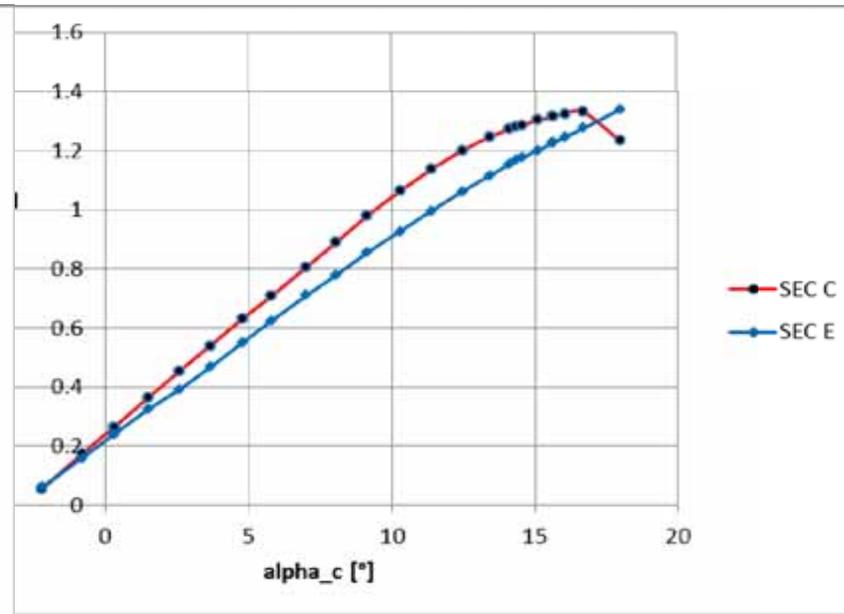
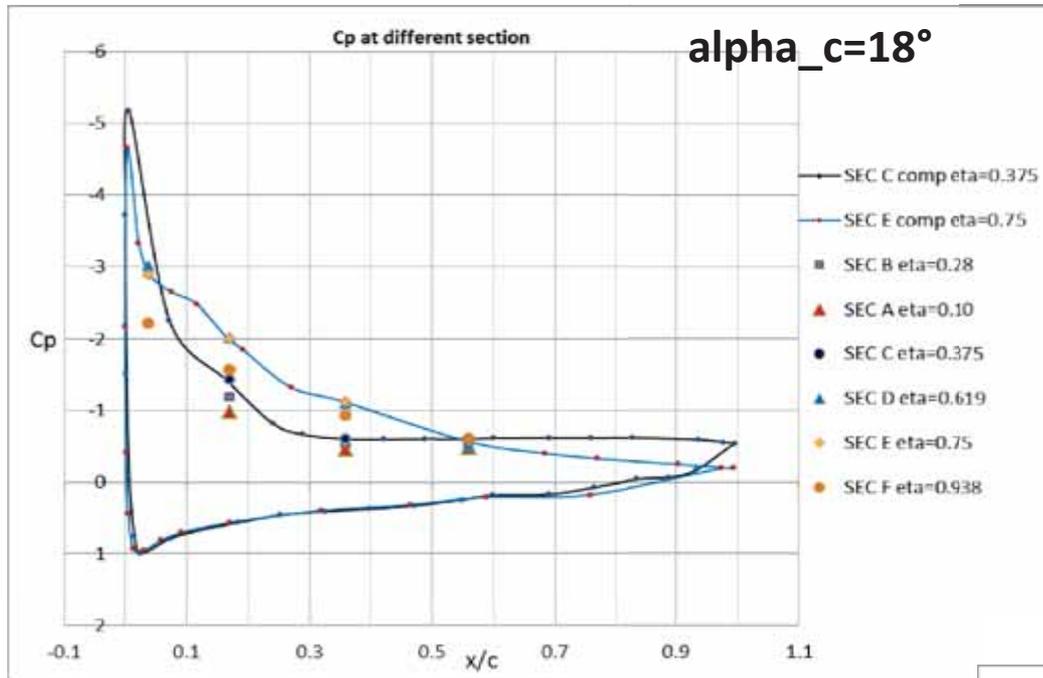
# TEST RESULTS. Pressure measurements

## TEST T30, V=30 m/s Turbulent



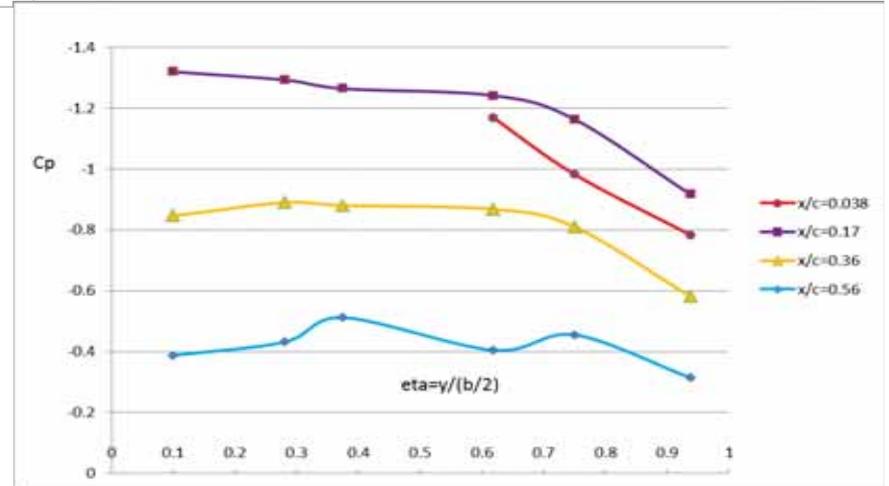
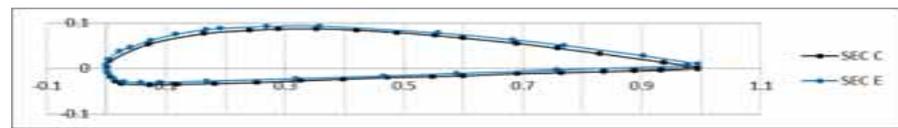
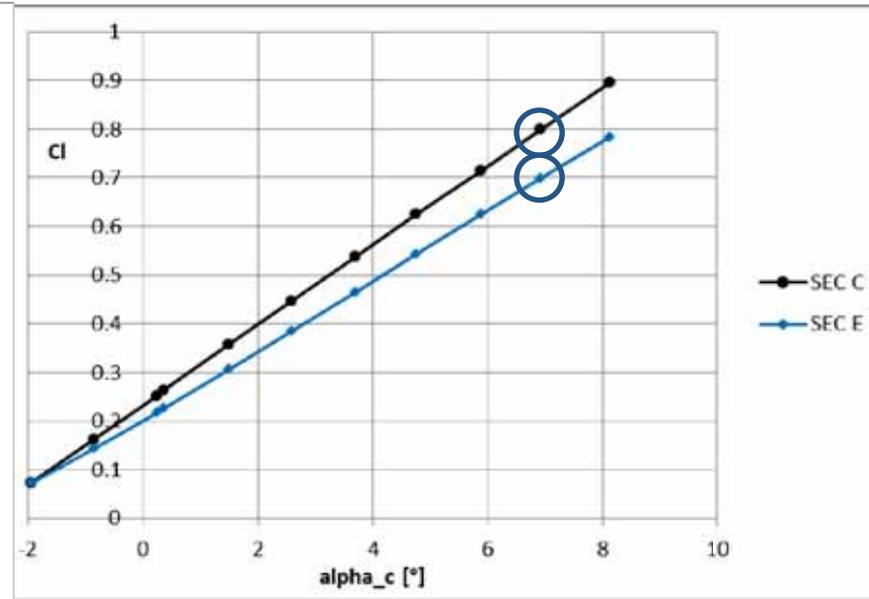
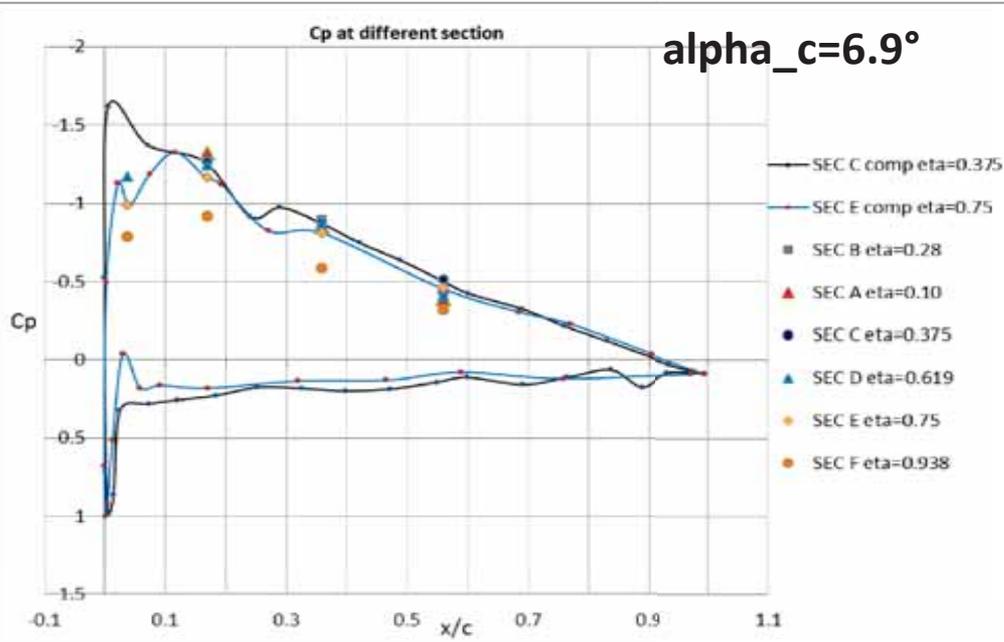
## TEST RESULTS. Pressure measurements

## TEST T30, V=30 m/s Turbulent



## TEST RESULTS. Pressure measurements

## TEST T40, V=40 m/s Turbulent

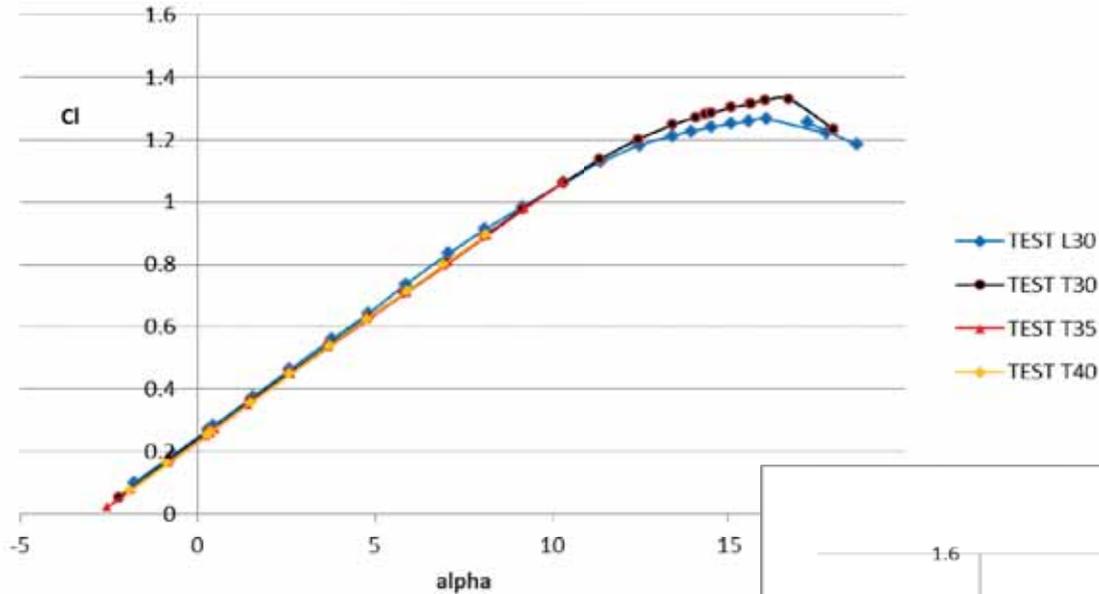


**Load condition chosen for stress and deformation monitoring**

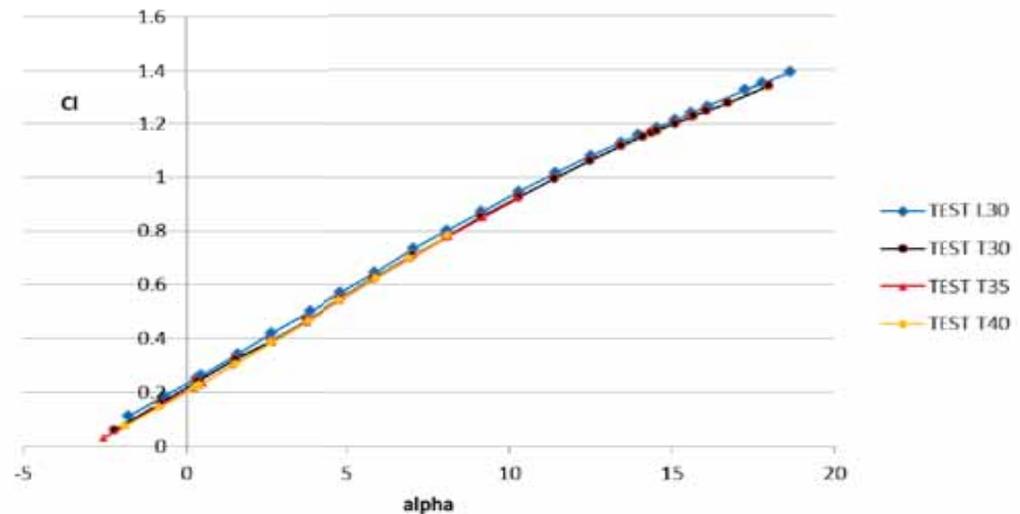
## TEST RESULTS. Pressure measurements

## COMPARISON

### Section C

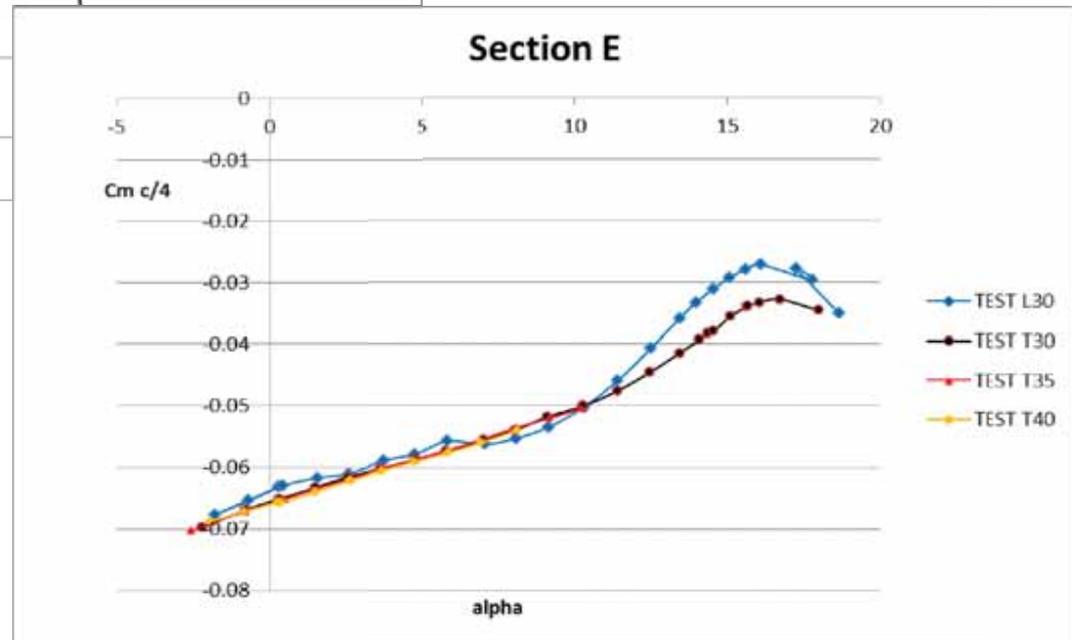
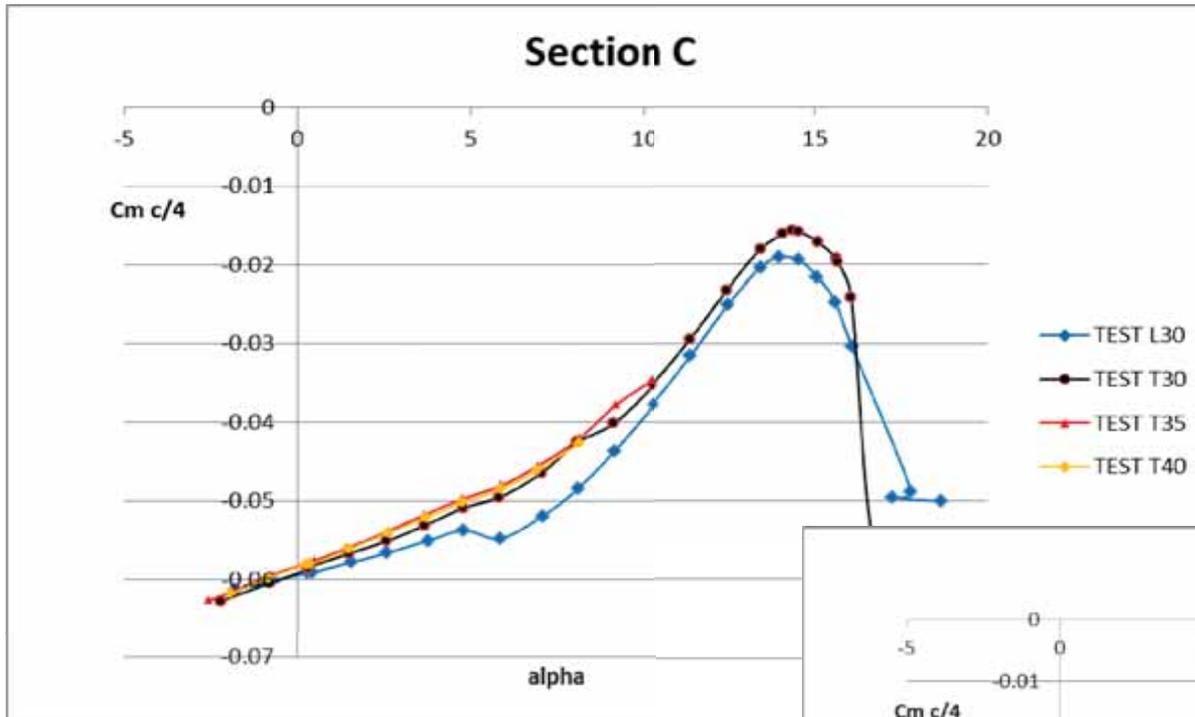


### Section E



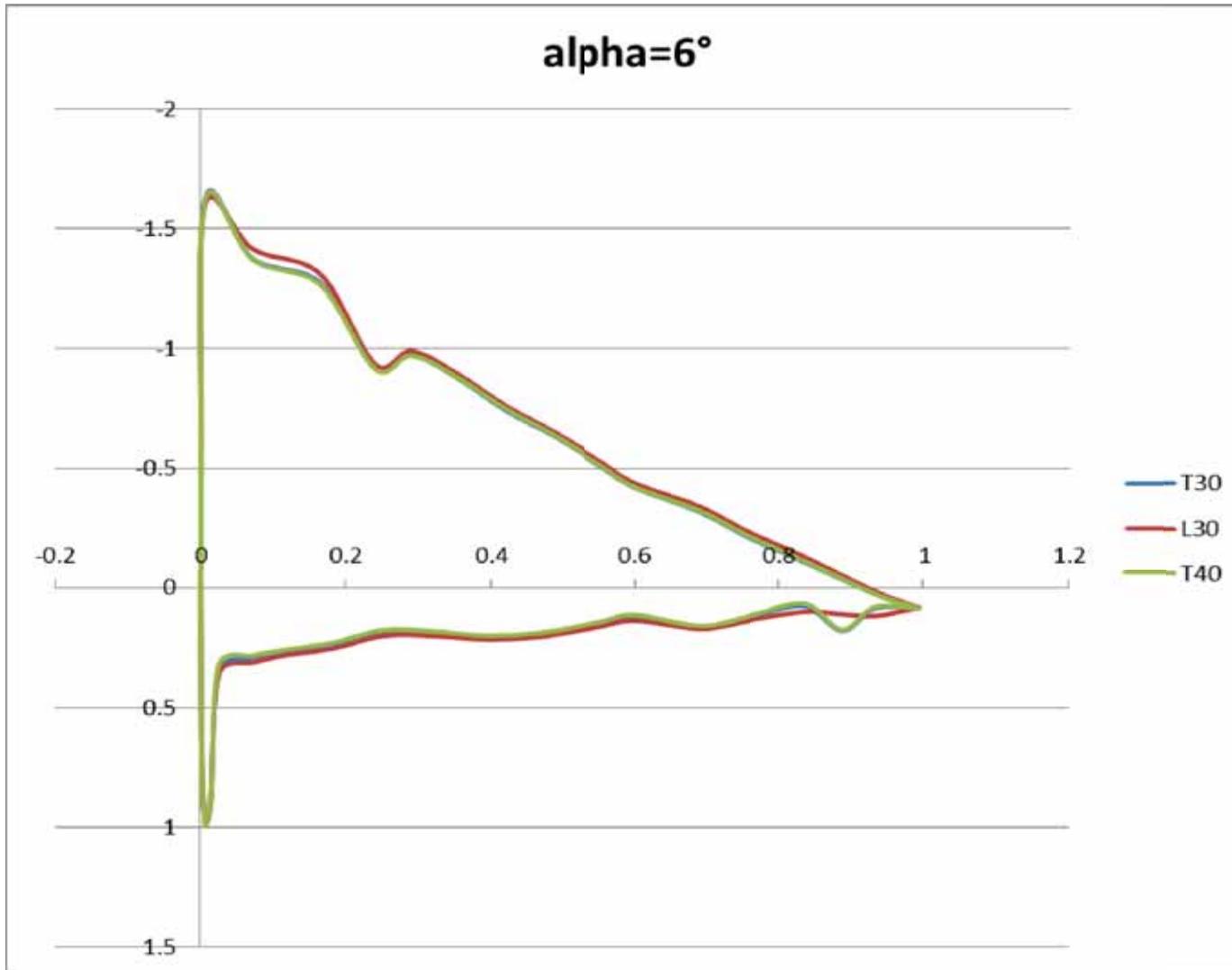
## TEST RESULTS. Pressure measurements

## COMPARISON



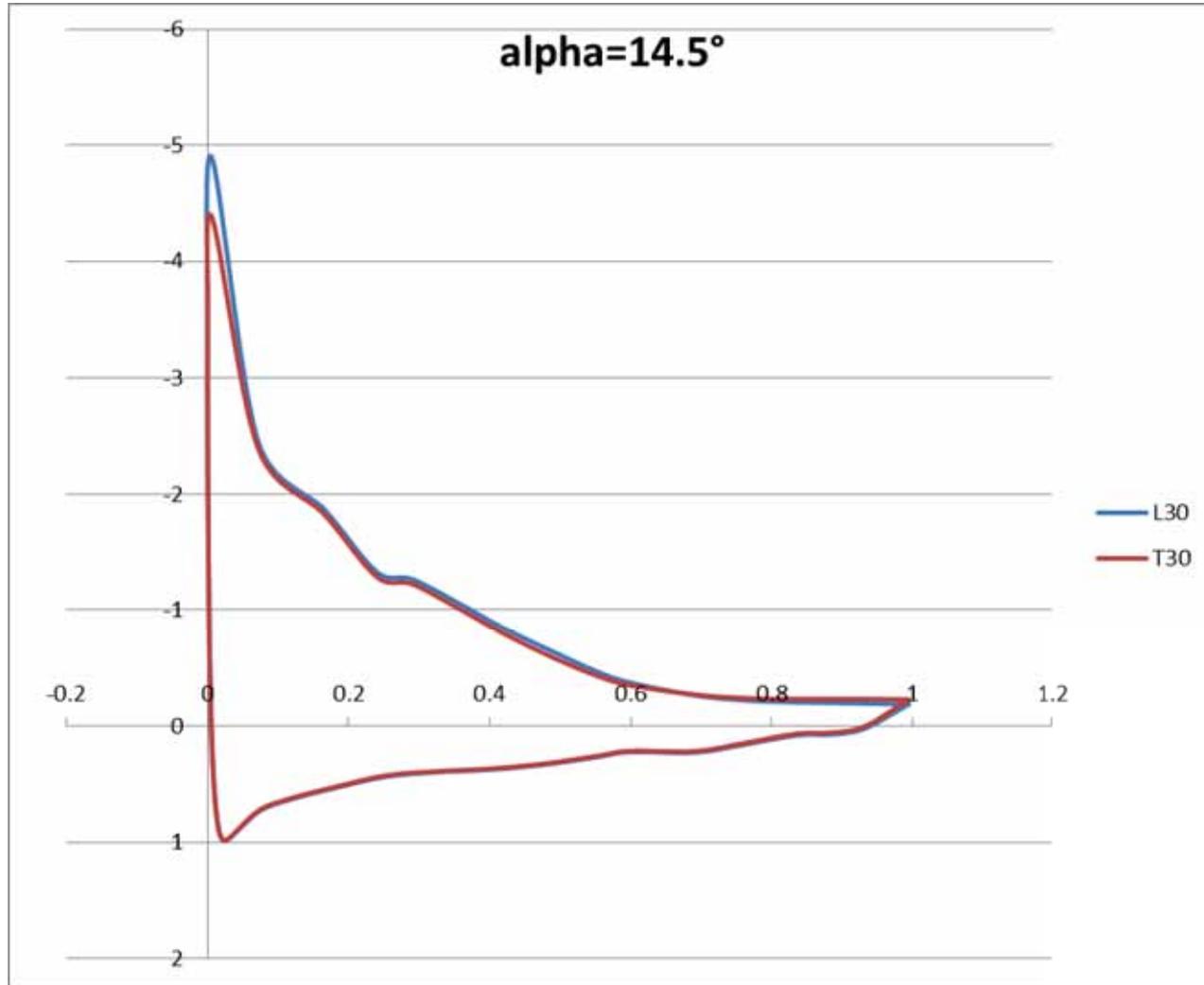
## TEST RESULTS. Pressure measurements

## COMPARISON section C



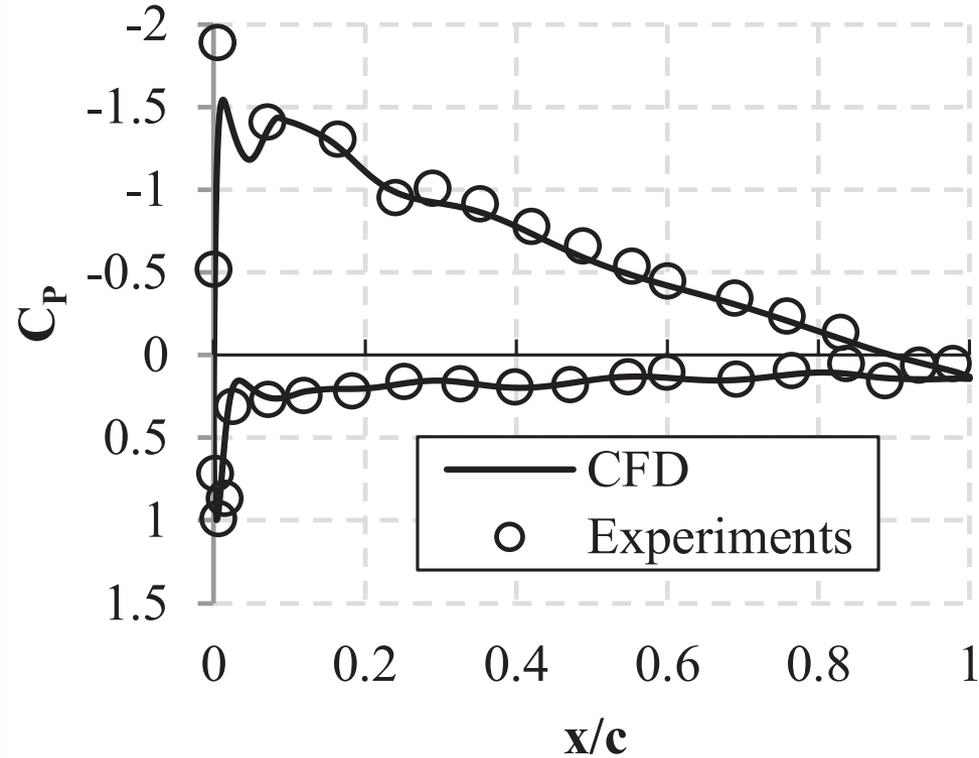
## TEST RESULTS. Pressure measurements

## COMPARISON section C

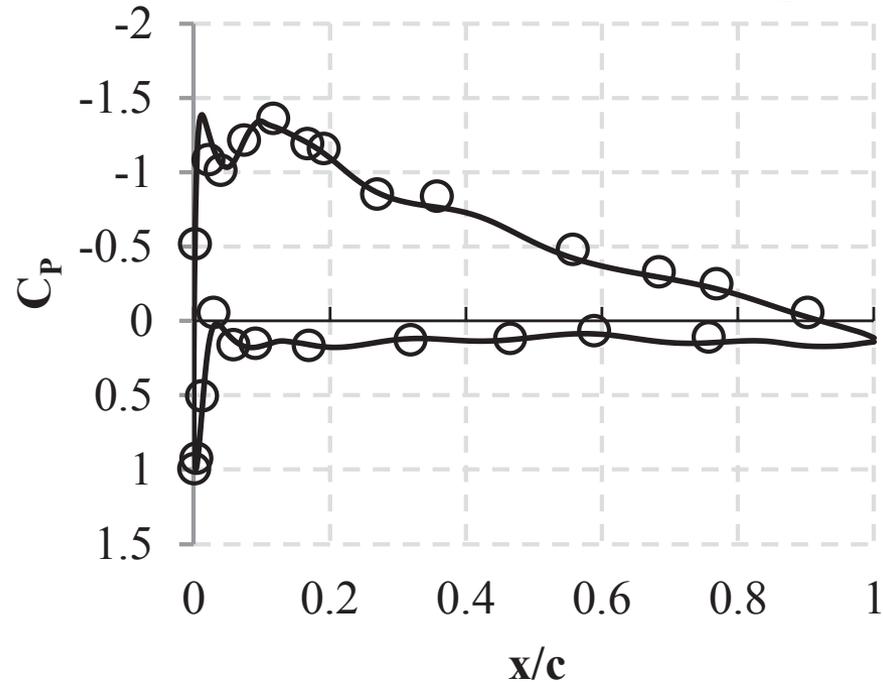


## TEST RESULTS. Pressure measurements

### Sec. 37.5 %b ( $\alpha = 6.6$ deg)

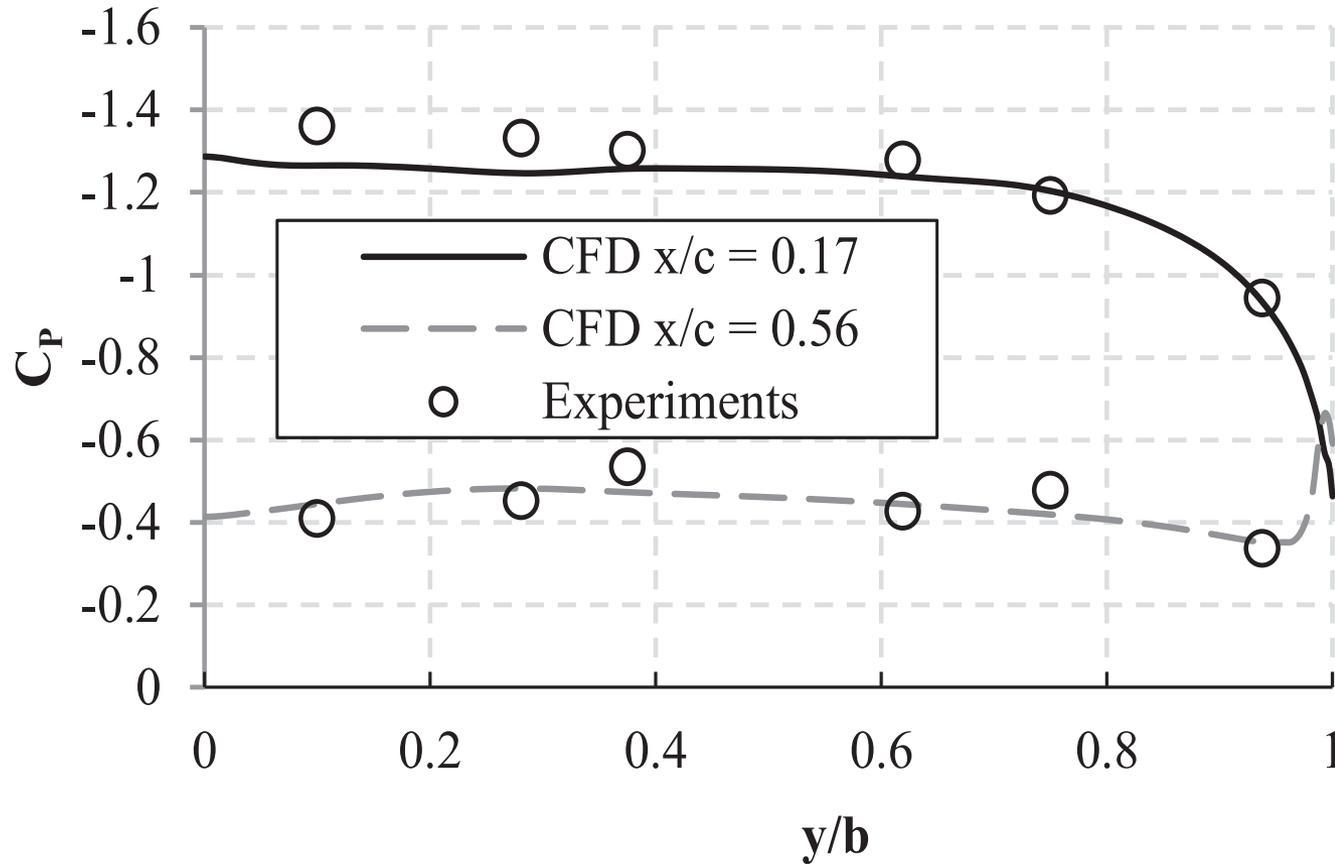


### Sec. 75%b ( $\alpha = 6.6$ deg)

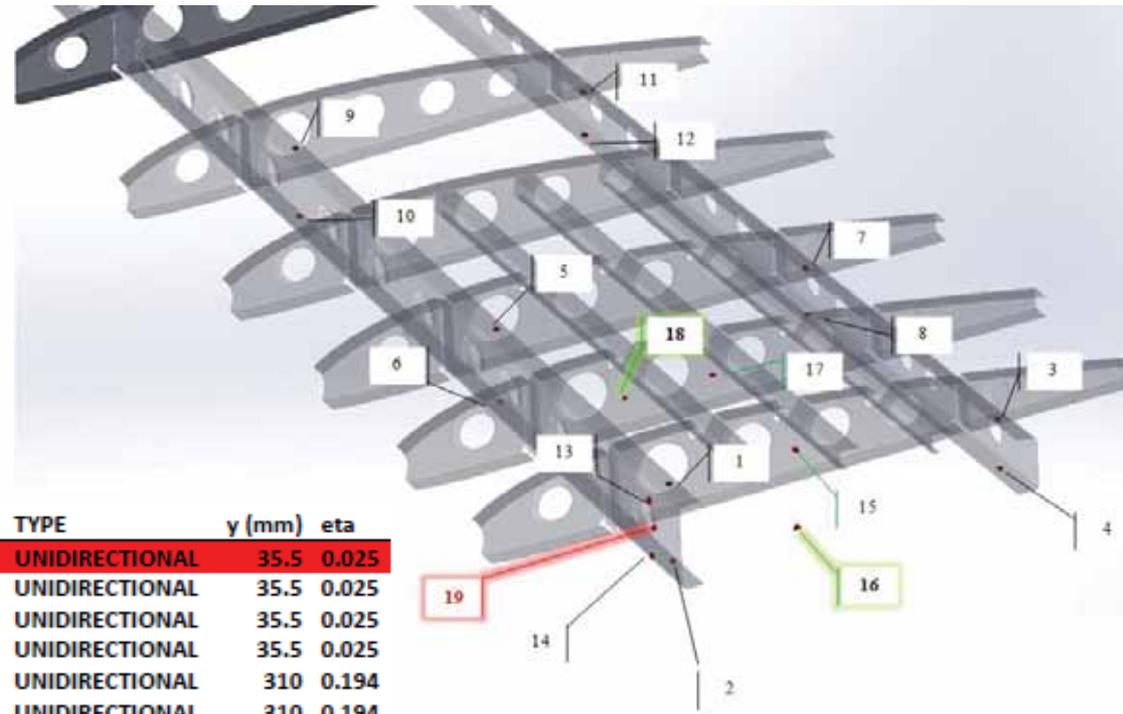


## TEST RESULTS. Pressure measurements

$\alpha = 6.6$  deg,  $C_L = 0.736$

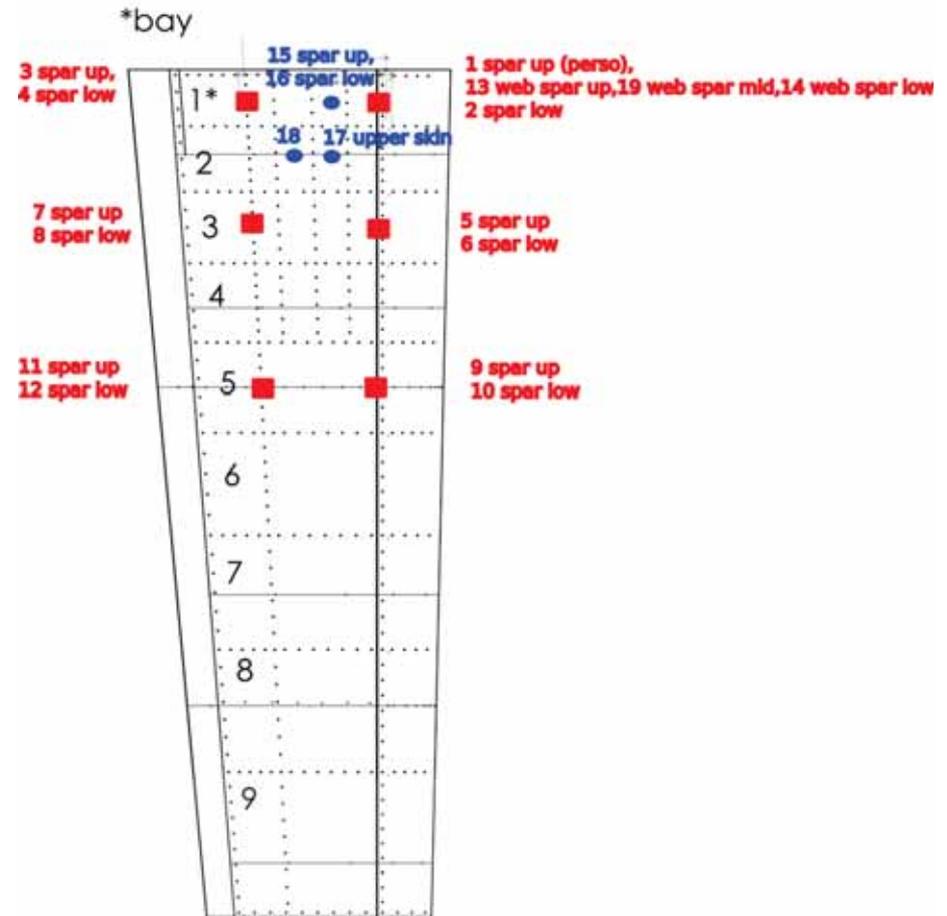
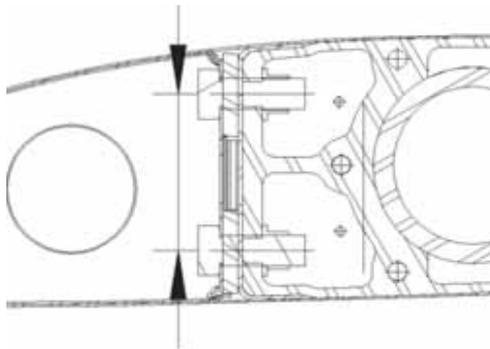


## TEST RESULTS. Strain and stress measurement



ID	Bay	POSITION	INSTALLATION	TYPE	y (mm)	eta
1	1	between rib1-rib2	front spar	UNIDIRECTIONAL	35.5	0.025
2	1	between rib1-rib2	front spar	UNIDIRECTIONAL	35.5	0.025
3	1	between rib1-rib2	rear spar	UNIDIRECTIONAL	35.5	0.025
4	1	between rib1-rib2	rear spar	UNIDIRECTIONAL	35.5	0.025
5	3	between rib3-rib4	front spar	UNIDIRECTIONAL	310	0.194
6	3	between rib3-rib4	front spar	UNIDIRECTIONAL	310	0.194
7	3	between rib3-rib4	rear spar	UNIDIRECTIONAL	297	0.194
8	3	between rib3-rib4	rear spar	UNIDIRECTIONAL	297	0.194
9	5	between rib5-rib6	front spar	UNIDIRECTIONAL	600	0.391
10	5	between rib5-rib6	front spar	UNIDIRECTIONAL	600	0.391
11	5	between rib5-rib6	rear spar	UNIDIRECTIONAL	598	0.391
12	5	between rib5-rib6	rear spar	UNIDIRECTIONAL	598	0.391
13	1	between rib1-rib2	front spar thickening	UNIDIRECTIONAL	35.5	0.025
14	1	between rib1-rib2	front spar thickening	UNIDIRECTIONAL	35.5	0.025
15	1	1stbay, between 1st and 2nd stringer	Upper Skin	UNIDIRECTIONAL	35.5	0.025
16	1	1stbay, correspondence to UD N.15	Lower Skin	ROSETTE-3SIGNAL	35.5	0.025
17	2	2ndbay, between 1st and 2nd stringer	Upper Skin	UNIDIRECTIONAL	169	0.106
18	2	2ndbay, between 2nd and 3rd stringer	Upper Skin	ROSETTE-3SIGNAL	169	0.106
19	1	between rib1-rib2	front spar	ROSETTE-3SIGNAL	35.5	0.025

## TEST RESULTS. Strain and stress measurement

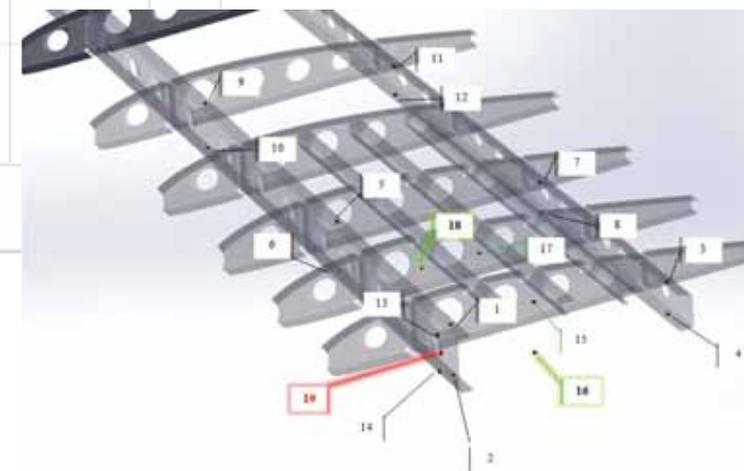
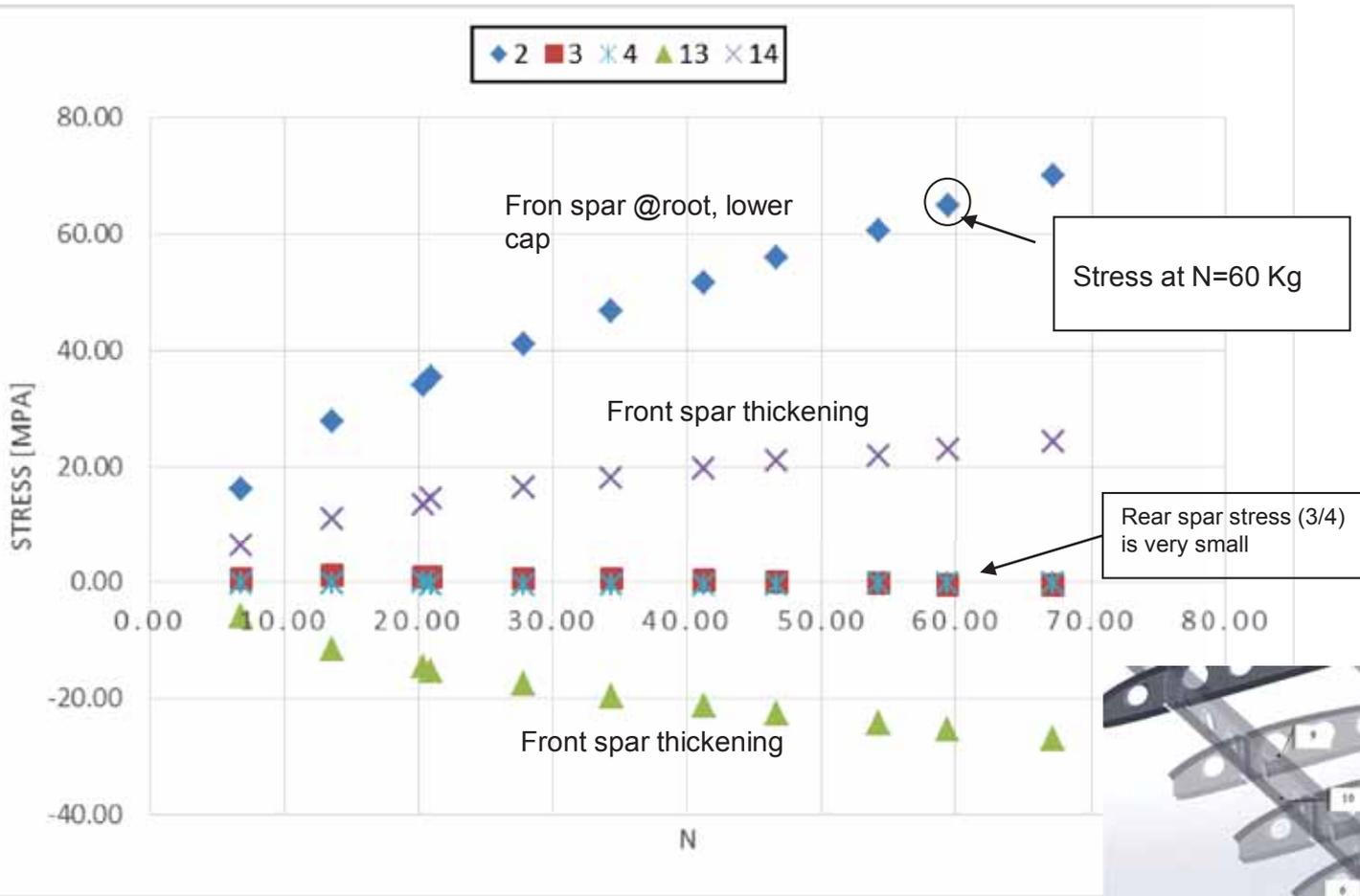


## TEST RESULTS. Strain and stress measurement

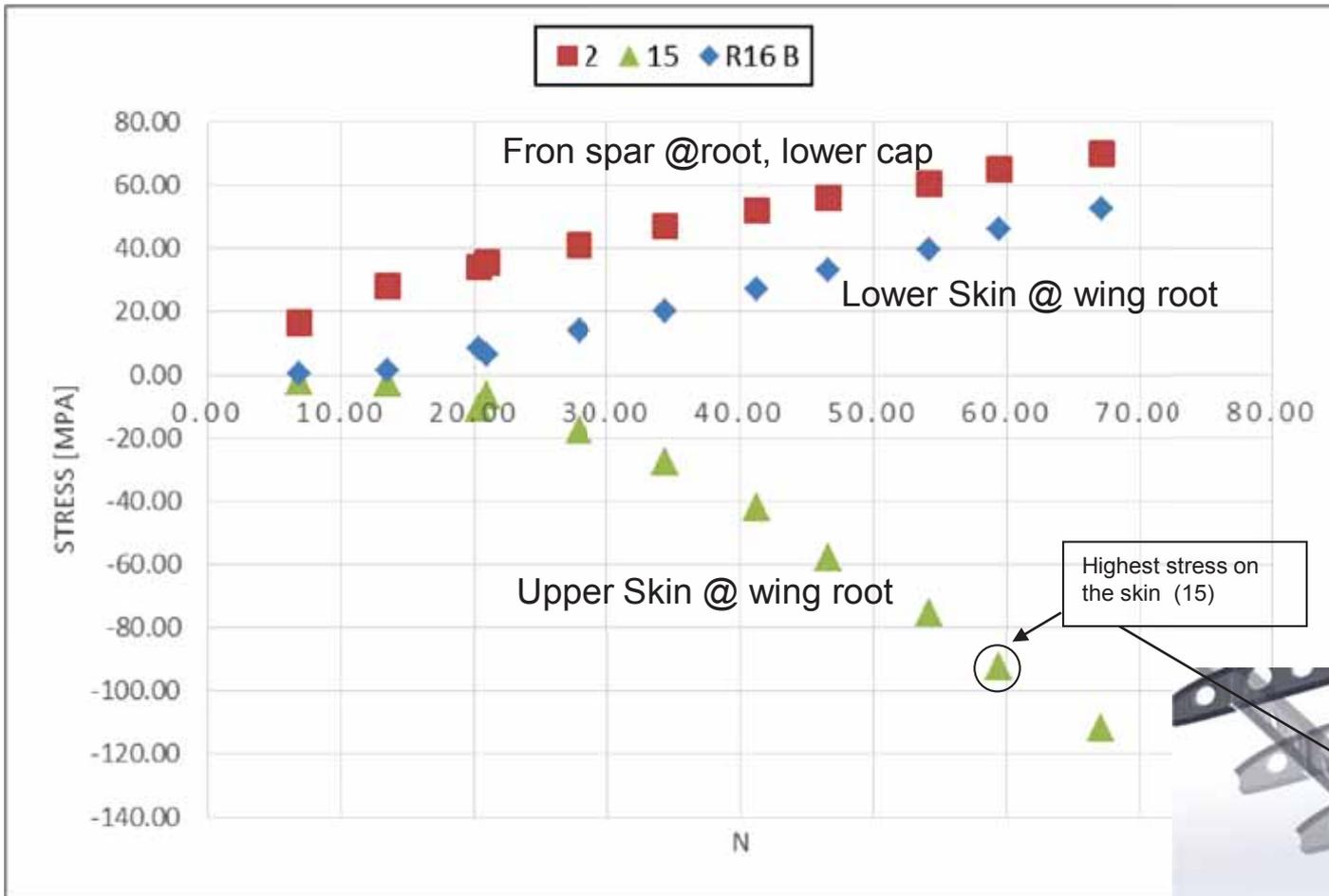
### Strain and stress measurement TEST T40, V=40 m/s , Fully turbulent

	Measured Forces and Moments							
Alfa_cor	N	Mfl	Yaw	Yaw_root	D	Mycb= My-	Mypolo	Mfl root
[°]	[kg]	[kgm]	[kgm]	[kg*m]	[Kg]	[kg*m]	[kg*m]	Kg m
-1.940	6.839	6.181	1.115	0.915	1.195	-2.279	-2.479	5.039
-0.850	13.536	12.042	1.039	0.849	1.137	-2.018	-2.441	9.782
0.250	20.370	17.941	1.049	0.857	1.151	-1.746	-2.395	14.540
0.360	20.989	18.470	1.043	0.852	1.143	-1.690	-2.360	14.964
1.490	27.873	24.419	1.145	0.938	1.241	-1.362	-2.257	19.765
2.590	34.378	30.105	1.321	1.085	1.413	-1.085	-2.192	24.364
3.700	41.261	36.209	1.577	1.298	1.670	-0.736	-2.066	29.318
4.750	46.616	41.015	1.819	1.496	1.929	-0.453	-1.954	33.230
5.880	54.178	47.827	2.192	1.794	2.384	-0.069	-1.810	38.779
6.920	59.420	52.519	2.436	1.975	2.761	0.244	-1.663	42.596
8.120	67.153	59.259	2.686	2.117	3.404	0.685	-1.463	48.044

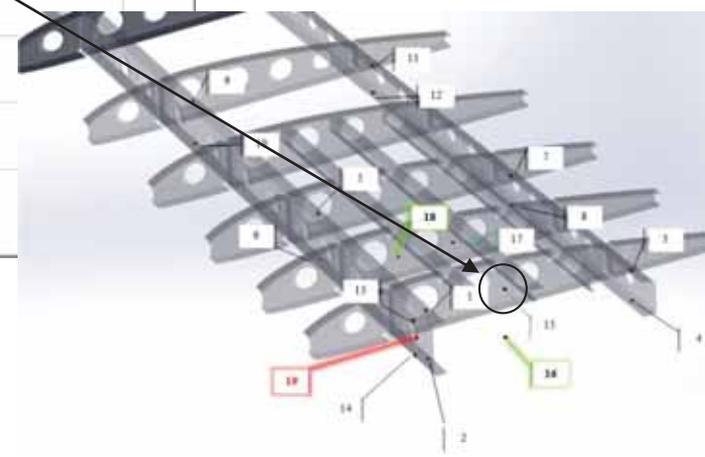
## TEST RESULTS. Strain and stress measurement V=40 m/s – Stress for different alpha (loads)



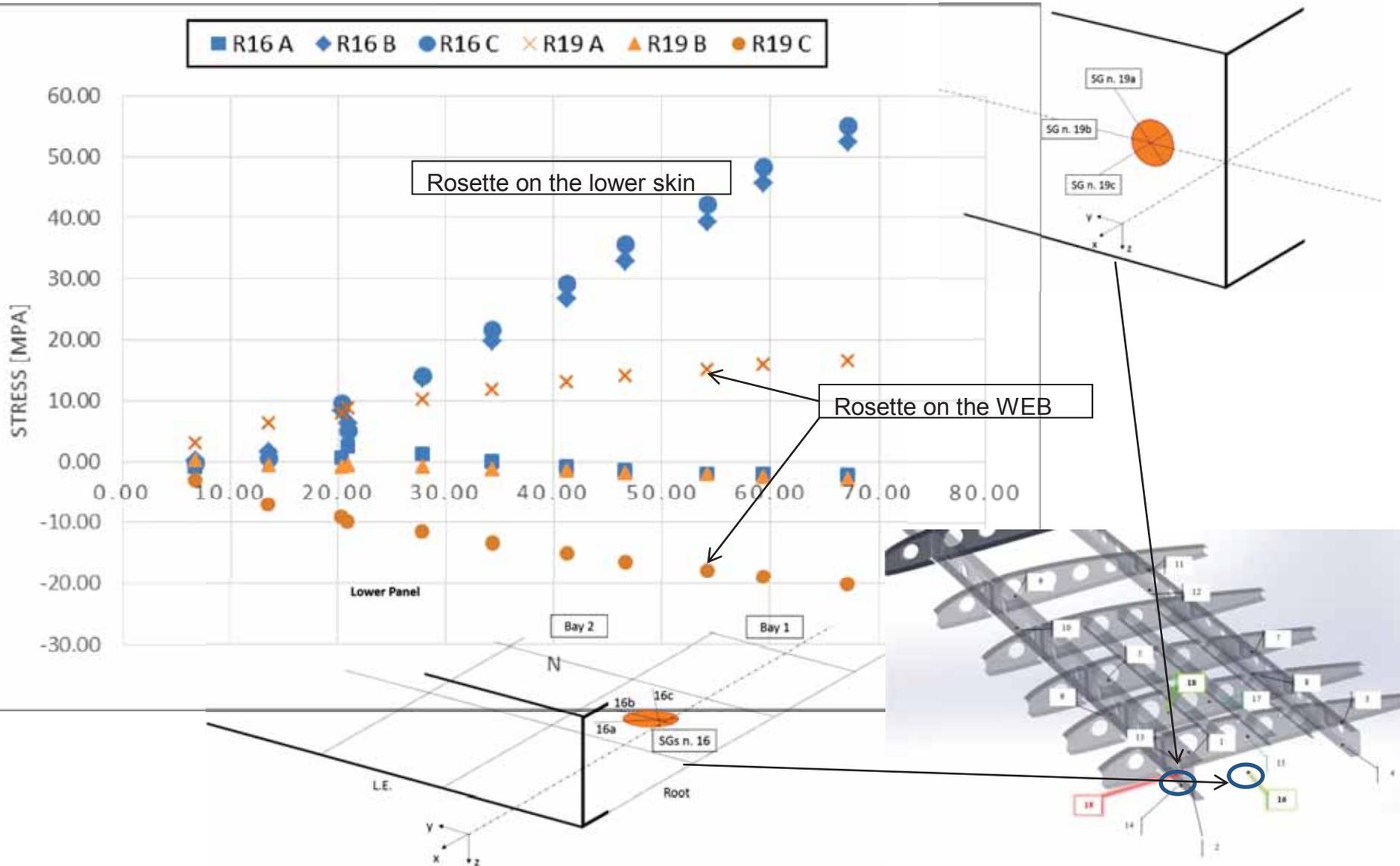
## TEST RESULTS. Strain and stress measurement V=40 m/s – Stress for different alpha (loads)



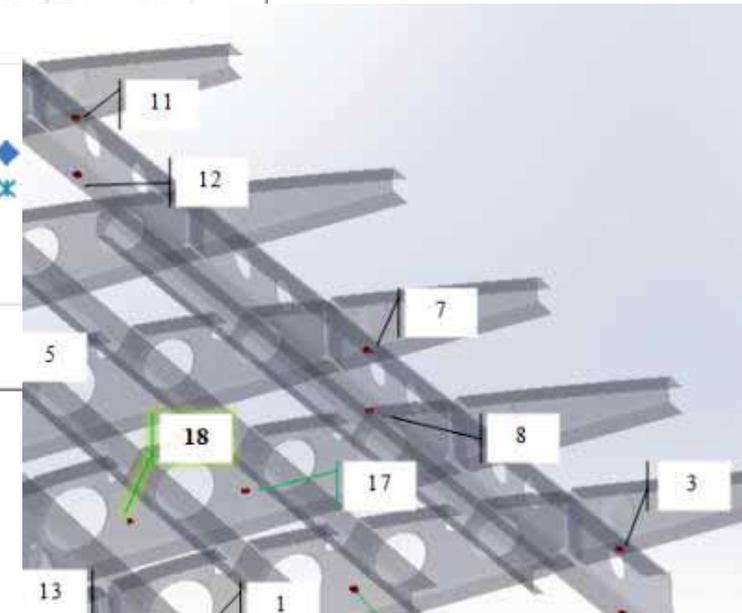
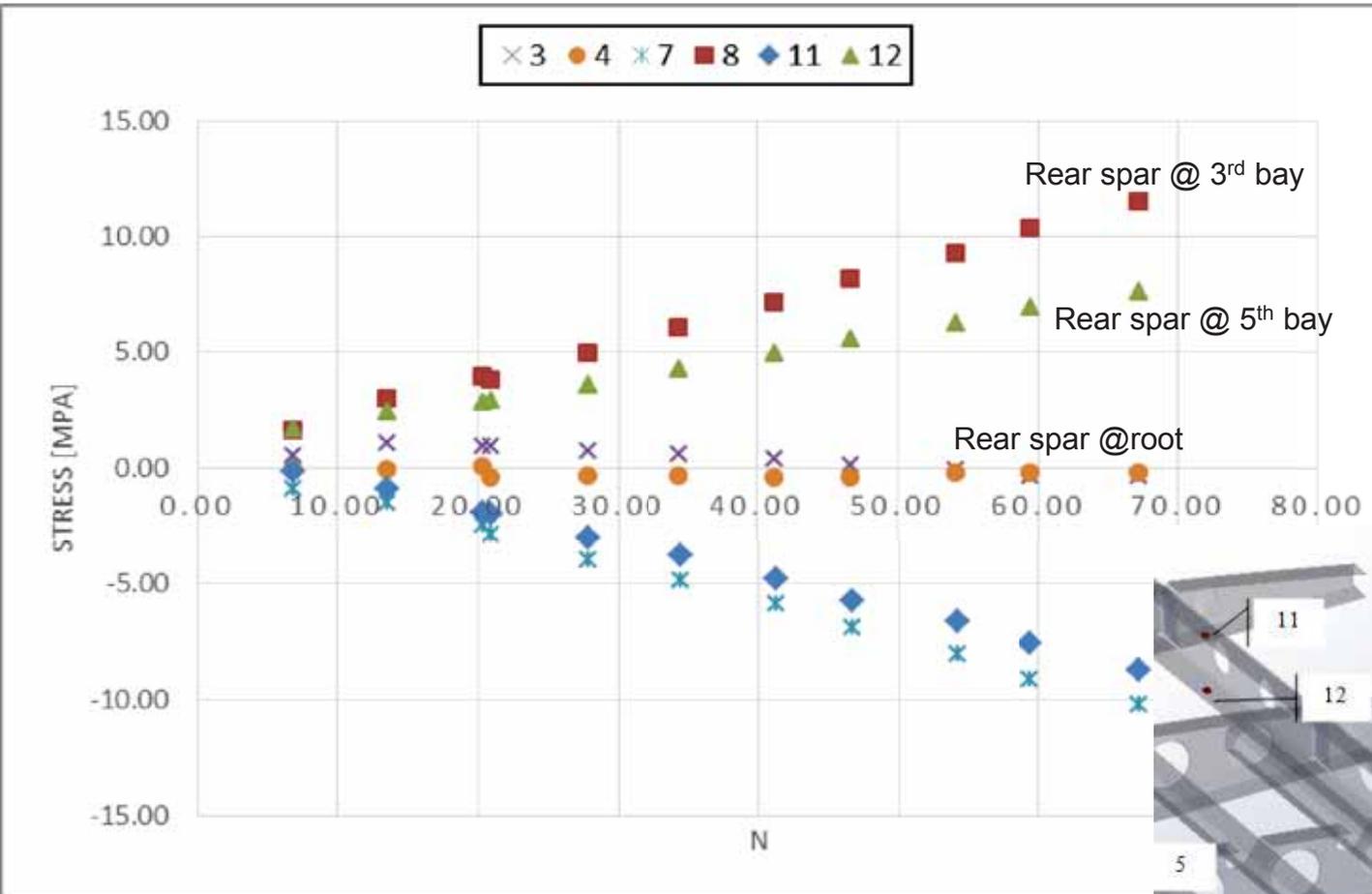
Highest stress on the skin (15)



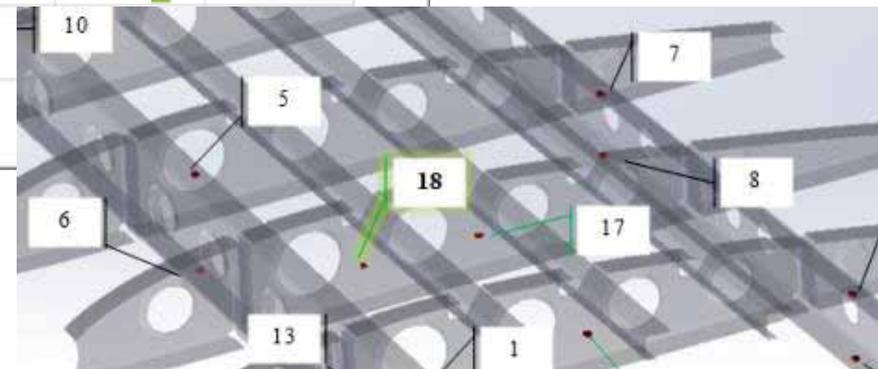
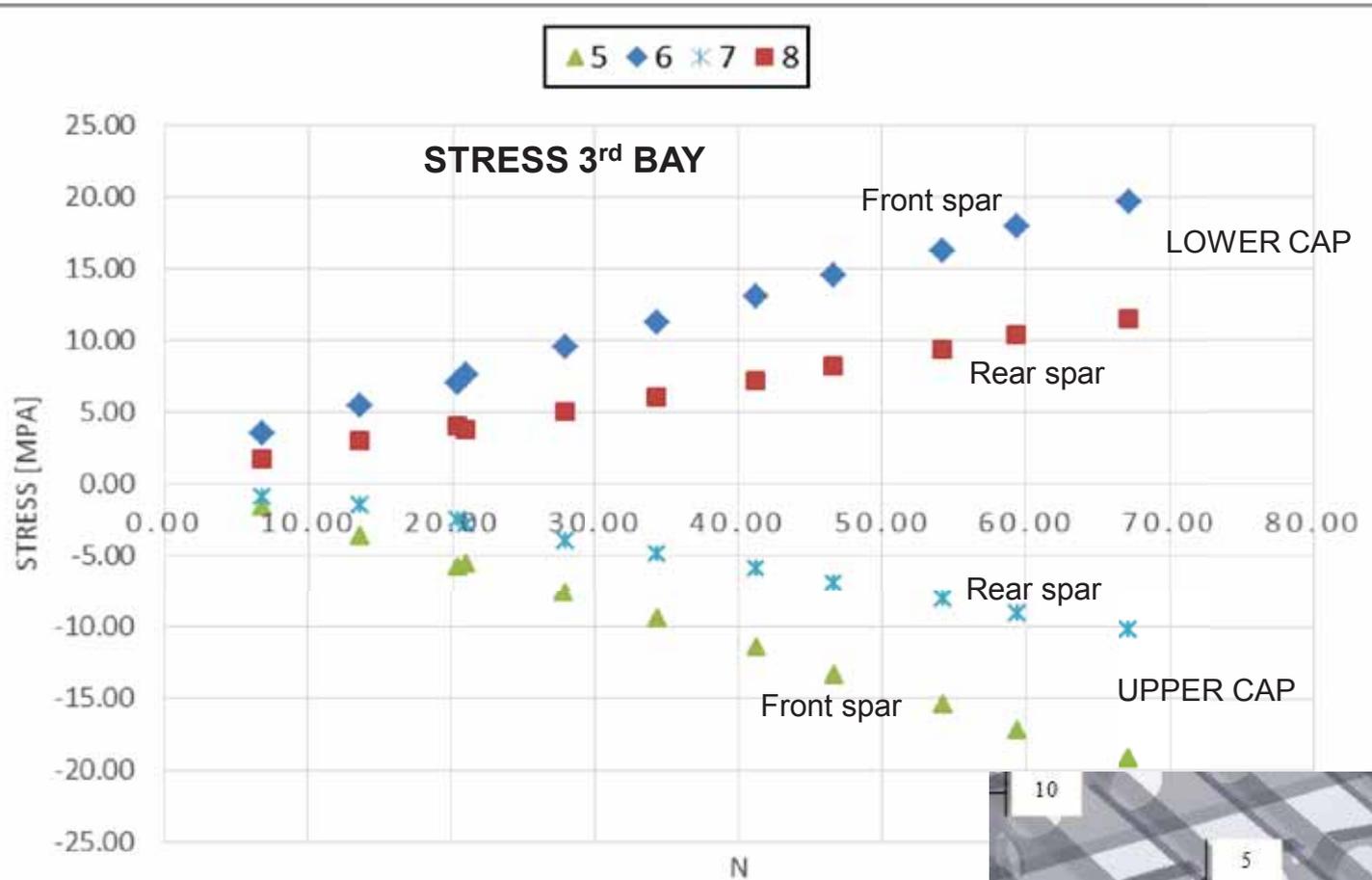
# TEST RESULTS. Strain and stress measurement V=40 m/s – Stress for different alpha (loads)



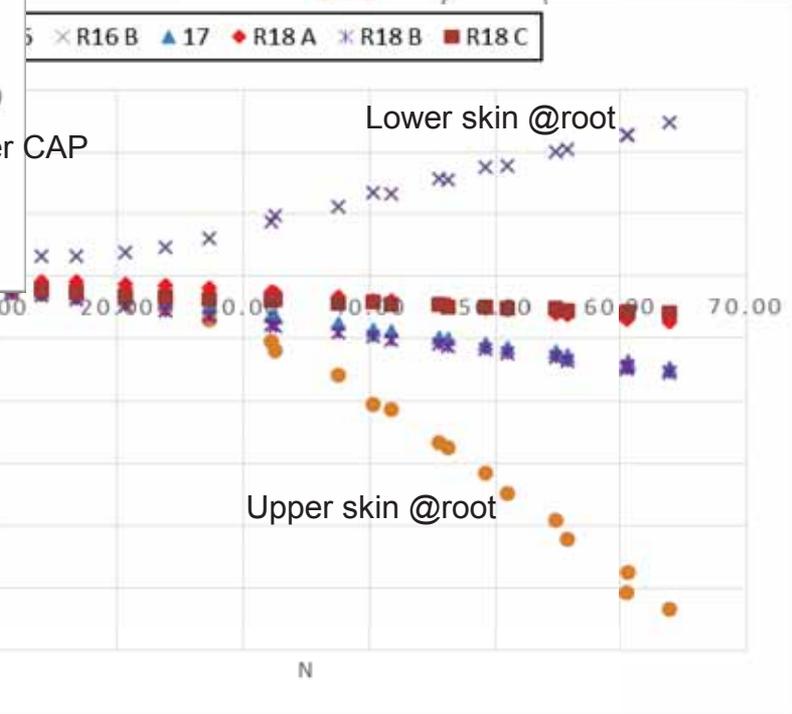
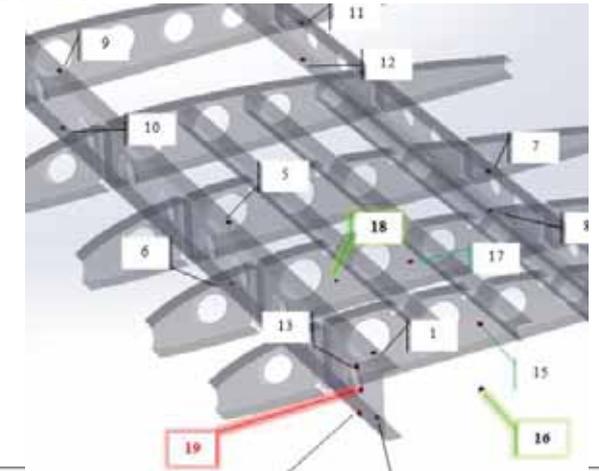
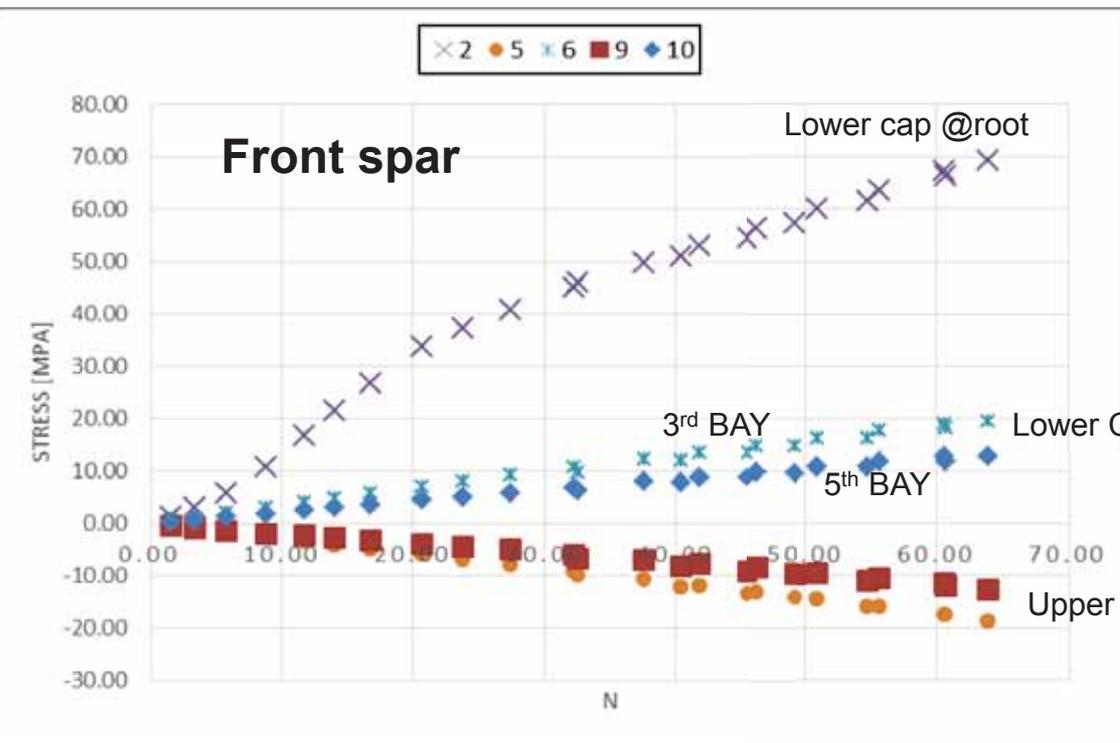
## TEST RESULTS. Strain and stress measurement V=40 m/s – Stress for different alpha (loads)



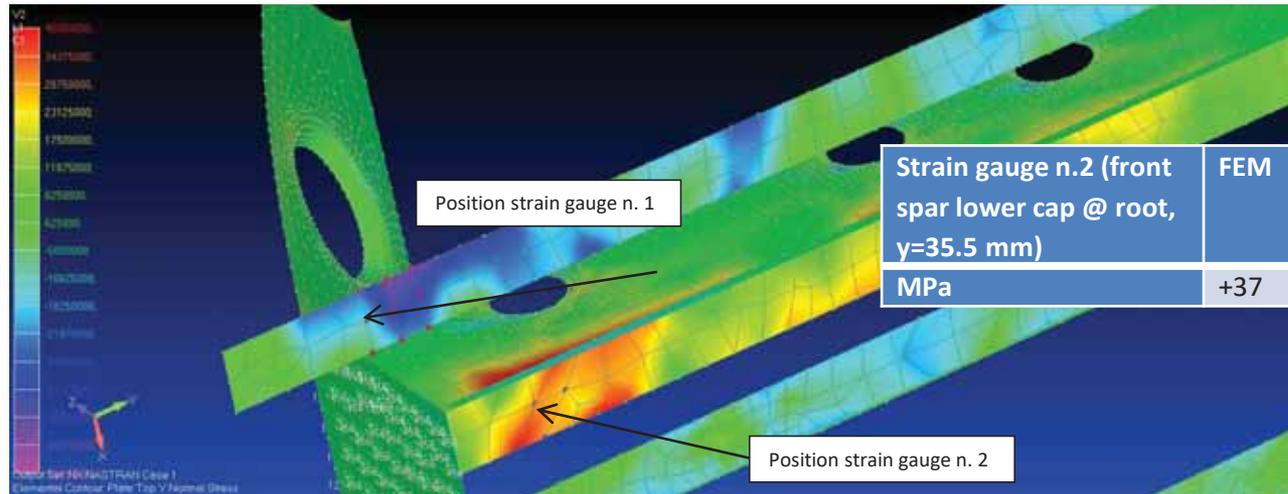
# TEST RESULTS. Strain and stress measurement V=40 m/s – Stress for different alpha (loads)



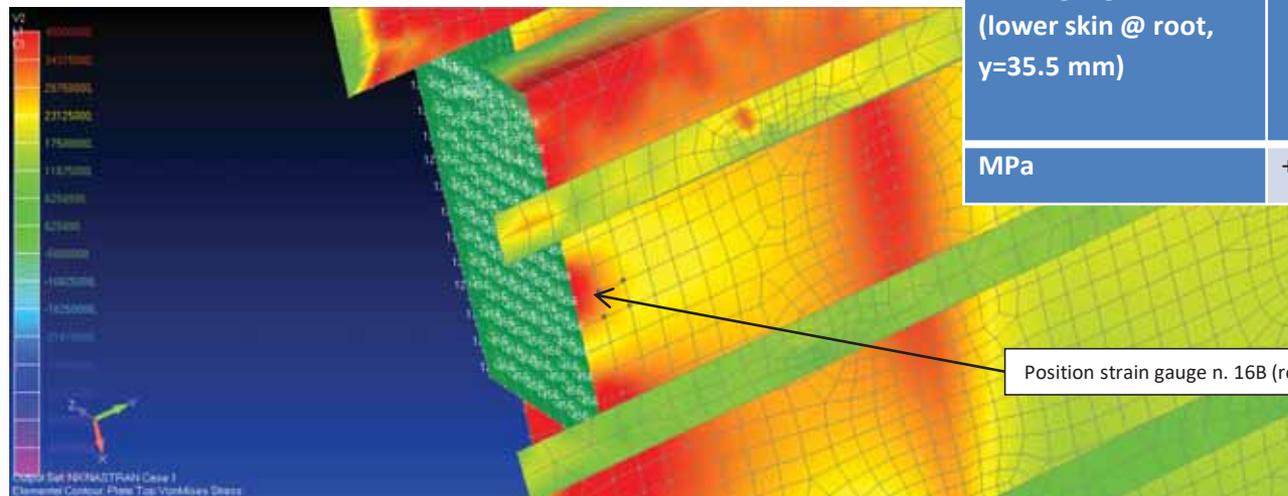
# TEST RESULTS. Strain and stress measurement , $\alpha=4^\circ$ , $V=$ variable



## TEST RESULTS. Strain and stress measurement , design condition V=40 m/s N=60 Kg

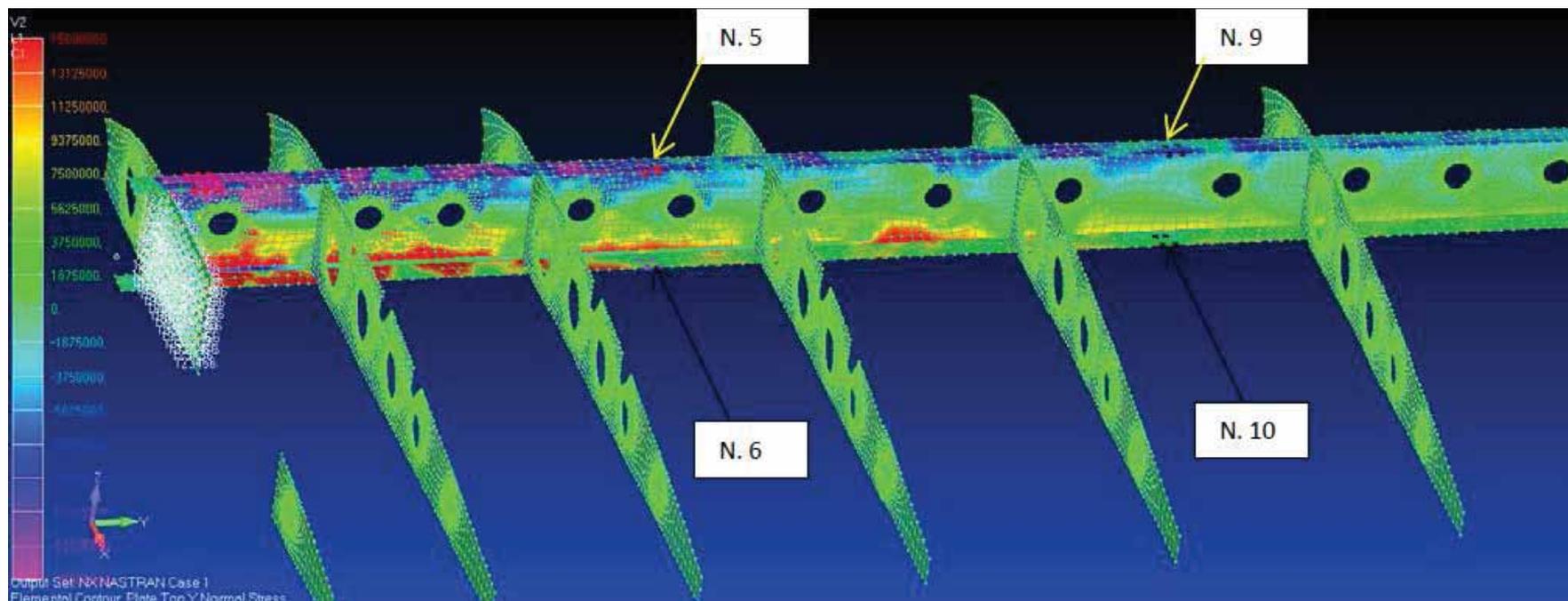


Strain gauge n.2 (front spar lower cap @ root, y=35.5 mm)	FEM	Experimental
MPa	+37	58



Strain gauge n.16B (lower skin @ root, y=35.5 mm)	FEM	Experimental
MPa	+26	44

## TEST RESULTS. Strain and stress measurement , design condition V=40 m/s N=60 Kg

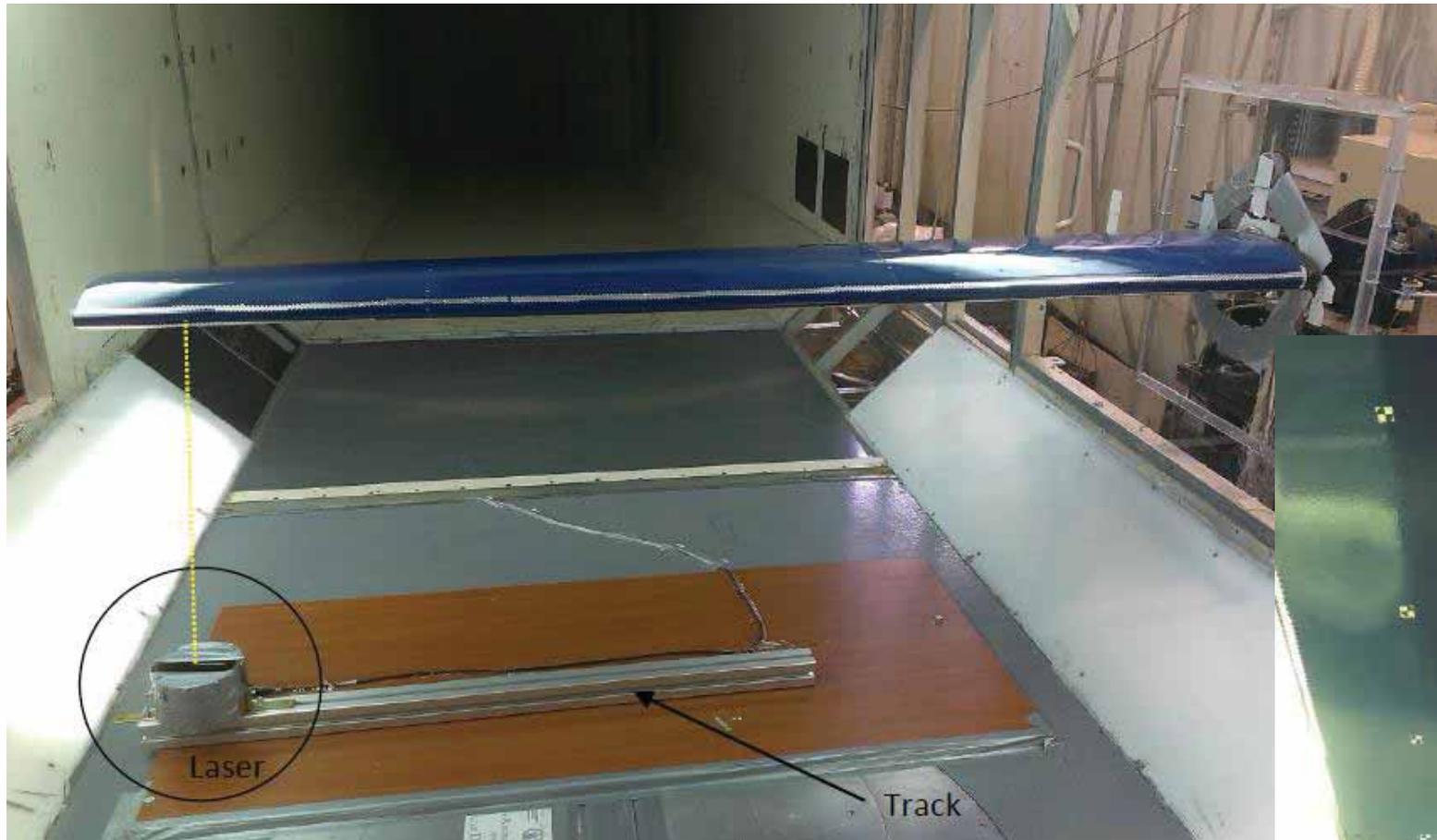


	FEM	Experimental
Strain gauge n.5 (front spar upper cap @ y=300 mm)	-16 Mpa	-17.5 Mpa
Strain gauge n.6 (front spar lower cap @ y=300 mm)	+15 MPa	18.2 MPa

	FEM	Experimental
Strain gauge n.9 (front spar upper cap @ y=600 mm)	-10 Mpa	-12.2 Mpa
Strain gauge n.10 (front spar lower cap @ y=600 mm)	+11 MPa	12.3 MPa

## TEST RESULTS. Deformation measurement

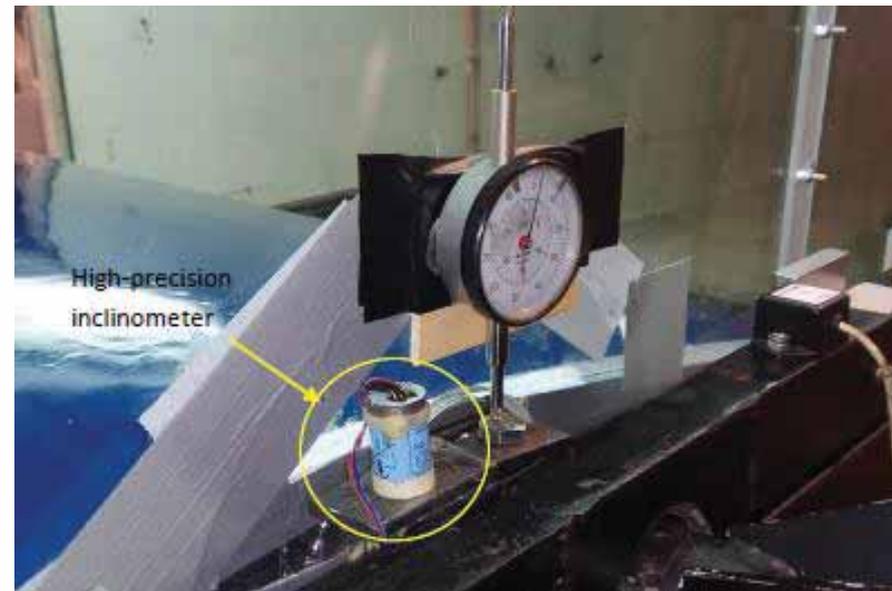
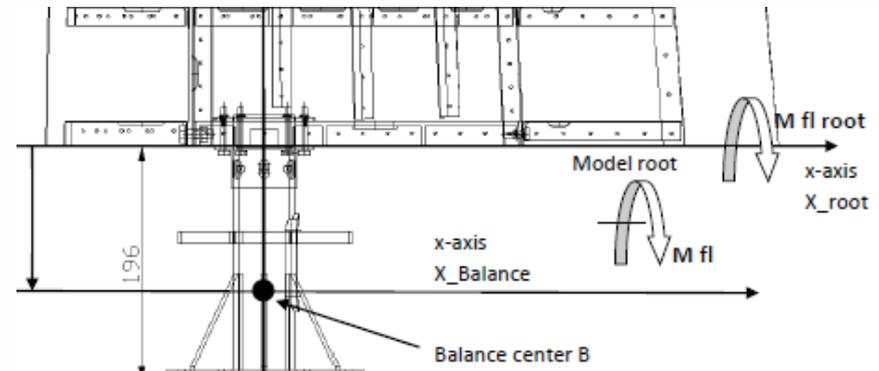
$V=40$  m/s,  $\alpha_g=6^\circ$ ,  $\alpha_c=7^\circ$   $N=60$  Kg



**TEST RESULTS. Deformation measurement**  
**V=40 m/s,  $\alpha_g=6^\circ$ ,  $\alpha_c=7^\circ$  N=60 Kg**

**Highly accurate tilt sensor**  
**On the wing root**

**Measure model rotation @ root**



**TEST RESULTS. Deformation measurement****V=40 m/s,  $\alpha_g=6^\circ$ ,  $\alpha_c=7^\circ$  N=60 Kg**

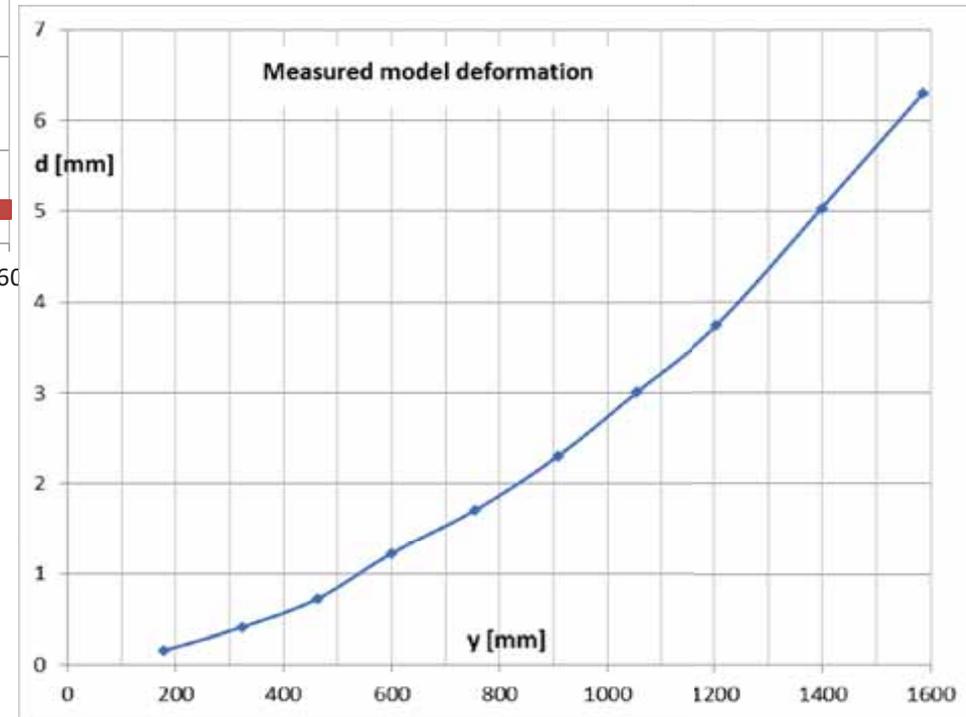
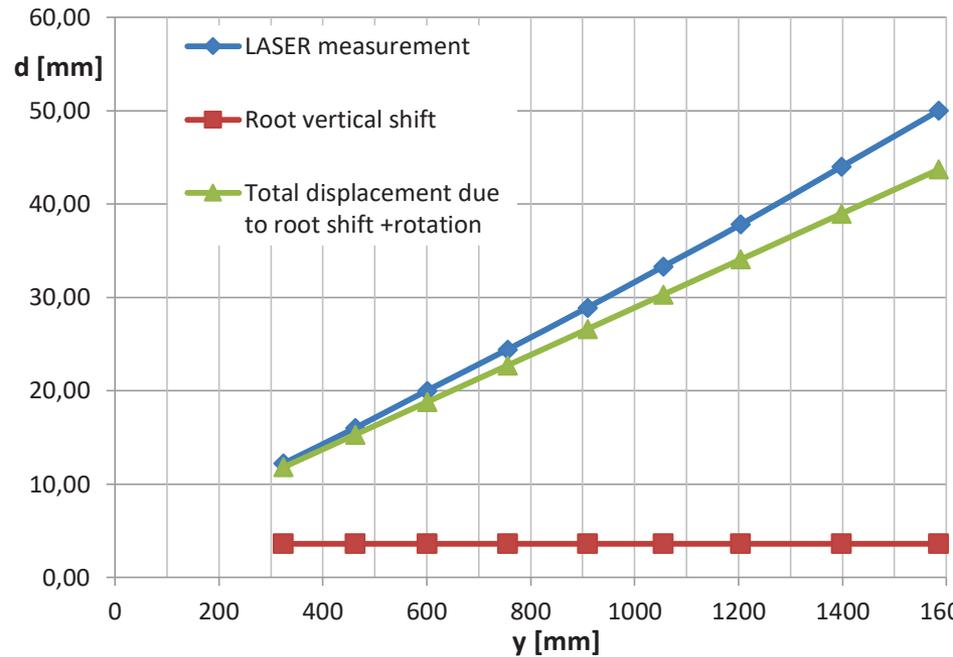
MARK	y [mm]	V	Normal Force	Root Inclinom Midori	LASER Measurem	Vertical root displacement (micro-meter comparator)	Total vertical shift	Shift due to only Root ROT	Deformation
		[m/s]	[Kgf]	[deg]	[mm]	[mm]	[mm]	[mm]	[mm]
11	1585	39.20	60.3	1.45	50.00	3.594	43.70	40.10	6.30
10	1398	39.20	60.3	1.45	44.00	3.590	38.96	35.37	5.04
9	1204	39.20	60.3	1.45	37.8	3.590	34.05	30.46	3.75
8	1055	39.20	60.3	1.45	33.30	3.590	30.28	26.69	3.02
7	909	39.20	60.3	1.45	28.90	3.590	26.59	23.00	2.31
6	755	39.20	60.3	1.45	24.40	3.590	22.69	19.10	1.71
5	600	39.20	60.3	1.45	20.00	3.590	18.77	15.18	1.23
4	462	39.20	60.3	1.45	16.00	3.590	15.28	11.69	0.72
3	324	39.20	60.3	1.45	12.20	3.590	11.79	8.20	0.41
2	178	39.20	60.3	1.45	8.25	3.590	8.09	4.50	0.16
1	35	39.20	60.3	1.45		3.590	4.48	0.89	

**From measurements of point 11 and 11P(Posteriore) at different chord position, also the torsion at wing tip has been measured:**

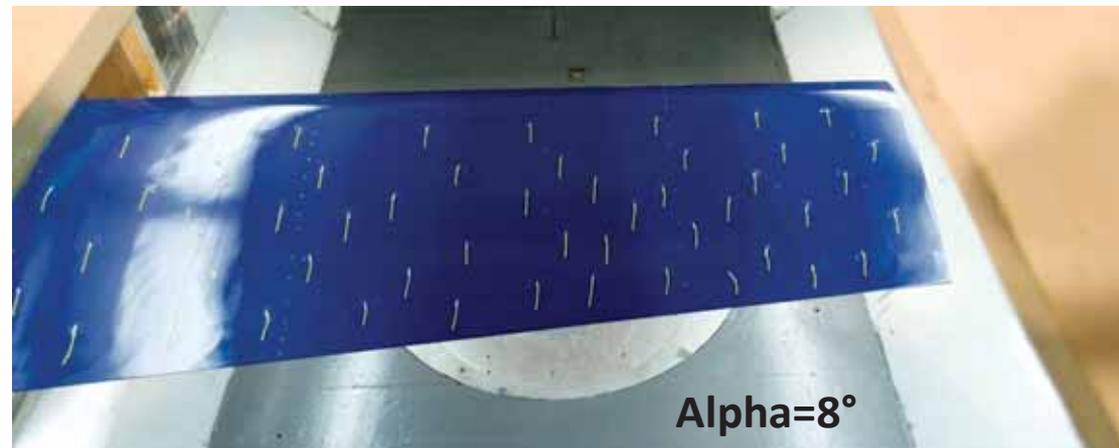
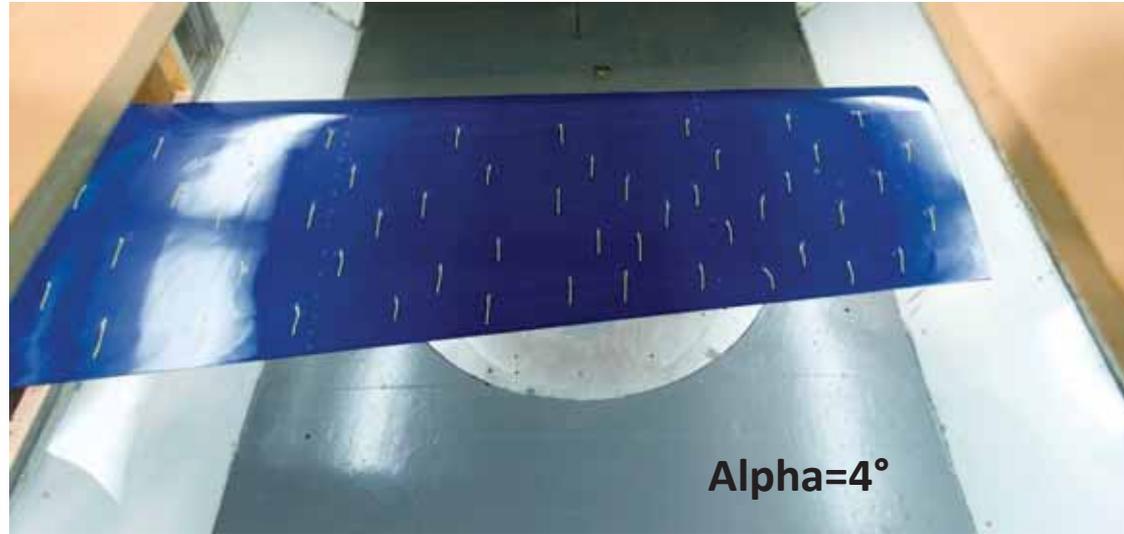
**The torsional deformation at wing tip has been measured and is equal to 0.82 deg. (positive, twist up).**

## TEST RESULTS. Deformation measurement

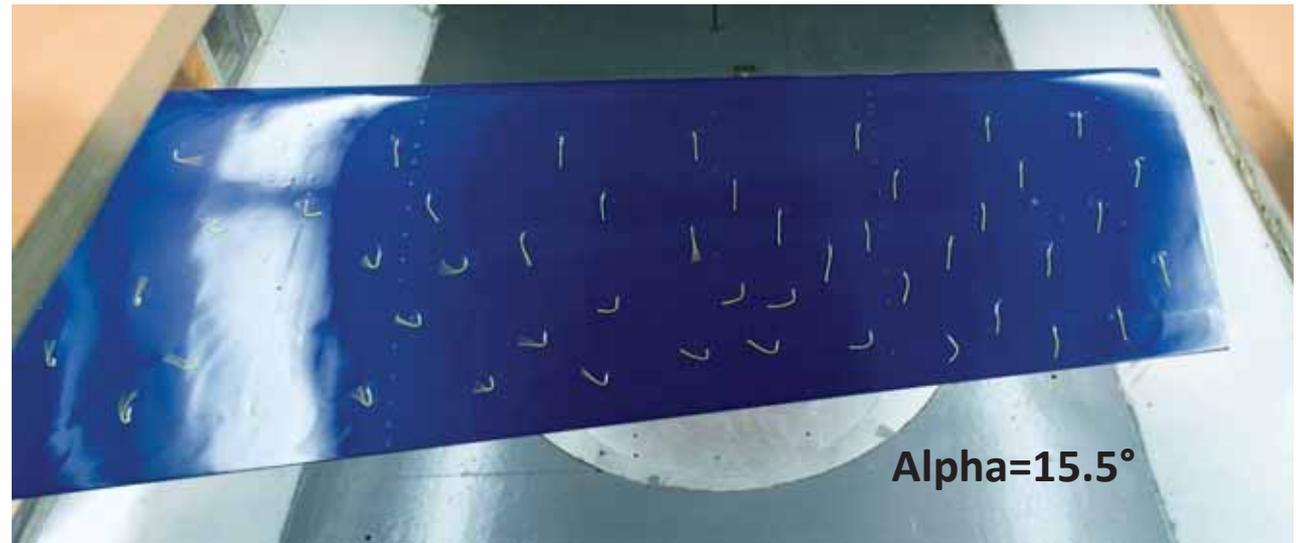
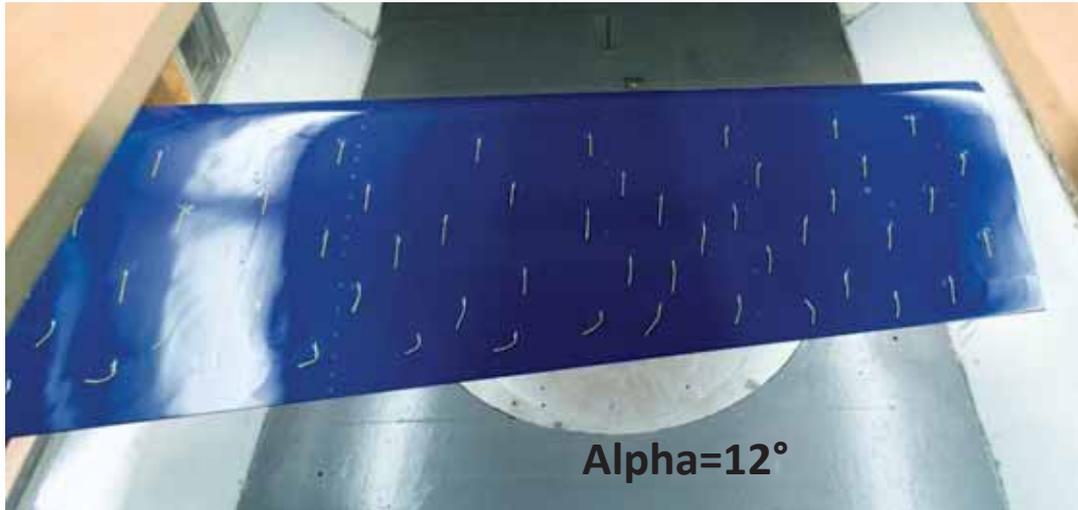
V=40 m/s,  $\alpha_g=6^\circ$ ,  $\alpha_c=7^\circ$  N=60 Kg



## TEST RESULTS. Visualization with tufts



## TEST RESULTS. Visualization with tufts



## CONCLUSIONS

- Model design and building
- Force and pressure measurement
- Only small discrepancies at l.e. in a section
- Good comparison with numerical results

### **Further considerations (concerning stress and deformation) :**

- It is difficult with a typical airplane structure and small dimensions to:
  - have very accurate reproduction of shape (especially at l.e.)
  - ensure reasonable deformations (especially torsional)
- Difficult to model constraint at root with connections through bolts